BERING STRAIT NORSEMAN II 2021 MOORING CRUISE REPORT

Research Vessel Norseman II, Norseman Maritime Charters Nome-Nome, 7th July to 17th July 2021

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Funding from NSF Arctic Observing Network Program PLR-1758565

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Cecilia Peralta-Ferriz, UW

Related PIs:

Marine Mammal Recorders:
Kate Stafford, UW, USA

Trace Metal/Nutrient Sampling:

Laramie Jensen, Randi Bundy, Ryan McCabe, UW Glider:

NORSEMAN NORSEMAN

Research vessel Norseman II during 2019 Nome on-load [Credit: Woodgate].

Hank Statscewich, University of Alaska Fairbanks (UAF)

As part of the Bering Strait project funded by NSF-AON (Arctic Observing Network), in July 2021 a team of US scientists undertook a $^{\sim}$ 11 day cruise in the Bering Strait and southern Chukchi Sea region on the US vessel Norseman II, operated by Support Vessels of Alaska, Inc..

The primary goals of the expedition were:

- 1) recovery of 6 moorings carrying physical oceanographic (Woodgate & Peralta Ferriz) and whale acoustic (Stafford) instrumentation. These moorings were deployed in the Bering Strait region in 2019 and 2020 from the Norseman II. The funding for the physical oceanographic components of these moorings comes from NSF-AON.
- 2) deployment of 3 moorings in the Bering Strait region, carrying physical oceanographic (Woodgate & Peralta-Ferriz) and whale acoustic (Stafford) instrumentation. The funding for the physical oceanographic components of these moorings comes from NSF-AON.
 - 3) collection of trace metal/nutrient water samples using a pumped system at selected CTD casts (Jensen)
 - 4) a set of CTD sections studying water properties in the region (Woodgate & Peralta-Ferriz)
- 5) collection of accompanying ship's underway data, viz. surface water temperature and salinity, ADCP velocity data and meteorological data (Woodgate & Peralta-Ferriz),
 - 6) deployment of a glider (Statscewich).

The cruise loaded and offloaded gear in Homer, Alaska, and people in Nome, Alaska.

As a Covid precaution, the science team quarantined in Fairbanks for 10 days prior to the cruise and transferred to the ship via a private air charter flight

Key Statistics:

6 moorings recovered, 3 moorings deployed, 276 CTD casts on 14 CTD lines, trace metal/nutrient water samples taken on 41 stations, 1 glider deployed

SCIENCE BACKGROUND

The \sim 50m deep, \sim 85km wide Bering Strait is the only oceanic gateway between the Pacific and the Arctic oceans.

The oceanic fluxes of volume, heat, freshwater, nutrients and plankton through the Bering Strait are critical to the water properties of the Chukchi [Woodgate et al., 2005a]; act as a trigger of sea-ice melt in the western Arctic [Woodgate et al., 2010]; provide a subsurface source of heat to the Arctic in winter, possibly thinning sea-ice over about half of the Arctic Ocean [Shimada et al., 2006; Woodgate et al., 2010]; are ~ 1/3rd of the freshwater input to the Arctic [Aagaard and Carmack, 1989; Woodgate and Aagaard, 2005]; and are a major source of nutrients for ecosystems in the Arctic Ocean and the Canadian Archipelago [Walsh et al., 1989]. In modeling studies, changes in the Bering Strait throughflow also influence the Atlantic Meridional Overturning Circulation [Wadley and Bigg, 2002] and thus world climate [De Boer and Nof, 2004].

Quantification of these fluxes (which all vary significantly seasonally and interannually) is critical to understanding the physics, chemistry and ecosystems of the Chukchi Sea and western Arctic, including sea-ice retreat timing and patterns, and possibly sea-ice thickness. The Bering Strait oceanic heat flux has been found to be the best predictor of Chukchi sea ice retreat [Serreze et al., 2016]. Understanding the processes setting these fluxes is vital to prediction of future change in this region, in the Arctic, and beyond. The Bering Strait is the only Arctic gateway where observations currently show significant interannual change [Østerhus et al., 2019].

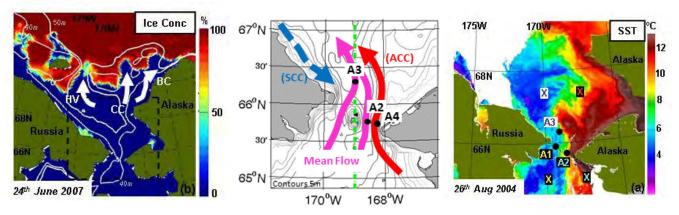


Figure 1: (Left) Chukchi Sea ice concentration (AMSR-E) with schematic topography. White arrows mark three main water pathways melting back the ice edge [Woodgate et al., 2010].

(Middle) Detail of the Bering Strait, with schematic flows and mooring locations (black dots – A2, A3, A4). The main northward flow passes through both channels (magenta arrows). Topography diverts the western channel flow eastward near site A3. The warm, fresh Alaskan Coastal Current (ACC) (red arrow) is present seasonally in the east. The cold, fresh Siberian Coastal Current (SCC) (blue dashed arrow) is present in some years seasonally in the west. Green dashed line at 168°58.7'W marks the US-Russian EEZ (Exclusive Economic Zone) boundary. Note all moorings are in the US EEZ. Depth contours are from IBCAO [Jakobsson et al., 2000]. The Diomede Islands are in the center of the strait, shown here as small black dots on the green dashed line marking the US-Russian boundary.

(Right) Sea Surface Temperature (SST) MODIS/Aqua level 1 image from 26th August 2004 (courtesy of Ocean Color Data Processing Archive, NASA/Goddard Space Flight Center). White areas indicate clouds. Note the dominance of the warm ACC along the Alaskan Coast, and the suggestion of a cold SCC-like current along the Russian coast [Woodgate et al., 2006].

Since 1990, year-round moorings have been maintained almost continually year-round in the Bering Strait region, supported by typically annual servicing and hydrographic cruises [Woodgate et al., 2015; Woodgate, 2018]. These data have allowed us to quantify seasonal and interannual change [Woodgate et al., 2005b; Woodgate et al., 2006; Woodgate et al., 2010; Woodgate et al., 2012; Woodgate, 2018; Woodgate and Peralta-Ferriz, 2021], and assess the strong contribution of the Alaskan Coastal Current (ACC) to the fluxes through the strait [Woodgate and Aagaard, 2005; Woodgate, 2018]. These data also show that the Bering Strait throughflow increased ~50% from 2001 (~0.75v) to 2011 (~1.15v), driving heat and freshwater flux increases

[Woodgate et al., 2012], with more recent fluxes also being high (e.g., 2014, 1.2Sv, [Woodgate, 2018; Woodgate and Peralta-Ferriz, 2021], see Figure 2).

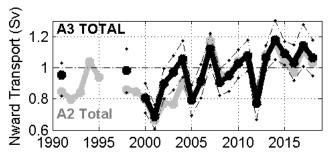
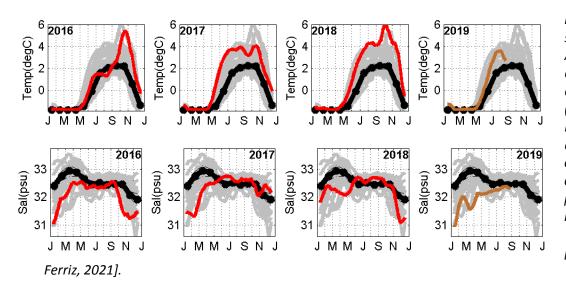


Figure 2: Annual mean (x-axis, time in years) of Bering Strait mooring data from 1991 to 2018, showing transport for the whole strait, as estimated from A2 (grey) or A3 (black).

Analysis [Woodgate, 2018] indicates this long term trend is driven by large scale changes between the Pacific and the Arctic oceans, with no significant trends

in the winds in the strait. Thus, satellite-sensed data sets (winds, SST) prove insufficient for quantifying long-term variability, indicating interannual change can still only be assessed by in situ year-round measurements [Woodgate et al., 2012]. The work to be accomplished on this cruise will extend this mooring time-series to mid-2022.

In addition, this cruise aims to provide a high resolution survey of the water properties of the strait and southern Chukchi Sea in early-summer. A particular goal is to quantify the early season heat and salt content of the waters, which have been unusually warm and fresh in the last 4 years (see Figure 3).



3: 30 **Figure** day smoothed near-bottom temperature and salinity (bottom), data for recent years (columns), showing labeled year in color, climatology [Woodgate et al., 2005b] in black, and all prior years (1990present) in grey. X-axis labels show month (J=January,etc.), [Woodgate and Peralta-

The winter freshenings observed are particularly remarkable and suggest Pacific waters are entering the Arctic 50m shallower than before, and no longer refreshing the cold layer which historically protected the sea ice from warmer Atlantic waters below. The impacts of this on Arctic climate are currently unclear.

In addition to physical oceanographic goals, our work also supports long term marine mammal acoustic monitoring in the Strait (PI: Stafford).

International links: Maintaining the time-series measurements in Bering is important to several national and international programs, e.g., the Arctic Observing Network (AON), started as part of the International Polar Year (IPY) effort in 2007; various NSF, ONR and NPRB projects and missions in the region. For several years, the work was part of the RUSALCA (Russian-US Long Term Census of the Arctic). Some of the CTD lines are part of the international Distributed Biological Observatory (DBO) effort. The mooring work also supports regional studies in the area, by providing key boundary conditions for the Chukchi Shelf/Beaufort Sea region (a current focus on ONR Arctic programs); a measure of integrated change in the Bering Sea, and an indicator of the role of Pacific Waters in the Arctic Ocean.

2021 CRUISE SUMMARY:

Since in 2020 no Bering Strait mooring recoveries were done due to the Covid situation, we scheduled our 2021 Bering Strait mooring cruise for July, traditionally a time of few storms, and early in the season, in the hope of avoiding the need to drag for too many of the old moorings.

Even though the Covid vaccination program was well advanced in both Washington and Alaska, anti-Covid precautions were still required for the cruise, and the science team followed a strict pre cruise quarantine consisting of 14 days "Strict social Distancing" in Seattle, a pre flight test, a 10-day isolation quarantine in Fairbanks, another predeparture test, and then a charter flight (rather than a commercial flight) to Nome. The charter flight left Fairbanks early (~ 7:30am) on the first day of the cruise (7th July 2021), and under a special arrangement with Nome, the science team transferred directly to the ship from the airport, without entering the airport building.

To minimize contacts in Nome, science gear was also loaded in Homer (the home port of the ship), rather than Nome, with the ship leaving Homer for Nome on the 29th June 2021. The transit north was used to trouble shoot the underway systems. Three issues were encountered - the seawater intake system not transmitting data (which seemed to resolve itself), the aft GPS providing erroneous dates (this is the GPS week rollover error, and resolved by using a different GPS unit/post processing), and the meteorological package (new this year), not logging (a set up issue). The ship reached Nome on the 6th July and on the am of the 7th July performed a calibration of the meteorological sensors' compass just outside Nome, prior to the arrival of the science party.

The ship sailed from Nome shortly after everyone was on board. The transit to the strait was used to set up science gear, including repotting the CTD termination and doing a test CTD cast.

The 8th July provided good weather for the first day of recoveries. Four mooring recoveries (A2-20, A2-19, A4-20, A4-19) were completed smoothly, with pre-recovery CTD casts. All moorings released as planned with no dragging necessary. It proving too late in the day to transit to A3 in time for working, an underway section across the Alaskan Coastal Current was run while the A2 mooring was prepared for deployment. Mooring A2-20 was deployed, and a post-deployment CTD was taken. The ship then ran underway sections (to BS11, up to NBS10, west along NBS and then up to A3) until the next morning. In the preliminary part of this run, the trace metal/nutrient pumping system was set up and tested.

The 9th July again provided good weather for mooring recoveries. After pre-recovery CTD casts, mooring A3-20 was recovered smoothly. Mooring A3-19 required dragging, an operation which first brought aboard one of our prior anchors (in extremely good condition). The A3-19 mooring was sighted during this operation and safely recovered afterwards. Then mooring A3-21 was deployed, with its accompanying post deployment CTD cast, and the ship steam south running underway lines (S along the DL line, east along BS, west back along BS, east along BS again) to be at A4 for the morning. These underway sections should capture the movement of the ACC under a wind change from southward to northward winds.

During this transit, we became aware that the release system for the iscat had not been installed in the A3 mooring. Thus, to safeguard the most important mooring of our project, we postponed the deployment of A4 until A3 could be recovered, repaired and redeployed, an operation which required better weather than we currently had. Thus, on the 10th July, we instead ran the BS CTD line, with sampling for trace metals/nutrients, continuing N along the DL lines (no trace metals/nutrients) and the A3line (with trace metals/nutrients). This enabled us to return to A3 for the mooring operations at A3 on the morning of the 11th of July. From that operation, we steamed to A4, to deploy A4-21, and then returned north to continue our CTD survey, pausing around the A3 line that evening to deploy the glider.

Starting early on the 12th July, we CTDed (with trace metal/nutrient sampling) the CS line towards Point Hope, although poor weather forced us to suspend operations for ~ 4hrs after CS13, a cast we retook once the weather had calmed to test the continuity of the section. The PH line was started late that night, and run westward to NPH13 only, a time choice to allow timely completion of the other sections, the end location being chosen beyond a chlorophyll maximum found in prior years, but absent this year. Thus on the 13th July, we completed the shortened NPH line, ran the CD line east from CD14, and the LIS line westward with trace metal/nutrient sampling, and started the CCL line heading south towards the NPH line. The initial stations of the

LIS line found remarkably fresh water (~ 25psu) and some surface samples were taken for O18 analysis when back in Seattle.

On the 14th July we repeated the NPH line (this time in full) and the CS line (this time in almost calm). A dead grey whale was spotted around station CS14.5 and reported to NOAA. In the teeth of a poor forecast, we started working south along the CCL line and DL lines late that evening. The bad weather predicted arrived on the 15th July, breaking off CTD operations after cast DL16.5. To retain a chance of repeating the BS line, we continued S into the high winds, attaining the lee of the Diomede islands around 11pm. During the night, we transited back and forward around the north and east sides of Little Diomede hiding from weather.

Early on the 16th July (~0630 ship time), we started the final run of the BS line with trace metal/nutrient sampling, although the winds were still strong (from the south). A small easing of the wind allowed us to accomplish the section, and half the stations on the SBSnn line before turning for Nome around 8:30pm ship time.

As in 2019, the transit to Nome was slowed by strong currents (possibly tidal), but the ship made Nome by around 8am, and was able to tie up alongside a barge, over which the science team was able to disembark gear (for Air Cargo). The science team left the ship around 1045am, catching the lunch time flight back to Anchorage and then onto Seattle. The ship left Nome around 1130 to transit to Homer, arriving in Homer on the 25th July.

Other than the missing weak link on the moorings (also missed on A2, though that could not be recovered and replaced), the cruise went exceptionally smoothly. It is remarkable that only one dragging operation was necessary, although this is in part due to the cruise being so early in the year. The 2019 moorings were deployed in September, after the main summer growing season and thus really only had one summer (2020) in which to biofoul. The 2020 mooring recoveries were remarkably clean. After some teething problems, the CTD operations went smoothly, recording 276 casts. The retermination of the cable was something we were prepared for, but not expecting. The first 10 CTD casts were missing the TS ducting on the CTD, causing a mismatch between T and C data. However as these were calibration casts of the deeper layer (where the timing mismatch was not critical) no special processing has been done to correct for this. Due to driver inattention, the CTD touched bottom on cast 222, but without damage or data loss other than on the oxygen upcast. Vent plugs caused the usual problems, though their impact on the data is minimal due to vigilance of the CTD driver and deck crew, to ensure regular and timely cleaning. The trace metal/nutrient pumping, a first for this cruise, went extremely smoothly, collecting data on 41 stations (33 separate locations). Unresolved issues remain with the meteorological data (new system this year), which we suspect may be reading high on wind speeds, and erroneously on temperature. This requires further investigation. Issues with the Aft-GPS date remained unresolved for the cruise - the aft A-frame GPS was repositioned to the aft rail, but CTD and other systems logged instead the forward GPS data which was correct.

Over all, a set of 14 CTD lines were taken, mostly under northward wind conditions, but through various wind strengths. For full station coverage, see map and listings below. Preliminary results are given in the various sections.

Summary of CTD lines.

BS (Bering Strait) (US portion) – the main Bering Strait line, run at the start and at nearly the end of the cruise. This line has been occupied by past Bering Strait mooring cruises. US portion only run here. This line was previously ~ 2nm resolution. On both runnings of this section, we used the more recent station spacing of ~1nm to better resolve the structure in the strait. Previous runnings of this line have included two stations (BS23 and BS24) which fall south of the main line near Prince of Wales, extending the line along (rather than across) isobaths. Neither BS23 and BS24 were taken during this cruise. Pumped samples for trace metals/nutrients were taken on both runnings of this line in 2021.

DLS and DLN (Diomede Line) (previously one line DL) – two consecutive lines running north from the Diomede Islands to A3, the southern portion DLS (stations DL1-12) at 1nm spacing, the northern portion DLN (stations DL13-A3) was previously run at 2.5nm spacing, but on this cruise a station spacing of 1.25nm was used. Run both at the start and end of the cruise, although the second running is complete due to bad weather. These lines study the hypothesized eddying and mixing region north of the islands.

AL (A3 Line) (US portion) – another previously-run line (previously run at ~ 1.7nm resolution, run this cruise once at 0.85nm resolution), just north of the Strait, running from the Russian coast, through the mooring site A3, to where the main channel of the strait shallows on the eastern (US) side. US portion only run here, and extended by 6.6nm to map the transition to shallower water. Run with trace metal/nutrient sampling.

CS (Cape Serdtse) (US portion) – another cross strait line (~ 3.9nm resolution), run here from the US-Russian convention line (~168° 58.7'W) to Point Hope (US), but originally starting at Cape Serdtse-Kamen, in Russian waters. Also repeated during the cruise, both runnings adding stations to make station spacing ~1.9nm. **First running done with trace metal/nutrient sampling.**

NPH (*North Point Hope*) (US waters) - a line run before in 2016, and 2019, crossing from north of Point Hope to the WNW, at 1.25nm spacing near the coast, and 2.5nm spacing after NPH5, to chart the Alaskan Coastal Current transformation on its route along the Alaskan Coast. Extended in 2019 to the Convention Line (CCL). Run twice this cruise. First running westward only to station NPH13, second running (eastward) of complete line from CCL.

CD (Cape Dyer) (US waters) - a line new in 2016, taken also in 2017 and 2019, running west-east towards the Alaskan Coast, midway between Point Hope and Cape Lisburne, set just south of some apparent topographic irregularities, also to chart the Alaskan Coastal Current transformation on its route along the Alaskan Coast. Extended in 2019 to the Convention Line, but run in 2021 only from CD 14 to the coast.

LIS (Cape Lisburne) (US waters) – from Cape Lisburne towards the WNW, a previous RUSALCA line, run by us also in 2011, 2012, 2013, 2014, 2015, 2016, 2017, 2018 and 2019 and close to the CP line occupied in previous Bering Strait cruises in 2003 and 2004 (station spacing ~ 3.6nm). Note that due to the Quintillion cable, station Lis 9 is replaced by 2 new neighboring stations, Lis 8.5 and 9.5. Run once during the 2021 cruise. Run with trace metal/nutrient sampling

Re-run of NPH (this time from CCL to the east), and CS lines

Parts of **CCL** *(Chukchi Convention Line)* (US waters) – a line running down the convention line from the end of the LIS line towards the Diomedes (also run in 2003, 2004, 2011, 2012, 2013, 2014, 2015, 2016, 2017 and 2018), typically incorporating a rerun of the high resolution DL line at the southern end, run variously at 10nm (typical) or 5nm (rarely) resolution. Run only in parts in 2021.

Re-run of BS line with trace metal/nutrient sampling

SBSnn – a previous line new in 2014, run only in 2014, 2015, 2017 and 2019, and then often only in part, just south of the strait, crossing the Alaskan Coastal Current before it enters the strait proper (previously and this year run at 2.2nm resolution, run in 2019 at 1.1nm resolution). This year run with the same alignment (i.e. from BS22 as used since 2019, and thus denoted SBSnn. (Previous SBS line started at BS24).

Summary of ADCP/Underway data lines

The ship's ADCP recorded for the duration of the cruise, and between lines steams were often positioned to give more useful underway information. The following were targeted underway surveys:

After A4 recovery east to shallow waters and then back to A2

After A2 deployment, west to BS11, then NE to NSB10, back west along the NBS line and then N to A3 See maps for details of these lines.

Prior lines not taken on this cruise:

DLa and DLb – two other high resolution lines (1nm resolution), mapping the eddying/mixing region, parallel to DLS, allowing for a 2-dimensional mapping of the region.

AS – a line sampled only once before (2011) (although sometimes run for underway data), running from the eastern end of AL back towards the western end of the CS line, taken at variously 4nm or 2nm spacing (closer stations over steeper topography).

NNBS (North North Bering Strait) – a new line run only three times before (2015, 2017, 2019) west-east across the eastern strait, south of A3 and north of NBS, run at ~ 1.8nm resolution, to better map the Alaskan Coastal Current north of the Strait proper.

NBS (North Bering Strait) – an east-west cross-strait line ~ 8nm north of the Bering Strait line, run in previous years, with ~ 1.7nm resolution.

MBS (*Mid Bering Strait*) — an east-west cross-strait line ~ 10nm north of the Bering Strait line, run in previous years, with ~ 1.7nm resolution, with higher resolution near the coast

CONTENTS

Cruise Map Science Participants and Norseman II Participants Cruise Schedule

Summary of Science Components

Mooring Operations

Table of Mooring Positions and Instrumentation Schematics of Mooring Recoveries and Deployments Photographs of Recovered Moorings Preliminary Mooring Data Figures

CTD Operations

Notes on CTD Processing CTD operation notes CTD lines Preliminary CTD section plots

Water Sampling Operations (Trace Metals, Nutrients and delta O18)

Underway Data (ADCP, Temperature and salinity, Meteorology) Operations Underway Data Preliminary Plots

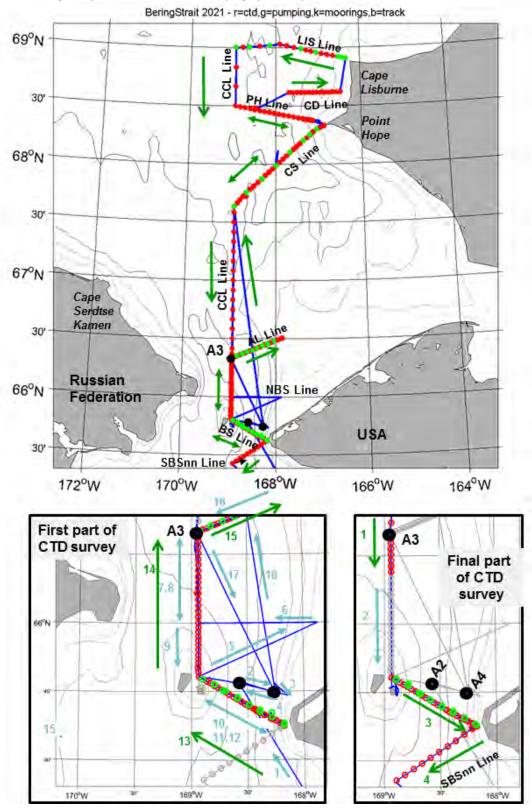
Listing of target CTD positions

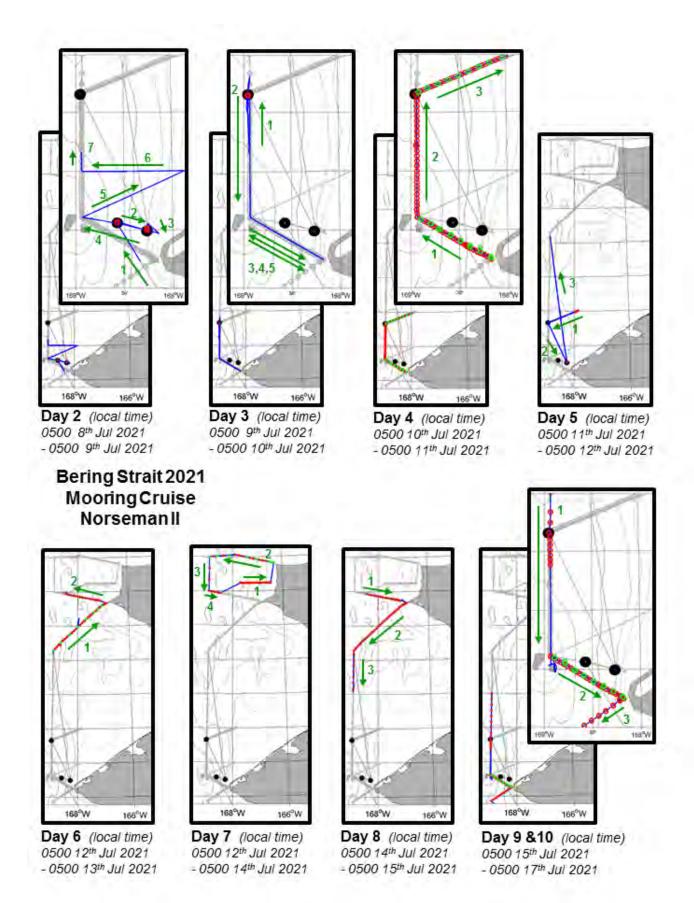
References

Event Log

Full Delta O18 processing results

BERING STRAIT 2021 CRUISE MAP: Ship-track, blue. Mooring sites, black. CTD stations, without (red) and with (green) trace metal/nutrient sampling, Consecutively numbered arrows show direction of travel (on this figure, green marking CTDing lines, cyan marking transit). Depth contours every 10m from IBCAO (International Bathymetric Chart of the Arctic Ocean [Jakobsson et al., 2000]. Lower panels give detail of strait region at the start (left) and end (right) of the cruise. (See next page for daily detail.)





BERING STRAIT 2021 SCIENCE PARTICIPANTS

On Shore:

 Rebecca Woodgate 	UW	Chief Scientist and UW PI
2. Cecilia Peralta-Ferriz	UW	Co-Chief Scientist and UW Co-PI
On board:		
 Jim Johnson (M) 	UW	UW lead and chief mooring technician
John Guthrie (M)	UW	UW research scientist
3. Laramie Jensen (F)	UW	UW postdoc & lead of trace metal/nutrient sampling
4. Katy Christensen (F)	UW	UW graduate student & lead of CTD measurements
Robert Daniels (M)	UW	UW mooring technician

UW - University of Washington, US

Cabin Allocations:

Main deck (Cabin 4) - Jim Johnson Lower deck, starboard aft (Cabin 7) - Laramie Jensen & Katy Christensen Lower deck, port aft (Cabin 8) - John Guthrie Lower deck, starboard forward (Cabin 5) - Robert Daniels

BERING STRAIT 2021 NORSEMAN II CREW

1. Mike Hastings (M)	SVA	Captain
2. Pat Murphy (M)	SVA	Mate
3. Jim Wells (M)	SVA	Boson
4. Dan Hill (M)	SVA	Cook
5. Bryce Walker (M)	SVA	Asst. Cook
6. Kevin Duff (M)	SVA	Engineer
7. Mike Leiffeste (M)	SVA	AB
8. Nathanial Charbonneau (M)	SVA	AB

SVA – Support Vessels of Alaska, Inc. , https://www.supportvesselsofalaska.com

Ship contract arranged by:

CPS Polar Field Services, partner of Battelle ARO Anna Schemper, anna@polarfield.com

BERING STRAIT 2021 CRUISE SCHEDULE (Times: Alaskan Daylight Time (UTC-8), 24hr format)

(Wind directions are wind source .. so S Wind = wind from South)

Mid May 2021 Shipment of container of UW equipment to Homer

Mid June 2021 Loading of gear in Homer

Sat 12th June 2021 UW Science team start period of "Strict Social Distancing" in Seattle

Wed 23rd June 2021 UW Science team do PCR Covid test in Seattle

Sat 26th June 2021 UW Science team fly commercial to Fairbanks

and start 10-day quarantine at Wedgewood Resort, Fairbanks

Tuesday 29th June 2021 Norseman2 leaves Homer (~ 0300UTC)

Wednesday 30th June 2021 Norseman2 at Takli Island

Tests of underway systems during this transit

Thurs 1st July 2021 UW Science team do PCR Covid test in Fairbanks

Friday 2nd July 2021 Norseman2 passes Aleutian Chain east of Unimak Island (1200)

Sunday 4th July 2021 Norseman2 passes S of Nunivak Island (~0735)

Norseman2 passes N of Nunivak Island (~1530)

Monday 5th July2021 Two of UW Science team retest as test results not back

Finally all test results (including duplicates) return negative

Norseman2 passes St Lawrence Island (~1800)

Tuesday 6th July 2021 Norseman2 reaches Nome Harbor (~1800) and then waits outside

Wednesday 7th July 2021 ~ 0800 Norseman2 performs Met system calibration off Nome

~ 1130 returns to Harbor for onload of personnel

UW Science team fly private charter to Nome (~0730-1030), UW science team board Norseman2 in Nome ~ 1130

Safety briefings, Sail ~ 1445

Set up underway, reterminate CTD cable, do test CTD cast.

Thurs 8th July 2021 (*JD 189*) Arrive on site A2 ~ 0630

From 0803 do pre recovery CTDs at A2 0829 Start A2-20 recovery, all on deck 0843

0909 Start, all on deck 0925

Steam to A4

From 1110 do pre recovery CTDs at A4

1217 Start **A4-20 recovery**, all on deck 1231 1257 Start **A4-19 recovery**, all on deck 1310

Start towards A3, then replan as too far for working today

Steam towards Alaskan Coast to map ACC Return towards A2, setting up deployment

1654 Start A2-21 deployment run, drop Anchor 1659

1726 A2-21 post deployment CTD cast

Steam towards DL1, with trace metal/nutrient (TMN) pumping test

Steam underway lines over night (to NBS10, to NBS1, to A3)

Fri 9th July 2021 (*JD 190*)

Arrive on site A3 ~ 0715

From 0811 do pre recovery CTDs at A3

0905 Start **A3-20 recovery**, all on deck 0917 0940 Start **A3-19 recovery**, required dragging, all on deck 1101

Prepare A3-21 deployment

1600 Start A3-21 deployment, drop Anchor 1605

1620 A3-21 post deployment CTD cast

Prepare A2-21 deployment while steaming South overnight

Steam S along DL to DL1, Steam SE along BS to BS22 Steam NW along NS to BS11 Steam SE along BS to BS22

During this transit, discover problem with A3-21 deployment

Sat 10th July 2021 (JD191)

0752 Start CTDing BS line (from BS22 to NW) with TMN pumping

1438 finish BS line at BS11, steam to DL1 1445 Start **CTDing DL line (from DL1 to N)**

2043 finish DL line at DL19.5, steam to A3

2051 Start CTDing AL line (from A3 to NE) with TMN pumping

Sun 11th July 2021 (JD192)

0541 finish AL line at CL27.5, steam to A3 (foggy)

0859 Start A3-21 recovery, all on deck 0914

Prepare A3-21 redeployment

1012 Start A3-21 deployment, drop Anchor 1019

Steam to A4, preparing A4-21 deployment

1517 Start A4-21 deployment, drop Anchor 1518

1529 A4-21 post deployment CTD cast

Steam towards CS10, preparing glider on transit

2121 Stop to **deploy glider** at ~ 66 32.93N, 168 32.72W

2149 Continue on to CS10

Mon 12th July 2021 (JD193)

0526 Start CTDing CS line (CS10US to NW) with TMN pumping

1055 Break off CTDing at CS13 due to bad weather 1625 Restart CTDing at CS13 as weather improves

2223 finish CS line at CS19, steam to NPH1

2312 Start CTDing NPH line (from NPH1 to NW)

Tues 13th July 2021 (JD194)

0444 finish NPH line at NPH13, steam to CD14

0709 Start CTDing CD line (from CD14 to E)

1123 finish CD line at CD1, steam to LIS1

1327 Start CTDing LIS line (LIS1, to NW) with TMN pumping +O18

2242 finish LIS line at CCL22n, steam to CCL21

2242 Continue CTDing CCL line S

Wed 14th July 2021 (JD195) 0301 Start CTDing NPH line (from CCL19 to SE)

1020 finish NPH line at NPH1, steam to CS19

1118 Start CTDing CS line (from CS19 to SW)

2202 finish CS line at CS10.

2202 Continue CTDing CCL/DL line S, including A3

Thurs 15th July 2021 (JD196) 1519 break off DL line at DL16.5 due to bad weather

Make headway south to the Diomedes

2306 arrive near Little Diomede, run arcs around NW side of island

Friday 16th July 2021 (JD197) 0635 Start CTDing BS line (from BS11 to SE) with TMN pumping

1424 finish BS line at BS22

1424 Continue CTDing SBSnn line (from BS11 to SW), halves only

2027 finish SBSnn line at SBSnn10.5

2027 Turn for Nome

Sat 17th July 2021 (JD198) ~0800 Tie up in Nome alongside barge, send CTD to AirCargo

1045 UW Science party leave ship.

1130 Norseman2 leaves Nome for Homer 1255 UW Science party fly from Nome,

arriving back in Seattle ~2100PDT

Sunday 25th July 2021 ~0620 Norseman2 docks in Homer.

Bering Strait 2021 Mooring cruise TOTALS

9.75 days at sea (away from Nome)1445 7th July - 0800 17th July 2021 **10 days on ship (including on/offload)**1130 7th July - 1045 17th July 2021

Moorings recovered:

Moorings deployed: 3

CTD casts: 276 (including 1 test cast) on 14 lines

Trace metal/nutrient Pumping stations: 41

Gliders deployed: 1

SCIENCE COMPONENTS OF CRUISE

The cruise comprised of the following science components:

- Mooring operations 6 mooring recoveries, 3 mooring deployments (UW moorings)
- **CTD operations** 276 casts on 14 lines (UW instrumentation, measuring temperature, conductivity, oxygen, fluorescence, and turbidity with pressure)
 - Water sampling for trace metals/nutrients 41 stations where samples taken with pumped system.
 - Opportunistic O18 sampling 2 samples taken at start of LIS line due to remarkably fresh waters.
- **Underway sampling** ship-based equipment of 300kHz hull-mounted ADCP; SBE21 underway Temperature-Salinity recorder, an SBE38 temperature sensor, and some meteorological data (air temperature, pressure, humidity, wind direction and wind speed).
 - Moored Marine Mammal Observations (acoustic instruments on the moorings)

All recovered A3 moorings and the deployed A3 mooring carried Marine Mammal Acoustic Recorders from Kate Stafford, UW.

- Marine Mammal Glider Deployment - one glider was deployed for PIs: Hank Statscewich and Seth Danielson (UAF), Kate Stafford (UW) and Mark Baumgartner (WHOI) as part of a project monitoring marine mammal calls in the western Chukchi.

http://dcs.whoi.edu/chukchi0721/chukchi0721 unit 595 html/chukchi0721 unit 595 summary.html

MOORING OPERATIONS (Johnson, assisted by others)

Background: The moorings serviced on this cruise are part of a multi-year time-series (started in 1990) of measurements of the flow through the Bering Strait. This flow acts as a drain for the Bering Sea shelf, dominates the Chukchi Sea, influences the Arctic Ocean, and can be traced across the Arctic Ocean to the Fram Strait and beyond. The long-term monitoring of the inflow into the Arctic Ocean via the Bering Strait is important for understanding climatic change both locally and in the Arctic. Data from 2001 to 2018 suggest that heat and freshwater fluxes are increasing through the strait [Woodgate et al., 2006; Woodgate et al., 2010; Woodgate et al., 2015; Woodgate, 2018; Woodgate and Peralta-Ferriz, 2021], with 2012 being a year of low flow, but 2013 to 2016 returning to higher flow conditions [Woodgate, 2015; Woodgate et al., 2015; Woodgate, 2018]. The data recovered this cruise will indicate if recent years show further increase or a return to older conditions.

An overview of the Bering Strait mooring work (including data access) is available at http://psc.apl.washington.edu/BeringStrait.html. Data are also permanently archived at the National Oceanographic Data Center, now renamed the National Centers for Environmental Information (https://www.nodc.noaa.gov/ or https://ncei.noaa.gov).

A map of mooring stations is given above. Six UW moorings were recovered on this cruise. These moorings (all in US waters – A2-19, A4-19, A3-19, and A2-20, A4-20, A3-20) were deployed from the Norseman II in September 2019 and 2020 respectively, with mooring funding from NSF-AON (PIs: Woodgate and Peralta-Ferriz, *PLR1758565*). Due to the Covid situation, the 2020 cruise sailed without a science party and thus no moorings were recovered that year.

Three UW moorings (A3-21, A2-21, A4-21) were deployed on this 2021 Norseman II cruise under funding from the same NSF-AON grant. All these deployments were replacements of recovered moorings at sites occupied since at least 2001 (A4) or 1990 (A2 and A3). Analysis of past data suggests data from these three moorings are sufficient to give reasonable estimates of the physical fluxes of volume, heat and freshwater through the strait, as well as a useful measure of the spread of water properties (temperature and salinity) in the whole strait [Woodgate et al., 2015].

All moorings (recovered and deployed) carried upward-looking ADCPs (measuring water velocity in 2m bins up to the surface, ice motion, and medium quality ice-thickness); lower-level temperature-salinity sensors; and the 2019 and 2021 moorings also carried iscats (upper level temperature-salinity-pressure sensors in a trawl resistant housing designed to survive impact by ice keels). All recovered and deployed moorings also carried marine mammal acoustic recorders. The A3-19 and A3-21 moorings also carried the first prototypes of the "Miscat", a multiple instrument version of the iscat, designed to allow instruments to be lost sequentially from nearer the surface. For a full instrument listing, see the table below.

This coverage should allow us to assess year-round stratification in and fluxes through the strait, including the contribution of the Alaskan Coastal Current, a warm, fresh current present seasonally in the eastern channel, and known to be a major part of the heat and freshwater fluxes [Woodgate and Aagaard, 2005; Woodgate et al., 2006; Woodgate et al., 2015; Woodgate, 2018]. The ADCPs (which give an estimate of ice thickness and ice motion) allow the quantification of the movement of ice through the strait [Travers, 2012]. The marine mammal recording time-series measurements should advance our understanding of the biological systems in the region.

Calibration Casts: Biofouling of instrumentation has been an on-going problem in the Bering Strait. Prior to each mooring recovery, a CTD cast was taken to allow for *in situ* comparison with mooring data. Similarly, CTD casts were taken at each mooring site immediately after deployment. These post-deployment casts will allow us to assess how effective this process is for pre-recovery calibration. Since the strait changes rapidly, and CTD casts are by necessity some 200m away from the mooring and may be as long as 1hr separated in time from the mooring reading, it is inevitable that there will be differences between the water measured by the cast and that measured by the mooring. **Action item: On recovery, check the post deployment casts to see how reliable the comparison is.**

This year (as in 2017 and 2018 and 2019), an on-deck calibration tank was also used for recovered instruments. This is discussed below.

2021 Recoveries and Deployments: Given that 3 moorings had been in the water for almost 2 years, mooring recoveries were exceptionally smooth this year, with only one of the moorings requiring dragging.

For recoveries, the ship positioned ~ 200m away from the mooring so as to drift towards the mooring site. Ranging was done from the port mid corner of the aft deck of the ship, with the hydrophone connecting to the deck box inside at the aft end of the port laboratory. Action item: Re check position as regards to ship's propellers. Once the ship had drifted over the mooring and the acoustic ranges had increased to >70m, the mooring was released. This procedure was followed to prevent the mooring being released too close (or underneath) the ship since in previous years the moorings have taken up to 15min to release. Action item: Be sure to distinguish between slant and horizontal range during soundings. As site A3 is ~0.6nm from the Russian border, prior to ranging on A3, the Norseman II's small boat was prepared for launching, to cover the eventuality that if the mooring had to be dragged, the mooring would surface and drift towards Russian waters before the ship was able to recover it. Action item: Continue to prepare for small boat operations at site A3.

On all moorings, we use double releases, with springs to assist the mooring release. For the all moorings, although our usual routine is to communicate and range with one release and then attempt to release the other release (to test both instruments), this year the same release was used for ranging and for release. This was successful at bringing the mooring to the surface on all moorings except for A3-19.

On A3-19, although both releases were activated (and confirmed release) the mooring did not surface, but ranges increases as the ship drifted away indicating the mooring was still connected to the anchor. Thus a dragging operation was initiated. Within ~ 30min of dragging the mooring was sighted on the surface, and the drag snagged an anchor, which was brought on board before the mooring could be recovered. On recovery, both releases were found to have released. Biofouling was present on the releases, and it is very possible that an unfortunately placed barnacle was the cause of holding the mooring down. Action items: Investigate better biofouling paint. Ensure all releases are newly painted each year. Continue to use external springs

In all cases, once the mooring was on the surface, the ship repositioned, bringing the mooring tightly down the starboard side of the ship. One boat hook and a pole with a quick releasing hook attached to a line were used to catch the mooring, typically on a pear link fastened to the chain between the float and the ADCP or on eyes welded to the float surface. The line from the hook was then passed back to through the stern A-frame, and tied with a "cat's paw" knot to a hook from the A-frame. This portion of the mooring was then elevated, allowing the second A-frame hook to be attached lower down the mooring chain, and tag lines to be attached if necessary. The iscat, if present, was recovered by hand at a convenient point in this operation, prior to recovery of most of the mooring. (This year, of the 4 iscat instruments that might have been present (only on the Ax19 moorings), the iscat was recovered only from A4-19.) Then the entire mooring was then elevated, using both hooks from the aft A-frame, and recovered onto deck. Recovery work was done by a deck team of 4 crew of the Norseman II – one on the A-frame controls, three on deck with on overhead safety lines ("dog runs") down each side of the deck (one of these working forward of the deck on tag lines), assisted by UW personnel further forward on the aft deck. Once on deck, the moorings were photographed to record biofouling and other issues. Action items: Be sure to add pear-link to the chain between float and ADCP. Prepare loops of line for threading through chain/shackles to provide a lifting point. High A-frame or crane very helpful for recovery. Also helpful to review mooring movies at start of cruise.

The A-frame of the Norseman II is atypically high (~ 26ft less block attachments). While this is extremely useful in fair weather, it allows for swinging of the load in rougher seas. Action item: Continue to use tag line options for recovery in rougher weather.

Good visibility (at least ~1nm) is required for mooring recoveries since the mooring may delay releasing due to biofouling, or the mooring may require dragging, as in previous years. Given the proximity of A3 to the US-Russian border, small boat operations may also be necessary during a dragging operation to prevent the

surfaced mooring drifting out of US waters. For these reasons, it was decided typically not to commence a new mooring operation after 5pm local time. Action item: Continue to include weather days in the cruise plan; plan also for small boat operations (including sending a battery powered release unit), considering especially if small boat operations could be used in fog. Assess causes of foggy conditions, in order to predict best strategy for finding workable visibility.

Biofouling was heavy in the recoveries of the 2019 moorings, but light on the 2020 moorings. On A2-19 and A4-19 the ADCP heads were entirely covered with barnacles, and the A3-19 ADCP was almost entirely covered with barnacles. Salinity cells were only just clear on the Ax19 moorings. Bryozoan growth was limited - instead barnacles were plentiful. The releases had some biofouling, but significantly less than on the rest of the moorings.

In contrast to 2016, when significant damage (hypothesized ice damage) was found on the moorings, this year there was no clear evidence of mechanical damage to the mooring frames in general, although the protective case on the hydrophone of the A3--20 mooring was twisted off. Luckily the hydrophone itself appeared undamaged. It is unclear when this damage occurred. As A3-20 was recovered prior to the dragging operation on A3-19, it was not due to the dragging operation. The only other damage was the loss of the Iscats on A3-19 and A2-19. On A2-19 much (all?) of the iscat tether was recovered, suggesting the tether parted at the block below the iscat itself (though the block was not recovered).

Mooring deployments were done through the aft A-frame, using the A-frame hooks for lifting. The height of the Norseman II A-frame was extremely advantageous for these deployments. Lacking such an A-frame, alternative ships might consider lifting the mooring with the crane, rather than the A-frame. The mooring was assembled completely within the A-frame. The ship positioned to steam slowly (~1 to 2knots) into the wind/current, starting between 500m and 600m from the mooring site. Action item: This distance (greater distance in strong current) works well. At the start of the deployment, the iscat was deployed by hand and allowed to stream behind the boat, which steamed at ~ 2knots, fast enough to maintain headway and to trail the mooring behind the ship, but not so fast as to damage the equipment being towed or pull equipment off the deck. Action item: Feed the iscat tether unwound to the person spooling it off the deck. The first pick (from one of the hooks of the aft A-frame) was positioned below the ADCP, except in the case of A4, where the first pick was below the top float. The second pick (from the other hook of the aft A-frame) was lower down on the mooring allowing all the mooring except the anchor to come off the deck during the lift. Then, the A-frame boomed out to lower these instruments into the water. Tag lines were used to control the instruments in the air. Action item: use deck cleats to fair tag lines. Be sure to position the lift point on the float so it does not cause the float to roll off. The first pick was released by a mechanical quick release, which was then repositioned to lift the anchor. (Previous years have shown that if the first pick was insufficiently high, the releases would still be on deck when the first package was in the water. The releases would then slip off the deck inelegantly. It was found that a higher lift of the instruments, and using both hooks of the A-frame, allowed the releases also to be lifted from the deck and then hang nicely behind the ship once the ADCP was placed in the water.) The anchor was lifted into the water just prior to arriving at the site. Positioning of this final pick very close to the anchor prevents the releases being pulled back over the lip of the ship when the anchor is lifted. Action item: Make final pick as close as possible to the anchor. When the ship arrived on site, the anchor was dropped using the mechanical guick release. Positions were taken from a hand-held GPS on the upper aft deck, some 5m from the drop point of the mooring. Action item: Continue to bring own GPS unit. Note that due to mooring fall back, actual mooring position may be ~ 10m from this position in the opposite direction to the steaming **direction during recovery.** This information is noted on the mooring diagrams.

A team of 4-5 crew did the deployments, with one person on the A-frame, 3 on the "dog runs' assisting the instruments up into the air, and other members of the crew/science team assisting with tending the tag lines during lifting.

Action items: design pick points into the moorings for recover; continue to put 2 rings on the anchors for tag lines. Consider using chain, not line for the moorings (saves on splicing and gives extra pick points);

Compute the best pick point, such that the releases are lifted free of the deck, rather than slipped over the edge.

After the deployment of A2-21 and A3-21, it was discovered that the weak link had been omitted from the iscat systems. Without the weak link, the mooring might be dragged by ice. As A3 is near the EEZ line, this was deemed to be too great a risk, and the decision was taken to use the anchor we had recovered during dragging to redeploy A3-21 after a recovery. Thus the deployment of A4-21 was postponed (in case unexpected snags were encountered and equipment from that mooring was needed to complete the new A3-21) and CTD lines were run until the weather and light were possible for mooring recovery. Despite initial fog, the recovery and redeployment of A3-21 (with the weak link installed) went smoothly, and subsequently A4-21 was also safely deployed. This leaves A2-21 deployed without weak link. Typically, iscats are only lost from the moorings in ~ half of the deployments. Thus there is at least a 50% chance the mooring will not be snagged enough to drag it. Action item: On recoveries in 2022 be aware that A2-21 may have moved position, and survey in the position before attempting recovery.

Deployment Instrumentation issues: This year, because the cruise was only loading people in Nome, instrumentation was again started in Seattle and shipped to Homer set on delayed start. All instrument starts went smoothly, although it was discovered the SBE37IM would not accept a delayed start longer than 30 days ahead.

Iscat housings and tethers were assembled in Seattle, and ADCPs incorporated into the ADCP frames, leaving the only assembly work to be done at sea the placing of the floats on the ADCP frames and the testing of the releases. Action item: Consider in future if starting instruments in Seattle is a safe way of saving time in Nome. Note that releases could also be deck checked ashore to save time at sea.

Recovered Data and Instrumentation issues: Data recovery on the moorings was generally good, although with some challenges, as detailed below:

- ISCAT SBE37IMS AND LOGGERS: Of the 3 iscats/miscat deployed on the recovered moorings:
- from **A2-19**, the top SBE37 sensor was not recovered, but the logger recorded data until 13th May 2020 and continued to write files until 24th Jan 2021. On recovery the logger battery was dead. This is as expected from an iscat that has been dragged off the mooring.
- from **A4-19**, the top SBE37 sensor was recovered (the cell was only just clear) and the SBE37 ran until recovery. The logger however had recorded no data. Its clock was still correct and battery voltage was still high. **Action item: Investigate**
- from **A3-19**, the MISCAT system was not recovered. Both sensors were missing, but the logger returned some data on recovery from deployment (7th Sept) to 11th Sept for the lower (~ 16m) sensor and longer to 15th Sept for the upper (~8m) sensor, although with increasing numbers of data gaps. Again the logger battery was dead, as expected once the SBE37IMs are lost. **Action item: Investigate, and run a wet test in Seattle.** Preliminary results (before any correction for biofouling or post cruise calibration) are plotted below.
- ADCPs: Of the 6 ADCPs deployed on the recovered moorings, all were running on recovery and gave complete data records, including the 2 year deployments. These instruments were deployed with lithium batteries (and no external battery pack) and a conservative recording schedule and were expected to last the two years. The ice track records have not yet been investigated. Action item: Check the sea ice data. : Preliminary results are plotted below.
- SBEs: A SBE16 was recovered from each mooring. None of these instruments were pumped. All instruments were running on recovery and returned full data records with only minor problems, viz. spikes in 2341 on A2-19, and 1700 on A4-19 appears to have lost one data record sometime during the 2 year deployment. Action items: Despike and investigate the instrument header to check the apparent missing record.

Biofouling was extreme on the moorings that had been out for two years, and thus we expect significant salinity drift over the deployment, as is evident in the mismatch of freezing temperatures during the second winter (see plots below). The test tank is designed to elucidate the size of this drift, in conjunction with post deployment calibration. Action item: Investigate drift. Check 0004, which appears to have gone from good agreement in the test tank to poor (0.3psu) agreement.

Preliminary results (before any correction for biofouling or post cruise calibration) are plotted below.

Post recovery tank calibrations: As an addition calibration test, uncleaned post-recovery SBE instruments were placed, for various periods between 8th July 2021 (1715GMT) and 11th Sept July 2021 (~0250GMT) in a large-plastic bin filled with salt water in conjunction with three recently calibrated SBE instruments:

- SBE19 #924, borrowed from the APL equipment pool and last calibrated in Jan/Feb 2018
- SBE16 # 0005, brought as a mooring spare and last calibrated in February 2020
- SB37IM #22408, brought as a mooring spare and last calibrated in September 2020

The intent was to ascertain to what extent cleaning after recovery changes the readings on the SBE instruments. The preliminary test with this system was in 2016, and had significant limitations, likely relating to the instruments being horizontal, trapping air bubbles or biofouling, or coming out of the water on the rolling ship, or possibly due to interactions between instruments. This year, as in 2017 and 2018 and 2019, the tank was designed to a) allow all instruments to be vertical and b) to include a pump to circulate water within the tank.

Once instruments were recovered from the moorings, they were placed in the tank for various periods of several hours, such as to obtain at least 6 readings. Since recovered instrumentation was recording either hourly (SBE16s) or every 5min (SBE37), this allows a good comparison with the calibration CTD, set at 5 second data, and the SBE37 recording every 5min. Instruments were then cleaned and placed again in the tank for at least another 6 readings. Note that at one point the water circulation pump in the test tank was found not to be working. It is unclear how long it was out of action. As the tank was not big enough for all instrumentation at one time, instruments were swapped in and out, and when not in the calibration tank or being cleaned, they were typically placed in a second "holding" tank so the cells did not dry out. The instruments will next be returned to the manufacturer for post cruise calibration.

Overall the methodology worked smoothly in 2021, although we found the SBE19 was consuming batteries at a much faster rate than expected, i.e., 7.75hrs for the first set of batteries, and 20hrs for the second.

Action item: Keep CTD upright. Do test before and after cleaning. Use both mooring spares. Track CTD time (only ~ 28hrs per battery set). Check CTD pump is working.

Preliminary results are shown below, relative to the SBE19 reference CTD. (At the time of writing, the records from the spare mooring instruments are not available for comparison, but these will be added to this document when it is updated with the post cruise calibrations.) **Action item: Add spare data** These records present some curious features:

- 1) The first soak of the 2020 SBEs show uniform agreement with the calibration CTD, as do most of the second soaks. However A420SBE becomes 0.3psu fresher than the calibration CTD after cleaning. **Action item:** Investigate SBE16, SN0004.
- 2) The first soaks of the 2019 SBEs show uniform freshness of 0.1-0.2psu compared to the calibration CTD. This is in line with previous results.

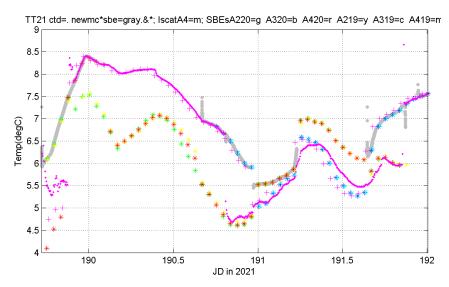
However, it is slightly concerning that

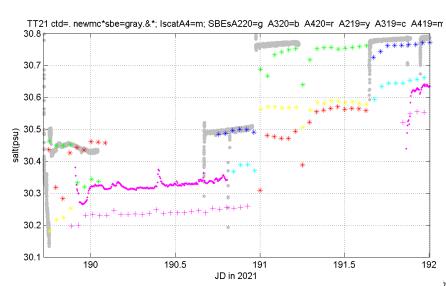
- a) cleaning does not improve agreement, but indeed in some cases, makes agreement worse.
- b) an initially good agreement (A420) can become 0.3psu off during a subsequent soak. The latter point shows the importance of including the other spare instruments in this analysis and considering all the points of evidence (e.g., agreement with in the water CTD casts and subsequent mooring deployments) before concluding a record is erroneously fresh.

Summary of comparisons to SBE924 (grey in plots below, accuracy 0.01°C, 0.001S/m, 0.05psu)

What	A2-19SBE	A3-19SBE	A4-19SBE	A4-19ISC	A2-20SBE	A3-20SBE	A420SBE
	yellow	cyan	magenta	magenta	green	blue	red
SN	2341	1698	1700	20935	1226	1225	0004
TAcc	0.01°C	0.01°C	0.01°C	0.002°C	0.01°C	0.01°C	0.01°C
CAcc	0.001S/m	0.001S/m	0.001S/m	0.0003S/m	0.001S/m	0.001S/m	0.001S/m
SAcc	0.05psu	0.05psu	0.05psu	0.008psu	0.05psu	0.05psu	0.05psu
PRECAL	Mar2019	Mar2019	Mar2019	Jun2019	Jan2004	Sep2009	Sep2008
First Soak	-0.2psu,	-0.1psu	-0.23psu	-0.15psu	~0.0psu	~0.0psu	~0.0psu
Second Soak	-0.2psu	-0.13psu	-0.22psu	-0.15psu	-0.02psu	-0.02psu	-0.3psu
POSTCAL							
First soak							
Second soak							

(Acc = manufacturer's accuracy for temperature (T), conductivity (C) and thus computed salinity (S))





This plot shows all the recovered instruments and the calibration CTD, colors as per the table above.

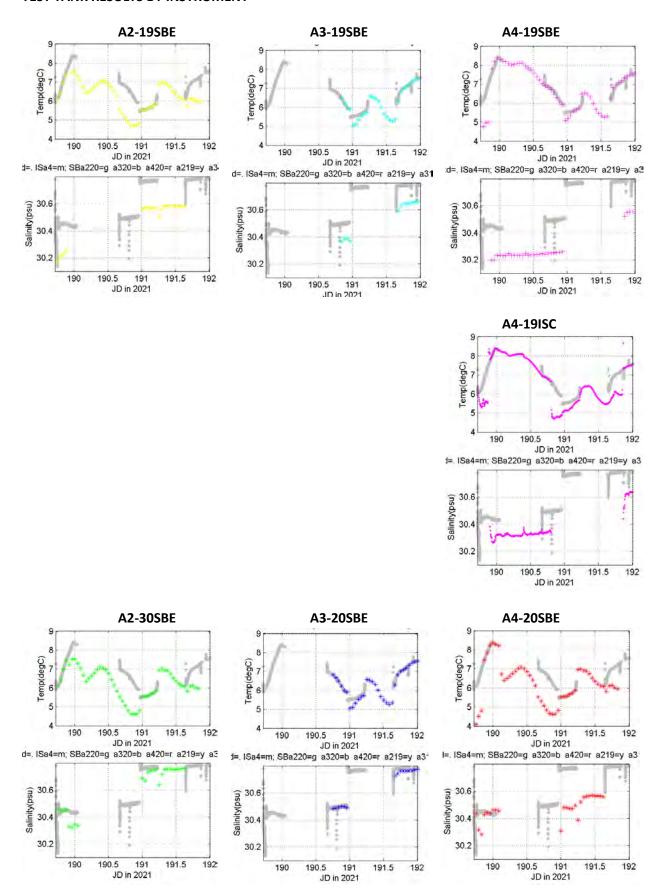
The plots below are 1 per instrument, as per colors in the table above, with grey being the CTD reference. For each plot, use the temperature record to find when the instrument was in the tank with the reference, and then compare the salinity records to find the approximate offset.

. Action item: - return to this once SBEs have been post-cruise calibrated and spare records are available. Revisit test methodology in Seattle to improve reliability. Note that washing can change calibration by 0.1psu. and either the tank may be in error by 0.3pu, or there is some issue with SBE#0004.

Action item: Once all SBEs have been post-cruise calibrated, also do:

- comparison to CTD casts
- comparison to instruments on same moorings

TEST TANK RESULTS BY INSTRUMENT



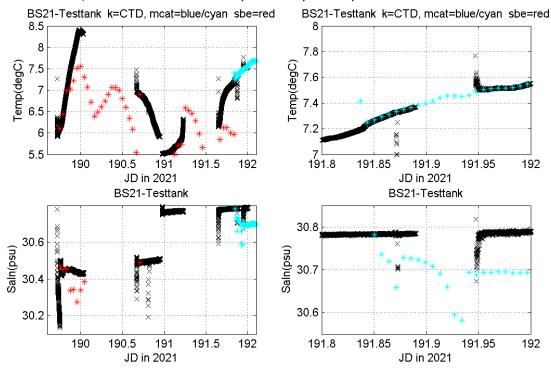
<u>Update May 2022 - checking for salinity calibrations in all moored instrumentation.</u> Discard 2nd Soak in test tank for being unreliable. All unmarked units are PSU

2019	A219sbe	A219isc	A319sbe	A319isc	A419sbe	A419iscat
	2341		1698		1700	20935
Notes	replatinized		replatinized		replatinized	replatinized
SAcc	0.05psu	0.008psu	0.05psu	0.008psu	0.05psu	0.008psu
1) PRE						
Tank - S1	-0.22 psu		-0.1psu		-0.2 psu	-0.1psu
- S2 to CTD	-0.2 psu		-0.13psu		-0.25psu	-0.15psu
- S2 to MC	NA		-0.035 psu or		-0.14 psu	-0.06psu
Rec CTD	-0.23,-0.25		-0.18,-0.18		Unclear	-0.14
Next Year	-0.08psu		-0.05		-0.15	NA
ISCAT/SBE	Too short		Too short		Too fresh	Too salty
Other moor	Unclear		Unclear		Unclear	Unclear
TFreeze	Yr1ok,Yr2TooF		Yr1ok,Yr2TooF		Yr1ok,Yr2TooF	tooF 2 nd yr
2)PPP	0.0941psu		0.3346psu		0.1663psu	0.1072psu
Tank- S1	-0.12psu		+0.2psu		-0.04psu	0.0psu
- S2 to CTD	-0.1psu		+0.28 psu		-0.08psu	-0.05psu
- S2 to MC			+0.2psu		+0.02psu	+0.05psu
Rec CTD	-0.14, -0.16		+0.15,+0.15		unclear	-0.04
Next yr	-0.02psu		+>0.15		-0.08psu	NA
Iscat/SBE	Too short		Too short		ok	ok
Other moor	Unclear		Unclear		Unclear	Unclear
Tfreeze	Ok		tooS 2 nd yr		tooF 2 nd yr	tooF 2 nd yr
CONCLUDE	Use POST cal		PostCal is off		Use POST cal	Use POST cal
	-0.02psu by yr1		Use Precal		-0.04 to -0.08	Tfreeze suggests Yr2
	-0.1 psu by yr2		-0,05psu by yr1		psu off	~0.1fresh, but this not
			-0.1psu by yr2			found in test tank

2020	A220sbe	A220iscat	A320sbe	A320iscat	A420sbe	A420iscat
	1226	None	1225	None	0004	None
Notes	Not replat.		Not replat		Too old to cal.	
SAcc	0.05psu	0.008psu	0.05psu	0.008psu	0.05psu	0.008psu
1) PRE						
Tank - S1	0 psu		0 psu		0 psu	
- S2 to CTD	-0.02psu		-0.01		-0.28	
- S2 to MC			+0.08			
Rec CTD	-0.006		0.001,0.005		Not clear	
Next Year	NA		NA		NA	
ISCAT/SBE	NA		NA		Is ok	
Other moor	Not clear		Not clear		Not clear	
TFreeze	TooF perhaps		ok		ok	
2)PPP	-0.0166psu		0.0075psu		NOT CALED	
Tank- S1	0 psu		0 psu		NOT CALED	
Rec CTD	-0.019		0.007, 0.013			
Next yr	NA		NA		NA	
Iscat/SBE	NA		NA		NA	
Other moor	Not clear		Not clear			
Tfreeze	Better		ok			
CONCLUDE	Use postcal, as		Use postcal, to		Use precal, as that is all	
	Tfreeze better,		match previous		we have, but agrees well	
	likely all better		methods. All better		on all tests, so likely ok,	
	than 0.02psu		than errors 0.02psu		better 0.01psu	

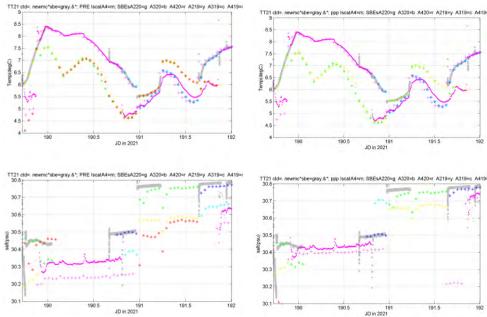
FINDINGS:

First check is of all the references in the test tank - the CTD 924, and then two newly calibrated instruments, SBE16-0005 and SBE37(Microcat) 22408)



** This suggests some issues with the test tank towards the end. So put all references on next the plots.

Next look at the entire set (left Pres, right postcals (ppp))



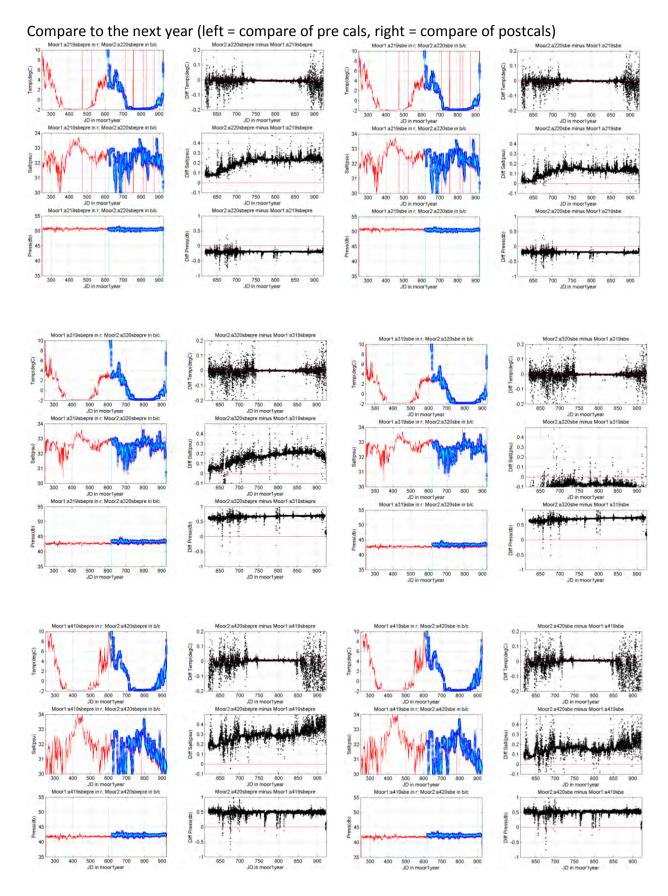
- Postcals generally improve the agreement, other than 1319#1698 where postcal is 0.2 saltier than initial soak.
- 0004 (A4-20) is missing from plots as Seabird did not calibrate it
- second soak appears problematic, with generally worse agreement to first soak.

Now by instrument, looking at pre and ppp. (larger symbols are ppp, A420 no ppp). **A2-19SBE A3-19SBE A4-19SBE** Temp(degC) Temp(degC) 190.5 191 191.5 190 190,5 191 191.5 192 190 190.5 191 191.5 192 JD in 2021 JD in 2021 JD in 2021 e ppp2x ISa4=m; SBa220=g a320=b a420=r a219=y a3 re ppp2x ISa4=m; SBa220=g a320=b a420=r a219=y a ppp2x ISa4=m; SBa220=g a320=b a420=r a219=y 30.6 30.6 Salinity(psu) Salinity(psn) Salinity(psu) 30.8 30.4 30. 30.6 30.2 30.2 30.4).5 191 JD in 2021 191.5 190 190.5 192 190 190.5 191 191.5 192 190 190.5 191 191.5 192 JD in 2021 JD in 2021 A4-19ISCAT 190 190.5 191 191.5 JD in 2021 : pre ISa4=m; SBa220=g a320=b a420=r a219=y a3-30.6 Salinity(psu) 30. 30.2 190 190.5 191 191.5 192 JD in 2021 A4-20SBE A2-30SBE A3-20SBE 8 Temp(degC) Temp(degC) Temp(degC) 5 190 190.5 191 191.5 190 190.5 191 191.5 190 190.5 191.5 191 192 JD in 2021 JD in 2021 JD in 2021 pre ISa4=m; SBa220=g a320=b a420=r a219=y a 'e ppp2x ISa4=m; SBa220=g a320=b a420=r a215 e ppp2x ISa4=m; SBa220=g a320=b a420=r a219= (nsd)/(lull)/(nsd)/(lull)/(nsd)/(lull)/(nsd)/(lull)/(nsd)/(lull)/(nsd)/((30.6) (30.4) (30.4) 30.6 Salinity(psu) 30.4 30.2 30.2 30.2 190 190.5 191 191.5 192 190 190.5 191 191.5 192 190 190.5 191 191.5 192

JD in 2021

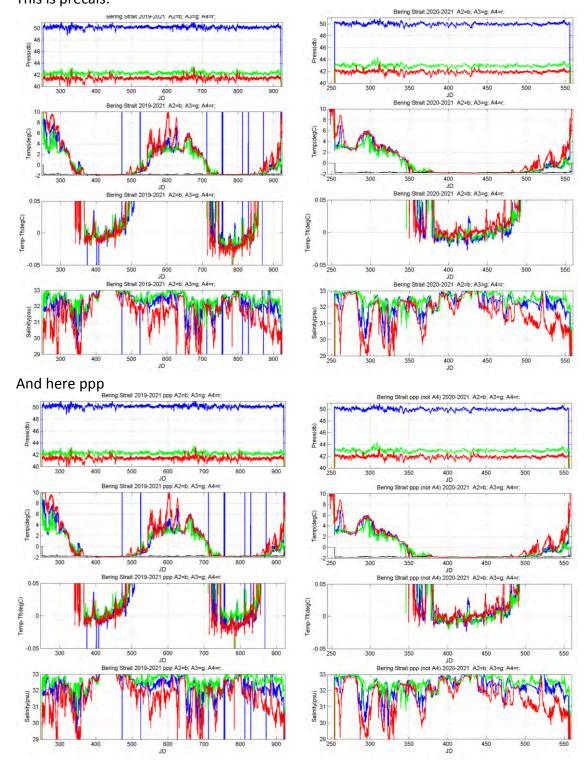
JD in 2021

JD in 2021



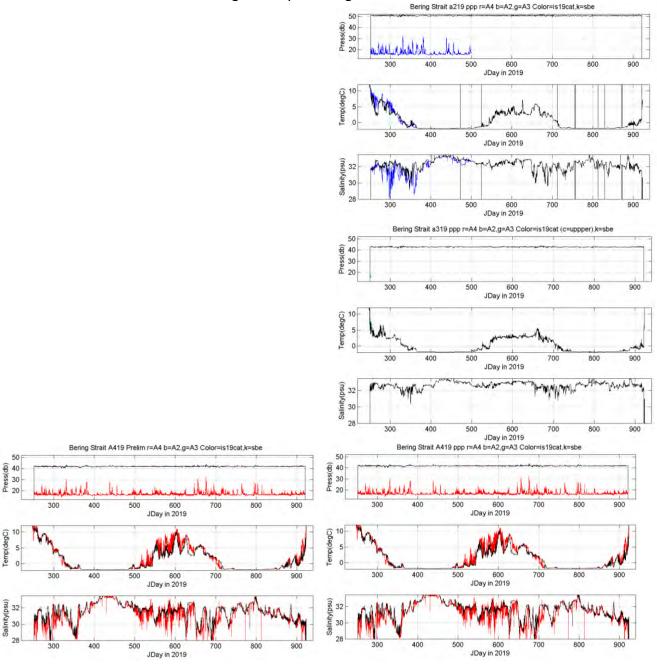
See table for conclusions

Compare freezing points in winter: This is precals:

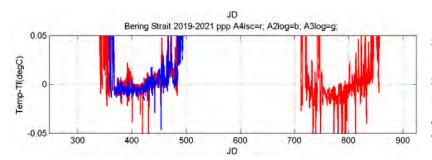


For first winter Ax19s seem ok, but by second winter freezing point is depressed too much.

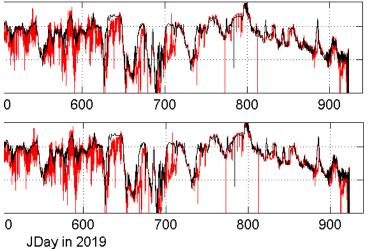
Now look at ISCATS and SBE data together by mooring:



Only A4 has iscat long enough to be useful.



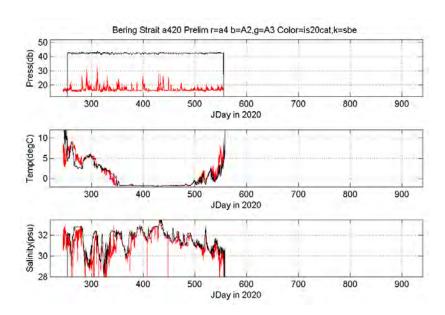
Note that ISCAT winter temperatures suggest year1 salinities ae reasonable, but that A4-19isc salinities may be somewhat too fresh.
(0.005degC equivalent to 0.1 psu), Although this is not found in the test tank results



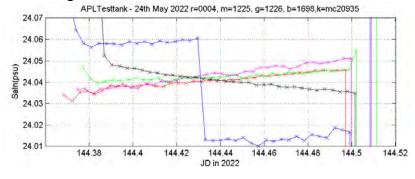
Precal is incorrectly stratified

.. postcal is better.

And then A419isc to compare to A420SBE (only precal)



As missing postcal on A4-20 (#0004) check in Seattle against newly calibrated instruments (May 2022) and find agreement within errors.



Other Recovered/Deployed Instrumentation: Other instruments on the moorings were recovered/deployed for other groups. These instruments are:

Recoveries: Aural Marine Mammal Acoustic sensors on both A3 were deployed by Kate Stafford, (UW). This instruments were cleaned and data storage returned to Seattle for analysis. Preliminary analysis suggests the instrument recorded throughout the mooring deployments.

Deployment: *Marine Mammal Acoustic* only 1 sensor (placed on A3) was deployed this year. This instrument is deployed for Kate Stafford, UW.

Details of mooring positions and instrumentation are given below, along with schematics of the moorings, photos of the mooring fouling, and preliminary plots of the data as available.

BERING STRAIT 2021 MOORING POSITIONS AND INSTRUMENTATION

ID	LATITUDE (N) (WGS-84)	LONGITUDE (W) (WGS-84)	WATER DEPTH /m (corrected)	INST.
		2019 Mooring	Recoveries	
		2023 1110011118		
A2-19	65 46.855	168 34.070	56	ISCAT, ADCP,
				SBE16
A4-19	65 44.748	168 15.765	48	ISCAT, ADCP,
				SBE16
A3-19	66 19.604	168 57.046	57	MISCAT, ADCP with SBE16,
				MMR

ID	LATITUDE (N) (WGS-84)	LONGITUDE (W) (WGS-84)	WATER DEPTH /m (corrected)	INST.
		2020 Mooring	Recoveries	
A2-20	65 46.86	168 34.60	56	ADCP, SBE16
A4-20	65 44.75	168 16.31	49	ADCP, SBE16
A3-20	66 19.60	168 57.60	59	ADCP with SBE16, MMR

ID	LATITUDE (N) (WGS-84)	LONGITUDE (W) (WGS-84)	WATER DEPTH /m (corrected)	INST.
		2021 Mooring D	anloyments	
		2021 WI001111g D	epioyments	
A2-21	65 46.849	168 34.089	57	ISCAT, ADCP, SBE16
A4-21	65 44.737	168 15.767	50	ISCAT, ADCP, SBE16
A3-21	66 19.636	168 56.993	59	MISCAT, ADCP with SBE16, new MMR

ADCP = RDI Acoustic Doppler Current Profiler

ISCAT = near-surface Seabird TS sensor in trawl resistant housing, with near-bottom data logger

MISCAT = ISCAT with two near-surface sensors (one at ~ 8m, one at ~ 16m)

SBE16 = Seabird CTD recorder, SBE37 = Seabird CTD recorder

MMR=Marine Mammal Recorder (new=new APL version)

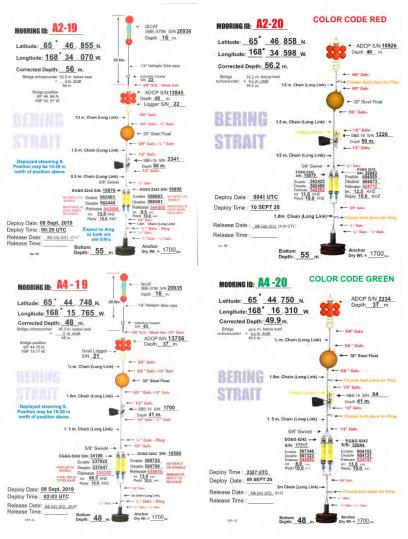
For 2019 deployments, water depths are assuming a ship's draft of 3m.

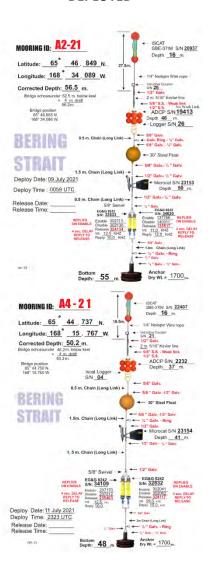
For 2020 and 2021 deployments, water depths are assuming a ship's draft of 4m.

BERING STRAIT 2021 SCHEMATICS OF MOORING RECOVERIES AND DEPLOYMENTS

RECOVERED = in the eastern channel of the Bering Strait

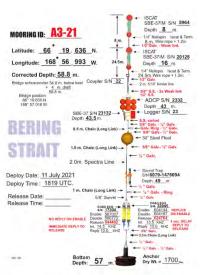
DEPLOYED





= at the climate site, ~ 60km north of the Strait

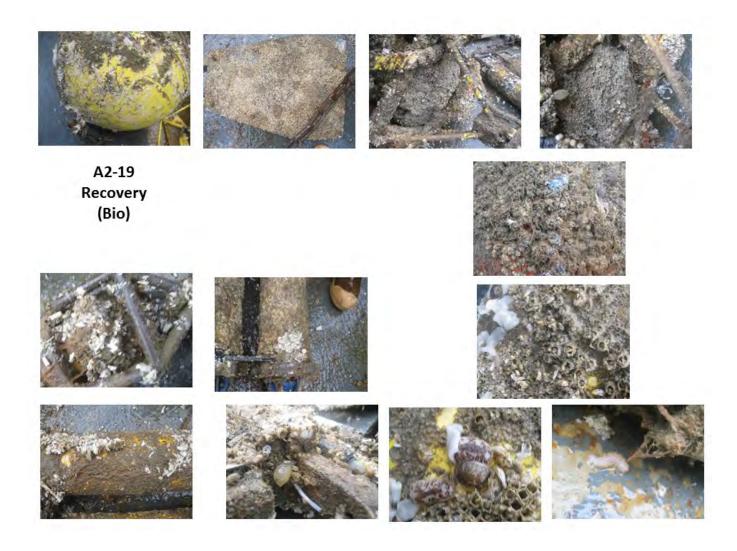




BERING STRAIT 2021 RECOVERY PHOTOS



BERING STRAIT 2021 RECOVERY PHOTOS (continued)



BERING STRAIT 2021 RECOVERY PHOTOS (continued)



BERING STRAIT 2021 RECOVERY PHOTOS (continued)

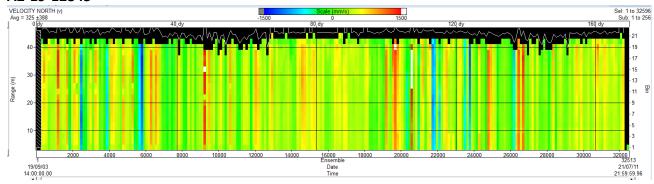


BERING STRAIT 2021 PRELIMINARY ADCP RESULTS

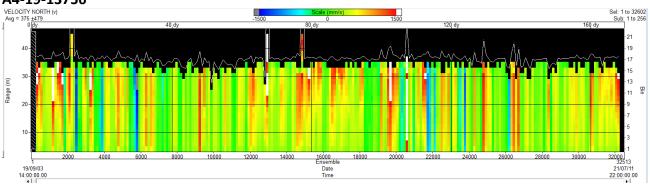
Preliminary plots of northward velocity, and velocity magnitude from the six recovered ADCPS are given below.

NORTHWARD VELOCITY from Bering Strait 2019-2021 ADCPs

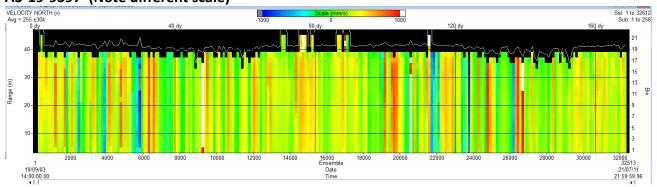
A2-19-12845



A4-19-13756

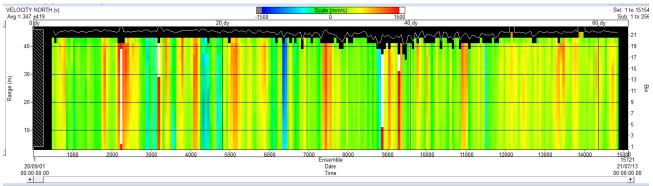


A3-19-9397 (Note different scale)

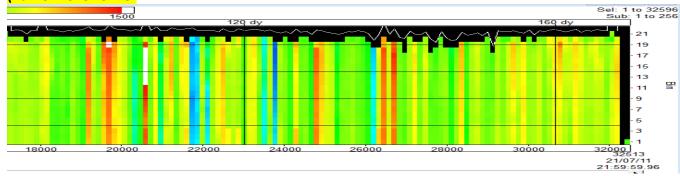


NORTHWARD VELOCITY from Bering Strait 2020-2021 ADCPs

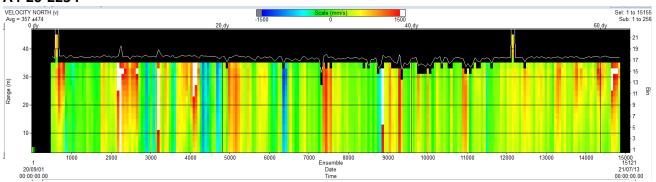




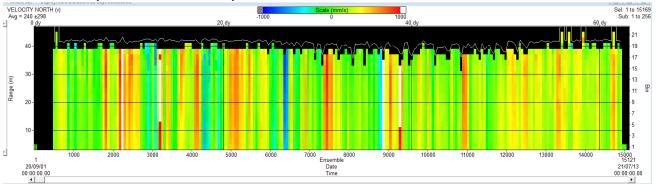
(half of 2019 for ref



A4-20-2234

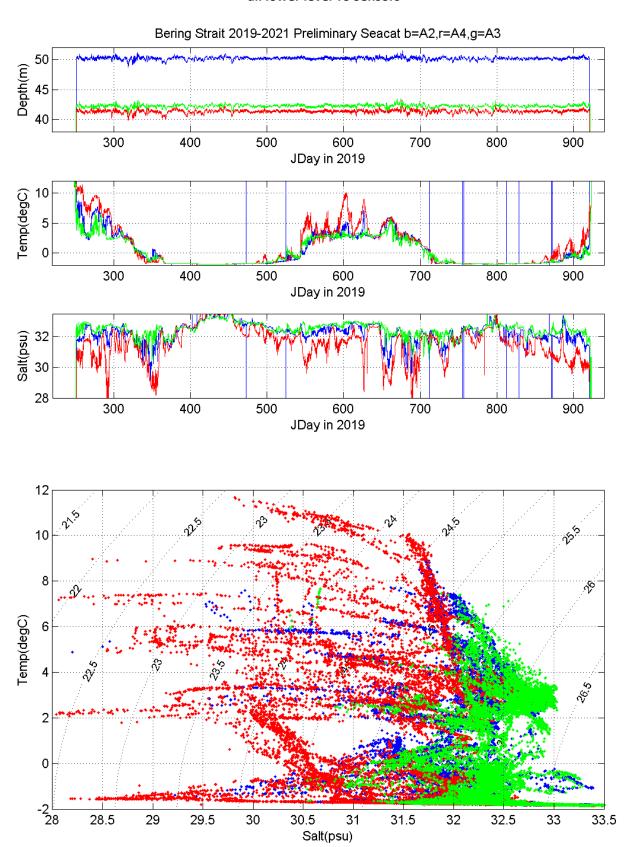


A3-20-13578 (Note different scale)



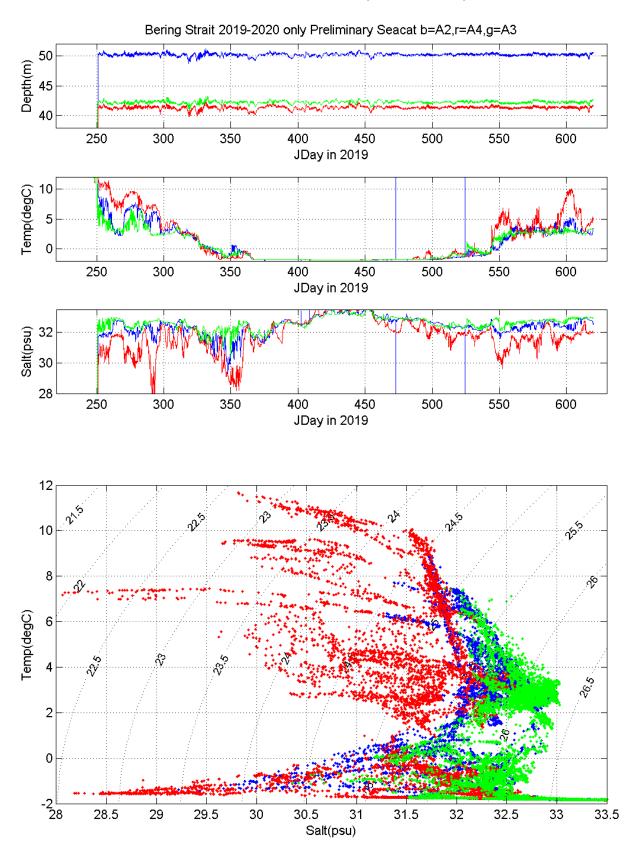
BERING STRAIT 2019-2021 SBE PRELIMINARY RESULTS (2 years, Ax19data)

- all lower level TS Sensors



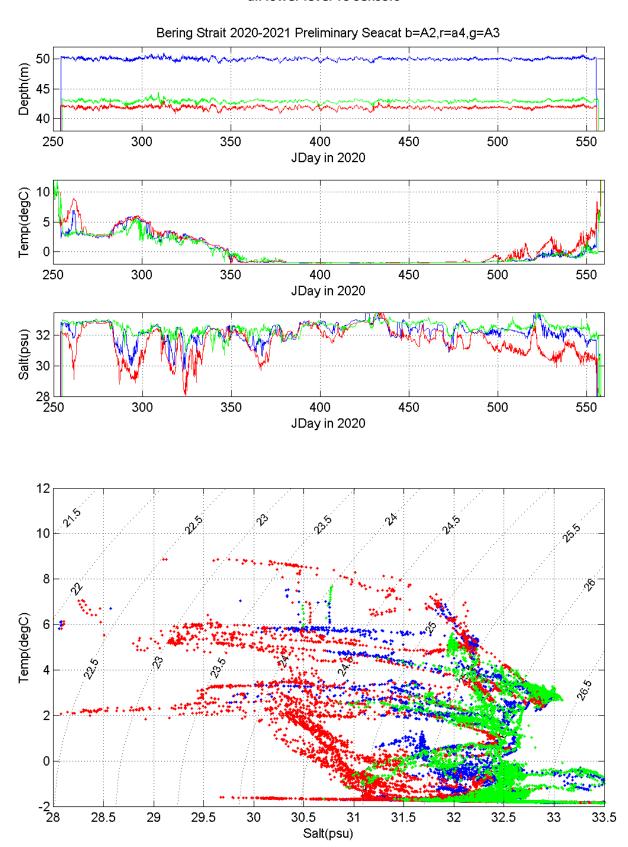
BERING STRAIT 2019-2020 SBE PRELIMINARY RESULTS (Ax19 data)

- all lower level TS Sensors (first year of data only)



BERING STRAIT 2020-2021 SBE PRELIMINARY RESULTS (Ax20 data)

- all lower level TS Sensors

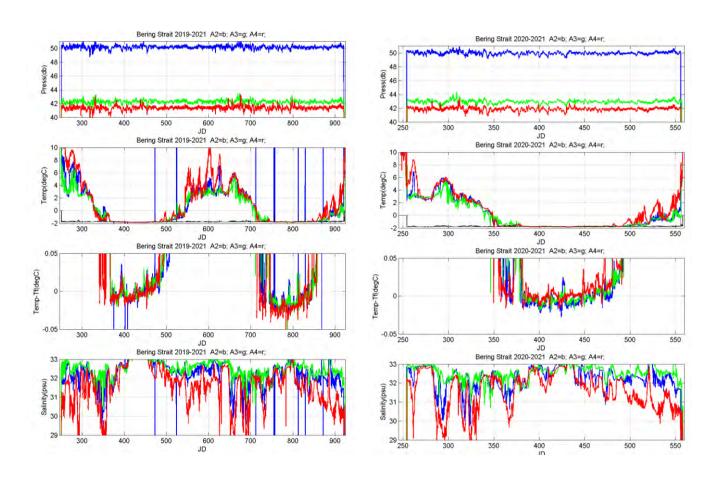


BERING STRAIT 2019-2021 SBE PRELIMINARY RESULTS (2 years, Ax19data)

- all lower level TS Sensors

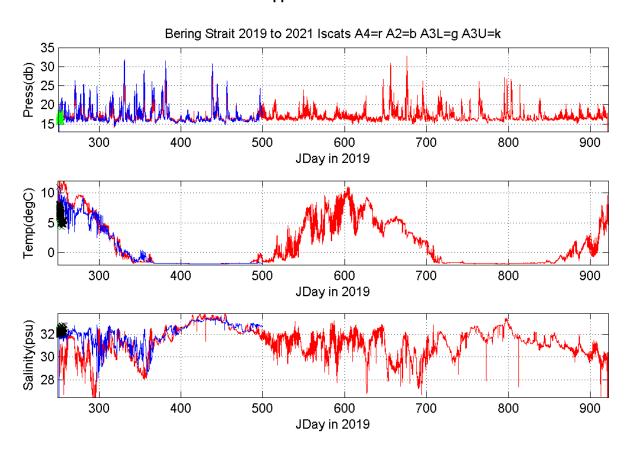
Comparison to freezing temperature

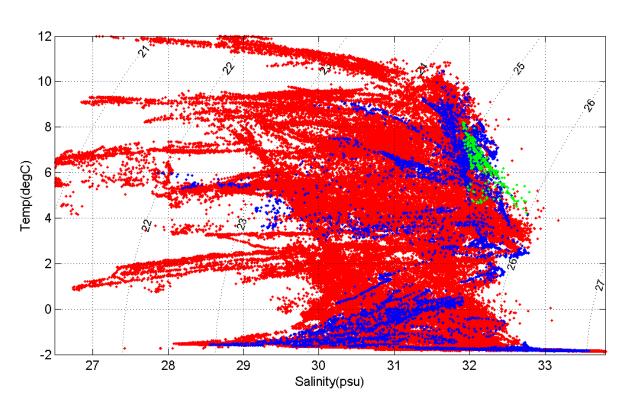
Note the Ax19s have a greater freezing temperature departure in winter, indicating the cumulative effect of biofouling



BERING STRAIT 2019-2021 ISCAT PRELIMINARY RESULTS (2 years)

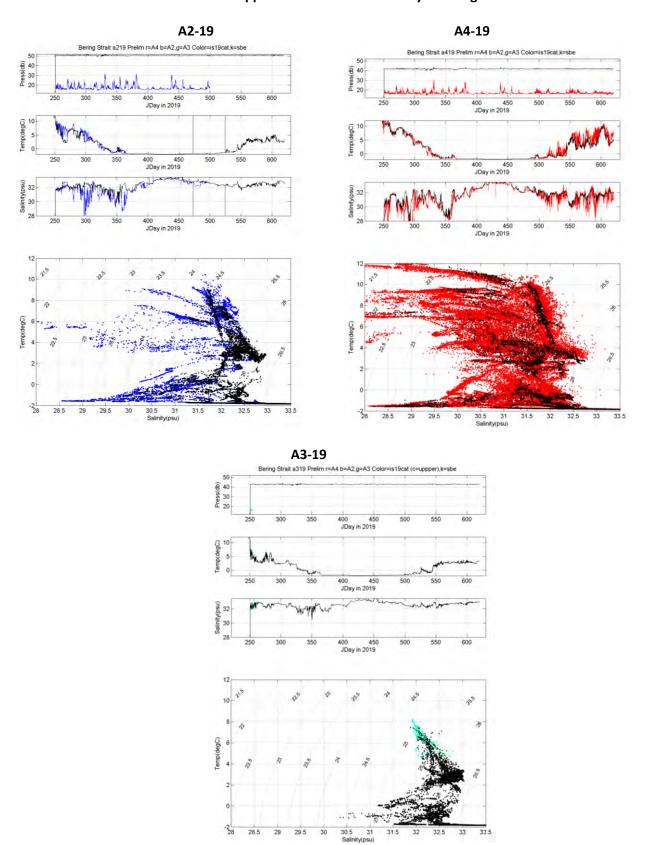
- all upper level TS Sensors





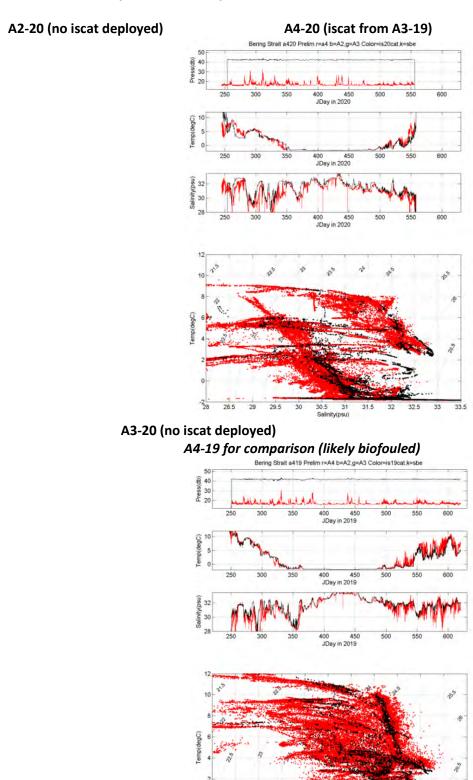
BERING STRAIT 2019-2020 ISCAT and SBE PRELIMINARY RESULTS (Ax19data)

-upper and lower TS sensors by mooring



BERING STRAIT 2020-2021 ISCAT and SBE PRELIMINARY RESULTS (Ax19&Ax20data)

-upper and lower TS sensors by mooring (only A419 iscat still present)



CTD OPERATIONS (On-board lead: Christensen)

As in previous years, in 2021 the moorings were supported by annual CTD sections. This year (as per 2014, 2015, 2016, 2017, 2018 and 2019) these sections were run without taking any bottle samples, although this year a separate pumped system was used to take trace metal and nutrient samples (and two samples for later O18 analysis).

The CTD rosette system used on this cruise was loaned from APL-UW and, was the same set up as in 2016, 2017, 2018 and 2019 (the same set up as in 2014/2015, with the exception of the transponder). The full package consisted of:

one SBE9+ with pressure sensor

(SN26451 – calibration 17th June 2019)

two SBE3 temperature sensors

(T1 = SN0843 - calibration 28th Jan 2021)

 $(T2 = SN0844 - calibration 28^{th} Jan 2021)$

two SBE4 conductivity sensors

 $(S1 = SN0484 - calibration 11^{th} Feb 2021)$

(S2 = SN0485 - calibration 2nd Feb 2021)

two SBE43 oxygen sensors

(Ox1 = SN1753 - calibration 4th Feb 2021)

(Ox2 = SN1754 - calibration 4th Feb 2021)

one Wetlabs FLNTURT fluorescence/turbidity sensor (SN1622 – calibration 11th March 2010)

one Benthos Altimeter (SN50485, repaired spring 2015)

two Seabird pumps (believed to be SN50340, SN55236, but not confirmed)

one EG&G transponder (D-CAT SN31892, Interrogate: 11.0kHz, Reply: 13.5kHz)

The temperature, conductivity and oxygen probes were paired as last year, viz:

	remperature	Conductivity	Oxygen	Pump
Primary	#843	#484	#1753	SN NA
Secondary	#844	#485	#1754	SN NA



with a y-like connection system, whereby the exit vent of the loop was at the same depth as the intake as per recommendation from the manufacturer. The top of the Y contained a slow leak valve (the vent plug) to keep the system sea-water primed on removal from the water. Tests in Seattle in 2014 showed air in the system was expunged after ~ 45s of emersion in water.

All instruments were housed in one frame (see left, photo from prior cruise), weighted with diving weights to ensure a close-to-vertical cast, as per 2014.

The CTD was connected to a conducting wire winch on the ship. This winch (Rapp Hydema NW, SOW 160 5000m capacity, with 3 conductor 0.322"diameter wire), was new on the Norseman II in 2014. Chris Siani, APL, assisted with wiring and CTD tests of this system while the ship was in Seattle in April 2014. In 2021, we found the termination had been changed to a plug which did not fit our system. Thus a temporary fix was installed for a test cast by Robert Daniels and Jim Johnson, and after the test cast, a more permanent potted connection was installed. Action item: Check with ship pre cruise re termination.

The winch was connected to an SBE11 deckbox, which in turn was linked via serial ports and USB-serial connectors to a

dedicated PC, running the software package Seasave v7. Data were recorded in standard hexadecimal SBE format, incorporating NMEA GPS input from the Norseman II forward GPS (since the aft-Aframe GPS was giving the wrong date). Action item: Check the ship is carrying a spare GPS antenna.

An event log (copied attached at the end of this report) was maintained on the CTD computer, including comments on data quality and other issues. The log, the data files, and a screen dump of the end-of-cast Seasave image were copied to a thumb drive as a backup after each cast, and regularly (every few casts) transferred ashore via google drive for analysis. Additionally, as each cast was completed, a WhatsApp photo of the screen shot was sent ashore for cruise/data quality tracking.

The CTD console was set on the port side of the interior lab. The package was deployed through the aft A-frame using a special block supplied by the ship. Although a Pentagon ULT unit had been mounted inside by the CTD console for lowering and raising the CTD, in practice, the winch driving was done by a crew member on deck, directed by the CTD operator using radio commands. This was deemed more efficient given the shortness of the casts (50m or less).

As in previous years, in 2021 the crew operated the winch from a remote console on the deck by the A-frame, and still, as in previous years, winch speed was an issue. The lowering (and raising) rate we seek is ~30 or 40m/min. There is no readout of winch speed at the remote console and winch drivers had to estimate speed either from the sound of the winch or from feedback from the scientist in the lab. Action item: Be sure to calibrate in winch speed early in the cruise, preferably with some scale on the winch so the speed is consistent between operators. Update ship's winch so as to provide a speed readout by the remote console. Also, train CTD driver to check winch speed on read-out beside CTD console both for lowering and raising.

The A-frame was set slightly outboard and not repositioned during the cast - the package was lifted to the height of the aft rail of the ship by the winch, and swung inboard by hand. For the casts done during mooring operations, the CTD was hand-carried forward after each cast to the port-forward corner of the aft-deck, to clear the aft-deck for mooring work. Once all the mooring work was complete, the CTD package was kept at the rail.

Once mooring work was complete, CTD operations were run 24hrs, using a team (per watch) of 1 science team member driving the CTD, and 2-3 personnel on deck - one (ship's crew) driving the winch, and one or two ship's crew/scientists recovering the instrument. This cruise, the science team provided 1 person for deck for 12 hrs a day in good weather and for an extra 12hrs in bad weather, since in bad weather, it was deemed necessary to always have two persons catching the CTD as it came aboard.

The efficiency of the crew made for very speedy CTD operations, and combined with the fast winch speed, resulted in commendably fast times for running lines. Since the CTD system required ~ 1min in the water to allow for the pumps to turn on (initiated by a manual command sent by the CTD driver), the CTD was generally put over the side and down to ~ 7m before the ship had come to a complete stop. Experience allowed the crew to time this such that, by the end of the 1min soak, the ship had come to a sufficient stop. Once the ship was stopped, the CTD pump was on and data were reliable, the CTD package was returned to ~ 1m depth (just below surface) and then was lowered to the sea floor, target depth ~ 3m above bottom, see discussion below. Only a brief (1-2 s) pause was taken at the bottom before the CTD was returned to the surface, and then recovered. If the cast was successful, the ship would start to move away just as the package was being recovered. Note on these stations, taken without any bottles, it was not necessary for the cast to be entirely vertical.

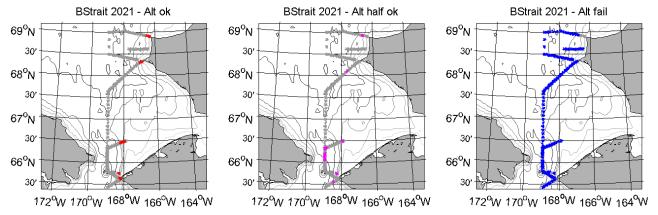
If pumped samples were to be taken, this operation followed on immediately after the CTD cast without the ship repositioning. Action item: Make sure the CTD is recovered and out of the water before the pump system is deployed, otherwise ship's manoeuvrability is compromised.

Prior to each cast the turbidity sensor was cleaned by rinsing with soapy water and freshwater and wiping. Action item: Bring syringe with better fit for flushing the CTD cell.

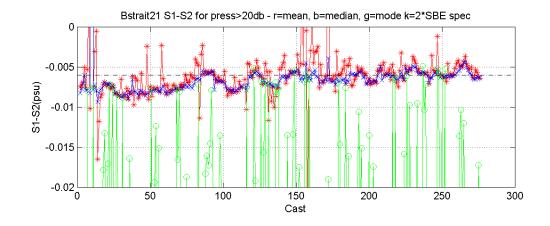
Ship's draft was estimated at 2m, and this should be taken into account in viewing the data. Also given that sea states were often significant and the altimeter on the CTD rarely functioned, some casts stop 5m-6m above the bottom.

Overall, CTD data this year are exceedingly clean, although the following issues were encountered:

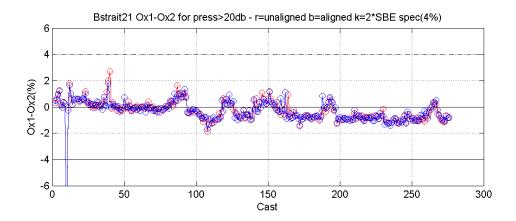
- 1) For casts up to and including 10. Significant mismatch was found between the up and down casts in salinity and oxygen, indicative of a timing mismatch between the sensors. (Cast 10 was run with pumps off to check the pumps were working they were.) Investigation of the system found the TS duct was missing. When this was replaced (for cast 11 onwards), the mismatch became much smaller almost unnoticeable in salinity, though still present in oxygen. The later was found to be greatly improved by data processing (see below).
- 2) Altimeter. In previous years, it was found that the altimeter only performed well intermittently, and the pattern of success and failure appeared to be strongly correlated with water temperature. This year, being early the season, the waters were generally colder and the altimeter was primarily useless. On viewing sections, recall bottom 3+m may be unsampled. Actin Item: Next year, reconsider bottom depth decisions in light of warmer waters.



- **3) Vent plug blocking.** As in previous years, the blocking of the vent plug due to impurities in the water was a continual concern. We instigated a cast-by-cast check that the tubes were draining once the CTD was recovered and if either was slow, the plugs would be cleaned with wire. **Action item: Continue this check in other years.** High vigilance to this issue this year resulted in fewer problems with the data, but data should still be checked for this problem. (Suspect casts: 16, 42, 62, 63, 117, 172(recast as 173)
- **4)** Offset between Salinity sensors. Prior years found an offset in salinity between the two sensors on the CTD. This year, a similar offset was observed (with S1 reading fresher as in prior years). The CTD should be accurate to 0.003psu, and thus discrepancies of < 0.006psu (marked as dashed line on plot) are within specifications. Early in the cruise (and after cast 222, which is suspected to have hit bottom), the sensors were flushed, and at the start of the cruise an airtest test taken which may be used later for information. In general, agreement was just within manufacturer's specifications. Action item: Flush cells with freshwater on deck at start of cruise and at regular intervals.



5) Offset between Oxygen sensors. Once aligned in post processing, differences between oxygen sensors were also within manufacturer's specifications.



6) Other cast issues:

- cast 25 was yoyoed after the main cast to examine the Oxygen maximum. For the archives, a trimmed version of this file has been made (with the original cast number) including the original full down and up cast. The full yoyed cast is retained as "orig".
- cast 114 was aborted as the CTD came out of the water, and recast as cast 115
- cast 172 (end of the LIS line) has an usual midlayer intrusion, worth further investigation
- cast 172 had vent plug issues, and was immediately recast (without recover) as cast 173
- cast 222 contains interesting layering at the surface (and is suspected to have hit bottom, making oxygen data suspect on the upcast.

NOTES ON BERING STRAIT 2021 CTD PROCESSING

For 2021, we have new cals for T, C and Ox, so we are running with:

```
Pressure 17thJune 2019 - this is the new one, and has a new SN of 26451 T1 (#843) 28<sup>th</sup> Jan 2021 T2 (#844) 28<sup>th</sup> Jan 2021 C1 (#484) 11<sup>th</sup> Feb 2021 C2(#485) 2<sup>nd</sup> Feb 2021 - Ox1 (1753) 4<sup>th</sup> Feb 2021 Ox2 (1754) 4<sup>th</sup> Feb 2021 FLNTURT (#1622) - 11<sup>th</sup> March 2010-
```

These are accurately in the BStrait21nnn.xmlcon files.

SUMMARY OF PROCESSING ISSUES 2021

=== casts 0-10 were done missing TS duct and thus there is significant alignment issue with Conductivity. As these were all calibration casts looking at the deep water, while the issue appeared in the layers above/below a temperature gradient, these casts have not yet been specially processed

```
== cast 10 was done with pumps off (a repeat of cast 9)
```

```
== cast 16 - vent plug issues
```

== cast 25, as an oxygen test, was yoyoed after the main cast to below the depth of the oxygen maximum and recovered slowly. ... original file is included as 025orig. 025 is trimmed to only the full initial cast

```
== cast 42 - suspect vent plug issue
== cast 62 - vent plug issues
```

== cast 63 - vent plug issues

```
== cast 114 was aborted as CTD came out of water. Recast as 115
```

== cast 117 - salinity issues

== cast 158 spike in C1

== cast 172 - vent plug issues, Recast as 173

= cast 222 is suspected to have hit bottom. Oxygen data suspicious on up cast.

- == many casts struggle with sharpness of thermocline giving spikes in Salinity. aligning seems to fix this
- == Almost all casts show align issues with Oxygen using Ox34 seems to mostly fix this

Results recorded by cast in master CTD log file RWnoteson2021BstraitCTDcasts.xls

FULL NOTES ON BERING STRAIT 2021 CTD PROCESSING

Rebecca Woodgate (based on 2019)

Start with files from SeaSave for each cast, i.e.,

Bstrait21nnn.hex and Bstrait21nnn.hdr

Then run through 9 steps (8 of them with SBEDataProcessing program from Seabird).

=== 1) First make up a file to be used for quick plotting. This contains all variables, but is not corrected in any way.

IN SBEDATA PROCESSING, RUN: DATA CONVERSION (PSA file for this = 001_DatCnvBStrait2021_allvars.psa) Inputs are: BStrait21nnn.hex and BStrait21nnn.hdr

- *In FILE SETUP
- -- CHECK box on match instrument to configuration file
- -- Choose input file (should be .HEX) and directory
- -- Name append .rw1
- -- Choose output directory
- *In DATA SETUP
- -- Convert data from:UP and downcast (Last year we just did down as we were firing no bottles. Here we do both, noting that upcasts may differ because of water being swept up with the CTD.)
 - -- Create file types: data (.CNV) only
- ...—Merge Header file
 - -- Select output variables... as in previous years we use
 - -- 1) Pressure, Digiquartz (db)
 - -- 2) Temperature (ITS-90, degC)
 - -- 3) Temperature,2 (ITS-90, degC)
 - -- 4) Conductivity (S/m)
 - -- 5) Conductivity, 2 (S/m)
 - -- 6) Oxygen raw, SBE 43 (Volts)
 - -- 7) Oxygen, SBE 43 (saturation)
 - -- 8) Oxygen raw, SBE 43, 2(Volts)
 - 9) Oxygen, SBE 43, 2(saturation)
 - -- 10) Fluorescence WET Labs WET star (mg/m^3)
 - -- 11) Upoly 0, FLNTURT
 - 12) Scan Count % This was done in 2018, but not recorded in the write up
 - -- 13) Salinity, Practical (PSU)
 - -- 14) Salinity, Practical, 2 (PSU)
 - -- 15) Time, NMEA (seconds)
 - -- 16) Latitude (deg)
 - -- 17) Longitude (deg)
 - -- 18) Altimeter (m)
 - -- 19) Pump Status
 - -- Source for start time in output .cnv header: Select NMEA time

-- Keep all defaults. Note the Oxygen is Window size (2s), Apply Tau Correction, Apply Hysteresis.

THIS GIVES files called: BStrait21nnn.rw1.cnv

^{*}In MISCELLANEOUS

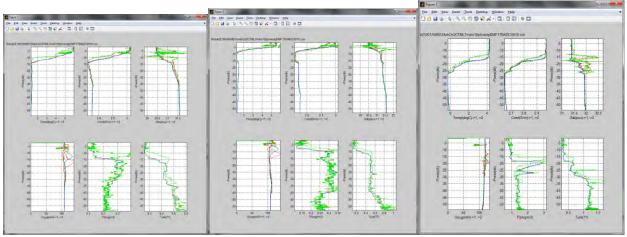
=== 2) Do first basic quality control by plotting everything in Matlab

Matlab master code = **testplotsBStrait2018RW.m** which calls subroutine **CTDQCpump.m Inputs are: BStrait18nnn.rw1.cnv**

Checks here include:

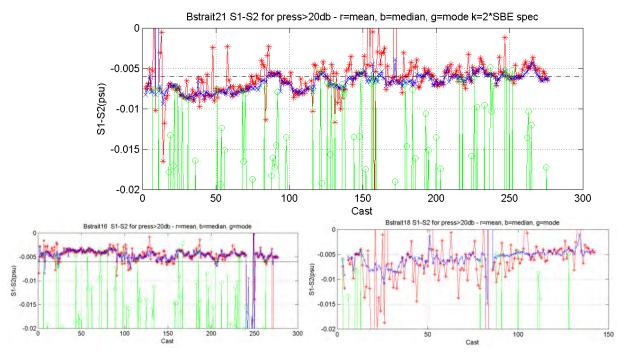
- --- that the pump comes on
- --- that the altimeter is working
- --- that T1=T2, S1=S2 and Ox1=Ox2
- --- preliminary identification of spikes and other issues.

Running all the processing steps on casts 0-10 did not remove the problem.



Examination of the system found that the TS Duct was missing.

Once the TDuct was installed, salinity differences became closer to and finally within manufacturer's specs



Worse than 2016 but on a par with 2018

=== 3) Now work through the 7 steps of SBEDataConversion. Start by applying the calibrations to get the converted files, but this time excluding all the derived variables.

IN SBEDATA PROCESSING, RUN: DATA CONVERSION

(PSA file for this = DatCnvBStrait2021 CTDforprocess.psa)

Inputs are: BStrait21nnn.hex and BStrait21nnn.hdr

- *In FILE SETUP
- -- CHECK box on match instrument to configuration file
- -- Choose input file (should be .HEX) and directory
- -- Name append NONE
- -- Choose output directory
- *In DATA SETUP
- -- Convert data from:UP and downcast (Last year as here, we do both, noting that upcasts may differ because of water being swept up with the CTD.)
 - -- Create file types: data (.CNV) only
- ...-Merge Header file
 - -- Select output variables... for 2018 we use
 - -- 1) Pressure, Digiquartz (db)
 - -- 2) Temperature (ITS-90, degC)
 - -- 3) Temperature,2 (ITS-90, degC)
 - -- 4) Conductivity (S/m)
 - -- 5) Conductivity, 2 (S/m)
 - -- 6) Oxygen raw, SBE 43 (Volts)
 - -- 7) Oxygen raw, SBE 43, 2(Volts)
 - -- 8) Fluorescence WET Labs WET star (mg/m^3)
 - -- 9) Upoly 0, FLNTURT
 - -- 10) Scan Count
 - -- 11) Time, NMEA (seconds)
 - -- 12) Latitude (deg)
 - -- 13) Longitude (deg)
 - -- 14) Altimeter (m)
 - -- 15) Pump Status
 - -- Source for start time in output .cnv header: Select NMEA time

THIS GIVES files called: BStrait21nnn.cnv

=== 4) Second step of SBEDataProcessing. Apply a time filtering to the data.

This step allows us to time-filter (i.e., smooth) the data. Routine allows us to select two filters, A and B. In 2014, we used A = 0.5 sec and B=0.15 sec, but in 2015 this appeared to remove too much variability. Manual for the SBE9plus suggests to not filter Temperature and Conductivity, but to filter pressure at 0.15s. So set A=0, and B=0.15 and then only filter pressure (this is now the same as 2015, but different to 2014).

Note these filters should be applied to the raw data (e.g., Ox voltage, Conductivities), not the derived data (e.g., salinity, oxygen saturation, etc).

IN SBEDATA PROCESSING, RUN: FILTER

^{*}In MISCELLANEOUS

⁻⁻ Keep all defaults. Note the Oxygen is Window size (2s), Apply Tau Correction, Apply Hysteresis.

(PSA file for this = FilterBStrait2021_CTDforprocess.psa)

Inputs are: BStrait21nnn.cnv

- *In DATA SETUP
- -- Lowpass filter A(sec): 0.0 (was 0.5 in 2014, but this seemed too smooth in 2015, so used 0, as here)
- -- Lowpass filter B(sec): 0.15 (This is as per the manual for SBE9plus)
- --> SPECIFY FILTERS
- -- Pressure: Lowpass filter B
- -- Temperature: None
- -- Temperature, 2: None
- -- Conductivity: None
- -- Conductivity,2: None
- -- Oxygen raw: None
- -- Oxygen raw,2: None
- -- All others: None
- *In FILE SETUP
- -- Name append = A00B15 ... this indicates data was filtered (Note: makes only small changes to the data)

THIS GIVES files called: BStrait21nnnA00B15.cnv

=== 5) Third step of SBEDataProcessing. Align the timeseries in time.

This step is to compensate for the delay between the water passing the various sensors in the pumped pathway. For the SBE9plus, the manuals suggest that

- the temperature advance relative to pressure =0
- that the salinity advance relative to pressure is 0.073s, but this advance is set in the SBE11plus by factory settings, and thus for this program we use conductivity advance =0. **Action item: Check this is what is set in the SBE11 plus.**
- that the oxygen advance should be between +2 and +5. This should be done on the Oxygen voltage.

IN SBEDATA PROCESSING, RUN: ALIGN

(PSA file for this = AlignCTDBStrait2021 CTDforprocessOx34.psa)

Inputs are: BStrait21nnnA00B15.cnv

- *In DATA SETUP
- --> Enter Advance values
- -- Oxygen: 2 (as recommended in SBE9+ manual (2 to 5), and tests suggest in 2014 and 2015)
- -- All others: 0
- *In FILE SETUP
- -- Append added = AdvOx5

THIS GIVES files called: BStrait21nnnA00B15AdvOx2.cnv

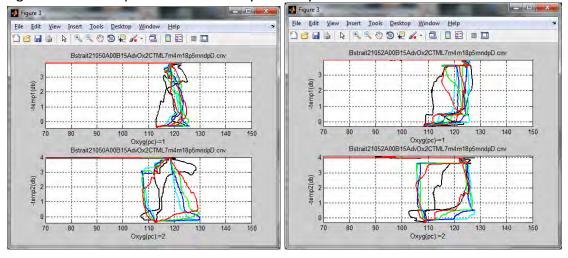
So, of these, it is suggested we investigate the various oxygen options. This we run this step with various values for the oxygen advance (2-5) and, by plotting oxygen against temperature, see which advance value gives the most consistent reading comparing the up and down casts.

Previous years have segregated casts into which colors are good. Here we look at casts up to 30 and spot check beyond that:

Black (0)	Red (2)	Green(3)	Blue (4)	Cyan (5)	Unclear
Primary	10,14,15,20	13,16,18,19,21,22,23	12		
Sensors		24,25,26,27,28,30			
Secondary		19	18,20,21,22,23,24,25	15.16,27	
Senors			,26,29,30		

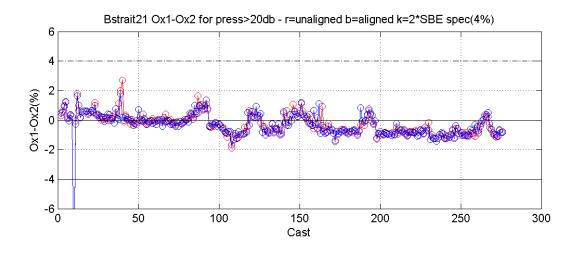
By this tally, Green(3) has the best fit most often is Green (3) for system1 and blue (4) for system 2. Use this here even though previous years have used (2).

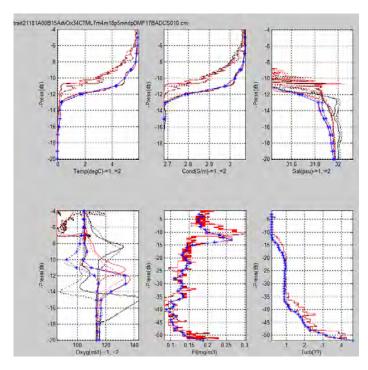
Again show that up and down casts by differ by 5%-10%.



Finally conclude:

- at this stage will use Ox1, as it shows less spread than Ox2.
- alignment is generally best for both as +3 for system 1 and +4 for system 2.
- recognize that up and down casts may differ by 5%-10%.
- agreement between sensors within manufacturer's specs





Check to see how much aligning fixes the problems in S and Ox with sharp T gradient: K = unaligned

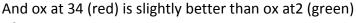
- Note S inversion
- -Note Ox + and -ve peaks at different depths

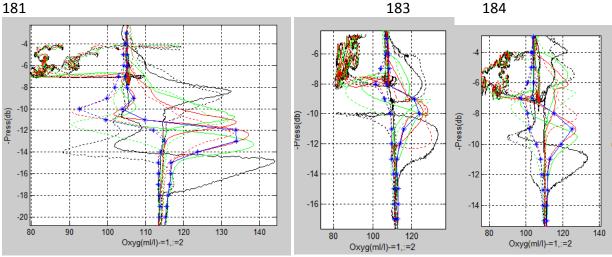
Red = aligned (Ox34)
Blue = Bin av down cast.

SO

- has fixed S overrun very effectively
- has moved ox peaks to be about same mag, and all +ve and a reasonable depth given difference in depth on up and down cast.

And this is all well reflected in bin average





184 -- ok with Ox1, less so with ox2

=== 6) Fourth step of SBEDataProcessing. Correct for thermal mass of the cell

This is a standard SBE correction to compensate for thermal mass of the cell. Assumes the pump is at 3000 rpm. *Action item: Check this.* Then manual suggests for SBE9+ Alpha=0.03, 1/beta=7.

IN SBEDATA PROCESSING, RUN: CELL THERMAL MASS (PSA file for this = CellTMBStrait2021_CTDforprocess.psa)

Inputs are: BStrait21nnnA00B15AdvOx234.cnv

- *In DATA SETUP (correct both Primary and Secondary values)
- -- Thermal anomaly amplitude [alpha]: 0.03 (suggested for SBE9+)
- -- Thermal anomaly time constant [1/beta]: 7 (suggested for SBE9+)
- *In FILE SETUP
- -- Append added = CTM

THIS GIVES files called: BStrait21nnnA00B15AdvOx34CTM.cnv

== 7) Fifth step of SBEDataProcessing. Remove pressure loops from the casts.

This step is to take out pressure looping, stalls in lowering, and the surface soak. To run this, you must have filtered the pressure first (as we did above). This does not remove any data, it just marks looped data with a bad data flag of -99e-26.

In 2015, we instigated a 5m depth for the initial surface soak, returning after that soak to the surface to start the downcast. Thus the used values were L5m2m6m (soak, min, max) and were used including deck pressure, and that seemed to work well with this routine. Prior years just used a 2m soak depth and that might be less successful with this routine.

In 2016 the soak was about 4m .. checks show this works with this routine and these settings. In 2017, soak is about 7m, but sometimes much deeper. Previous settings (L5m2m6m) did not work well with this data set. After investigation, we learn the following:

- likely best not to include the deck pressure as offset our system is never on while in air, and thus this will just introduce a non-intuitive offset.
- the max must be deeper than the deepest soak, yet shallower than the maximum depth of the shallowest cast. In 2017, the shallowest casts were (Cast1 and 2, tests, and thus not considered; 113(19.6m), 114(19.6m), 115(19.5m), 117(18.7m). Our deepest soaks were cast 20(18.25m), cast 31(16m). Thus, we set max to be 18.5m
- the min must be deep enough to separate the going-in-the-water oscillations from the soak. 2m and 3m were found to be too shallow in 2017, but by inspection 4m works well.

Finally settings for 2017 were thus: 7m soak, min 4m, max 18.5m. (Note if you specify max and min, the program is not supposed to use soak depth at all.)

In2018 these settings gave a good result and were used without further testing.

In 2021 we again adopted these settings. The only problematic casts are:

Cast 25,.. which was yoyoed because of initial discrepancies in the data.

In preliminary processing, copy the original hex file to 025orig, and take a trimmed version through the processing instead

IN SBEDATA PROCESSING, RUN: LOOP EDIT

(PSA file for this = LoopEditBStrait2021_CTDforprocess.psa)

Inputs are: BStrait21nnnA00B15AdvOx34CTM.cnv

Must run filter on pressure first. Flag surface soak with -9.99e-26...

- *In DATA SETUP
- -- Minimum ctd velocity (m/s) = 0.25
- --> Check box Remove Surface soak
- -- Surface soak depth (m) = 7
- -- Minimum soak depth (m) = 4
- -- Maximum soak depth (m) = 18.5
- --> UNCheck box Use deck pressure as pressure offset
- --> Check box Exclude scans marked bad
- *In FILE SETUP
- -- Append added = L7m4m18p5mndp

THIS GIVES files called: BStrait21nnnA00B15AdvOx34CTM L7m4m18p5mndp.cnv

=== 8) Sixth step of SBEDataProcessing. Derive the parameters you want.

This step takes the raw data and calculates derived parameters, such as salinity, density, oxygen values, etc.

IN SBEDATA PROCESSING, RUN: DERIVE

(PSA file for this = DeriveCTDBStrait2021_CTDforprocess.psa)

Inputs are: BStrait21nnnA00B15AdvOx34CTML7m4m18p5mndp.cnv

-- CHECK box on match instrument to configuration file (Prior notes says to check this box, however, in 2016 this crashed if the box was checked, so instead uncheck the box, **BUT MUST MAKE SURE IS USING A CURRENT CALIBRATION FILE**). If ever change sensors during cruise, will have to do something different here. Check these files to make sure the .con files are consistent.

- *In DATA SETUP
 - --> Select derived variables... add:
- -- Salinity (psu)
- -- Salinity,2 (psu)
- -- Salinity difference
- -- Sigma theta (kg/m3)
- -- Sigma theta, 2 (kg/m3)
- -- Sigma theta difference
- -- Oxygen, SBE 43 (ml/l)
- -- Oxygen, SBE 43 (saturation)
- -- Oxygen, SBE 43, 2 (ml/l)
- -- Oxygen, SBE 43, 2 (saturation)
- *In FILE SETUP
- -- Append added = D

THIS GIVES files called: BStrait21nnnA00B15AdvOx34CTM L7m4m18p5mndp D.cnv

Could stop here, and use these files, but to be more useful want to have Bin averages and despike, and the combination of the two of those processes. So, first look at the despiking options. SBEDataProcessing includes a file called "Wild Edit", but the manual describes that as "not the faint of heart" and says much trial and error is necessary to get good results. Thus, instead use something more automatic, Window Filter.

=== 9) Twelfth step of SBEDataProcessing. Use Window Filter to despike.

This is an attempt at automatic despiking. If just try so smooth over a spike, you will flatten it, but the bad data will still remain. Here we make one basic attempt, as outlined in the manual. This takes a window of data points, and for each window, replaces the central (?) point with the median of all the points. In some way thus, this is smoothing over the data points, but one that neglects extreme values. Their example suggests 17 points, and we have used that. Sampling rate is 24Hz. Drop rate is ~ 1m/s. So this is roughly equivalent to smoothing at 0.7 sec, or 70cm.

IN SBEDATA PROCESSING, RUN: WINDOW FILTER

(PSA file for this = W_FilterCTDBStrait2021_CTDforprocess_MF17.psa)

Inputs are: BStrait21nnnA00B15AdvOx34CTM L7m4m18p5mndp D.cnv

*In DATA SETUP

- --> Select Exclude scans marked bad
- --> Specify Window Filters:

Type: Median Parameters: 17

For variables: Temp1, Temp2, Cond1, Cond2, Oxraw1, Oxraw2, Fluorescence, Upoly (Turbidity/Transmissivity), Latitude, Longitude, Salinity1, Salinity2, Density1, Density2, Ox1ml/l, Ox1%, Ox2ml/l, Ox2%

-- Append added = MF17

THIS GIVES files called: BStrait21nnnA00B15AdvOx34CTM L7m4m18p5mndpDMF18.cnv

=== 10) Seventh step of SBEDataProcessing. Bin average all the data.

All data files prior to this have been the 24Hz data up and down casts. Here we separate out the downcasts only, exclude the data marked bad by loop edit, and create 1m bin averages. We chose here to create a surface sample, however often the number of scans in that sample is small and in any case surface stirring by the ship must also be considered.

IN SBEDATA PROCESSING, RUN: BIN AVERAGE

(PSA file for this = BinAvgBStrait2021 CTDforprocess.psa)

Inputs are: BStrait21nnnA00B15AdvOx34CTM L7m4m18p5mndp.cnv &

BStrait21nnnA00B15AdvOx34CTM L7m4m18p5mndpDMF17.cnv

- *In DATA SETUP
- -- Bin type = Pressure
- -- Bin size = 1
- --> Select Exclude scans marked bad
- → Select include number of scans per bin
- -- Scans to skip over = 0
- -- Cast to process = **Downcast**
- -> Include surface bin 0,1,0
- *In FILE SETUP
- -- Append added = BADCS010

THIS GIVES files called: BStrait21nnnA00B15AdvOx34CTM L7m4m18p5mndpDBADCS010.cnv & BStrait21nnnA00B15AdvOx34CTM L7m4m18p5mndp DMF17BADCS010.cnv

In 2021 this marks the end of the CTD pre processing.

BERING STRAIT 2021 CTD OPERATION NOTES from end of cruise

- 0. Coming onto station
 - pre fill Event Log (Excel file)
 - In Seasave
 - Real time data, Start, Begin archiving data immediately
 - Select Output Data File Name: Bstrait21nnn.hex, *** NOTE NAME 17, not 2017
 - Start
 - fill in header
 - Ship: Norseman 2, Station name (e.g., BS24), Operator
 - then WAIT
 - Driver to Deck: "clean wetlabs sensor"
 - Deck to Driver: "sensor cleaned"
 - Driver to Deck: "Is transponder in?"
 - Deck to Driver: "Transponder in"
- 1. On station confirmed from bridge "on station",
 - Driver to deck, "Ready to Deploy"

CTD in the water (Deck to Driver: "CTD in water and at 5m") (Driver: double click radio)

- Power on CTD Deck Unit, check get readout of "10" (0110)
- OK on SeaSave header, wait until SeaSave gray windows close
- Real-time Control, Pump on (to turn pump on manually)
- Fill out rest of Event log (Excel file) for deployment (including time).
- Driver to deck, "Please report wave height, air visibility, water visibility"
- WAIT until -"11", "Pump on", Data ok (incl S and position), check #'s agree
- check target depth ~ water depth under keel
- Driver to Deck: "return to surface and go down to xxx meters" (GET SURFACE WIRE OUT)
- Deck to Driver: "Going down"
- Check lower speed (want 30/40 m/min) on winch readout
- 3. CTD lowers
 - watch pressure ... (resist temptation to analyze the cast on the way down) .. focus only on the pressure
 - Driver to Deck: "3 2 1 stop" for target depth
 - Deck to Driver: "CTD stopped" (GET BOTTOM WIRE OUT)
 - wait ~2sec
 - Driver to Deck: "Come to surface" AND CHECK CTD COMES UP
- 4. CTD comes up ** COMPARE SENSOR PAIRS decide if data good enough to leave station

When at surface (Deck to Driver: "At surface") (Driver: double click radio)

- real time control Pump off
- real time data STOP
- Power off CTD Deck Unit
- Driver to deck: "Recover CTD and proceed to next station"
- OR IF may have to recast .. add "We have CTD issues, do not leave after this cast"
- fill in Event Log for up cast (including time), while
- Deck to Driver "CTD recovered, Pipes are/not draining", and default is ship leaves for next station.
- 5. THEN
 - screen dump to paint (Alt-print screen, Cntrl V, save as BStrait21nnn.png); F12 (save as);
 - QUIT paint.
 - Copy the 4 files (.hex, .hdr, .xmlcon, .png) to USB Backup file directory

(Start event log for next cast)

If leaves CTD for long time, check "transponder is out"

Deck responsibilities every cast:

- checking sensor cleaned and transponder in
- checking depth of surface soak
- watch wire (out aft is ok, under ship is not, far to side near ship not)
- keep winch operator focused
- count CTD as it goes down, listen for 3 2 1 stop and make sure winch stops
- At Bottom, make sure winch comes UP (e.g., watch wheel)
- Watch for tape on way up,
- Observe and report surface issues (e.g., broke surface, ask for repeat soak if out of water for more than 4 sec)
- report clarity of water (max range at which you can see CTD in m)
 - fog
 - wave height if exciting
- report if pipes are draining once CTD is on deck.
 - if not draining, clean vent plugs and report to CTD operator to add to notes.
- report if jelly fish remains on salinity cells
- make sure secure on deck.
- every 50 casts, check all CTD bolts

BERING STRAIT 2021 CTD LINES

A total of 14 CTD lines were run on the cruise.

Preliminary sections were plotted using code from An Nguyen from the preliminary processed data, which uses pre-cruise calibrations, and the quality control procedures outlined above to give 1m bin averages for plotting.

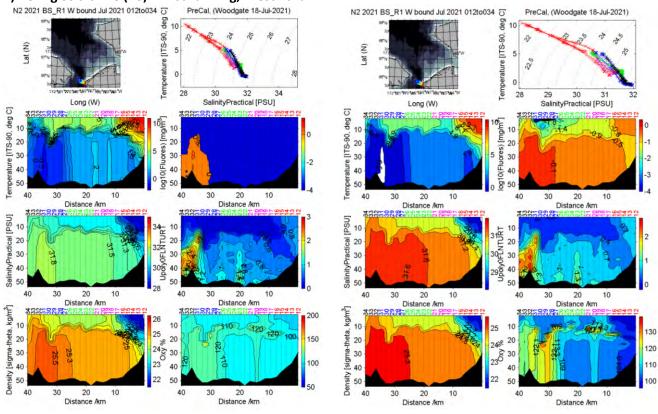
The plots below give all 14 sections on the same scales (left) and on a scale for that section (right), presented in order of data acquisition. Note that:

- this uses the S1 and Ox1 data,
- typically stops 2 to 3+ m above the bottom.

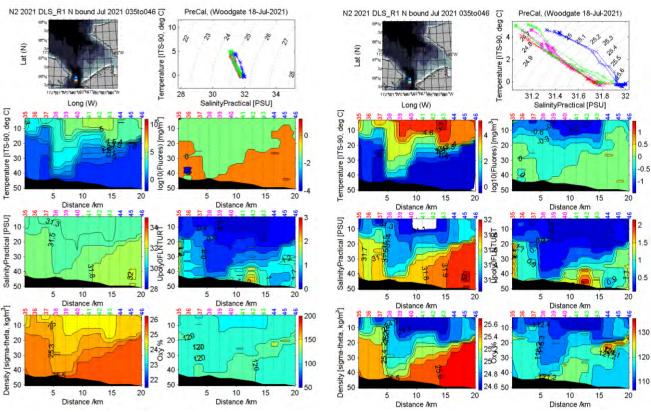
Several repeat sections were run on the cruise (see naming below)

For full positions and times see event log and data file headers.

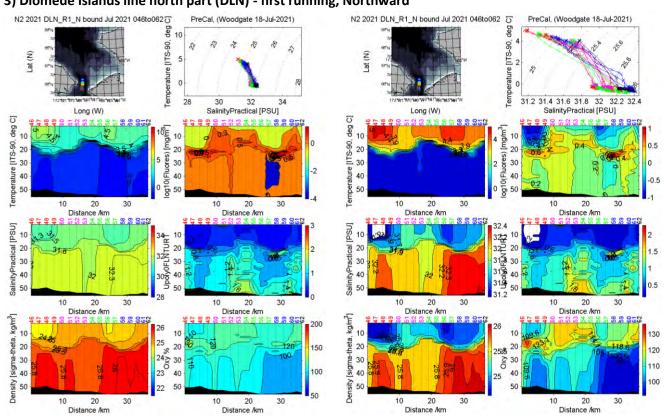
1) Bering Strait line (BS) - first running, Westward



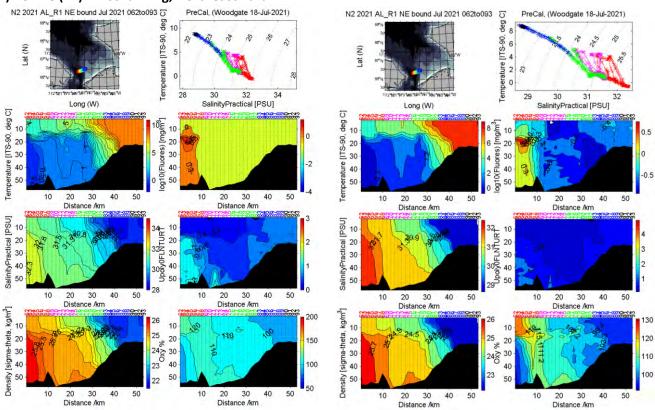
2) Diomede Islands line south part (DLS) - first running, Northward



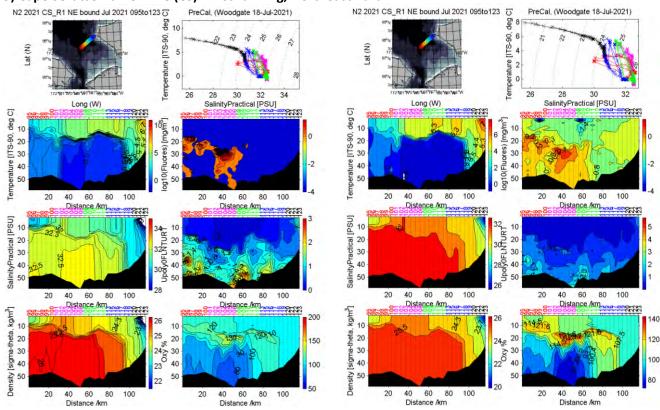
3) Diomede Islands line north part (DLN) - first running, Northward



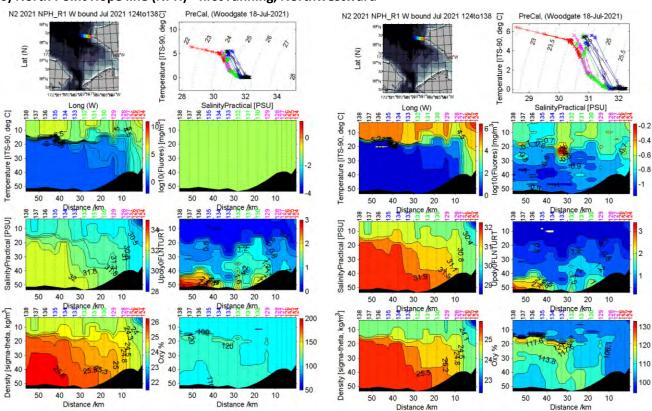
4) A3 line (AL) - first running, Northeastward



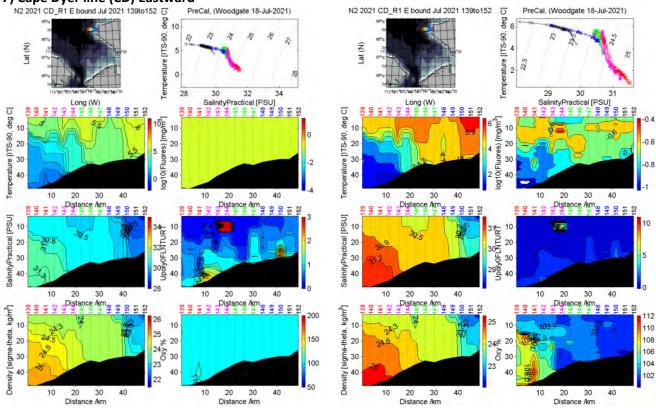
5) Cape Serdtse-Kamen line (CS) - first running, Northeastward



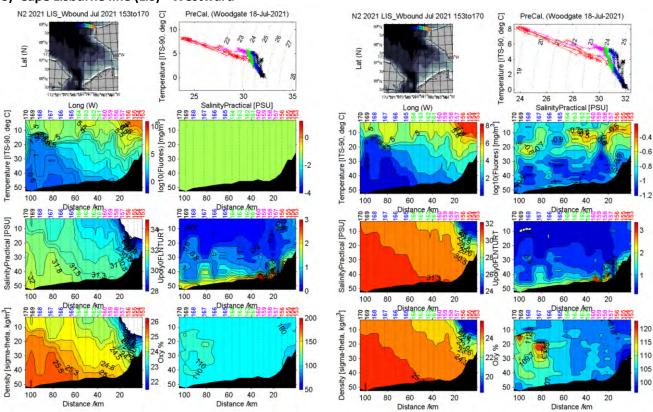
6) North Point Hope line (NPH) - first running, Northwestward



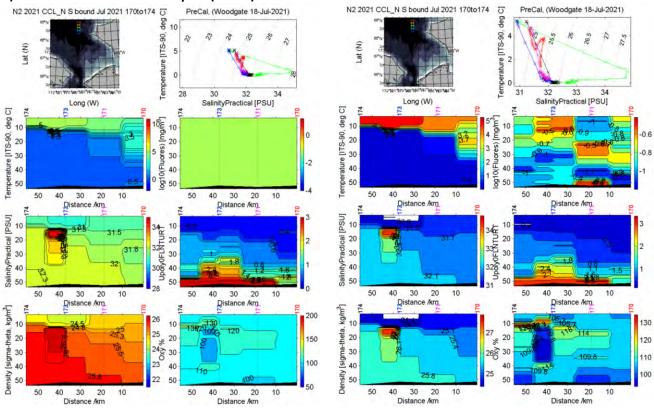
7) Cape Dyer line (CD) Eastward



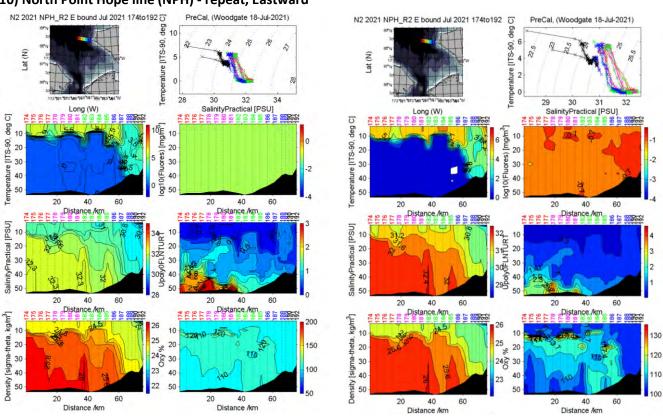
8) Cape Lisburne line (LIS) - Westward



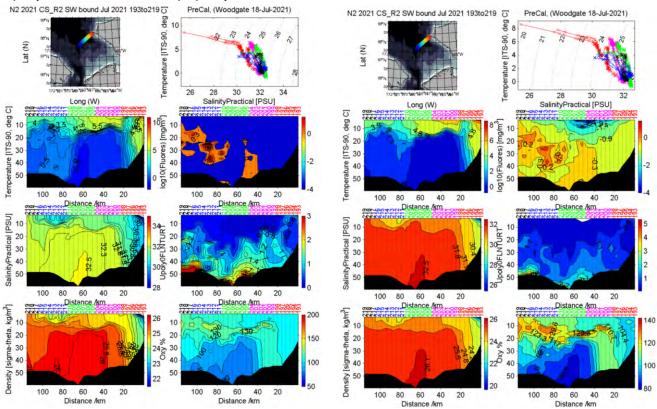
9) Chukchi Central line North part (CCL-N) - southward



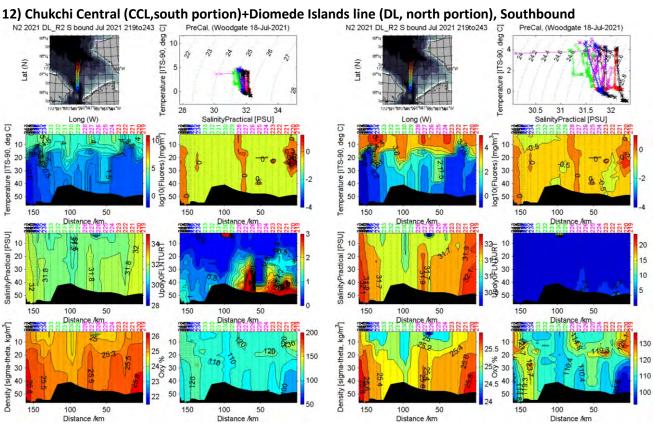
10) North Point Hope line (NPH) - repeat, Eastward



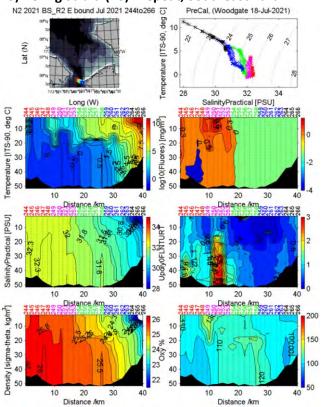
11) Cape Serdtse-Kamen line (CS) - repeat, Southwestward

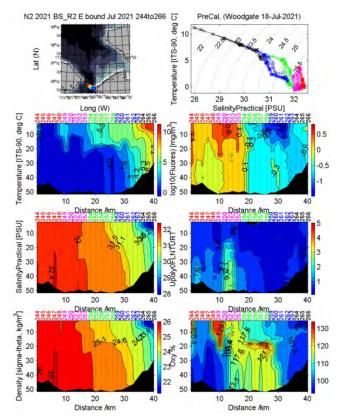


12) Chukchi Central (CCL, south portion)+Diomede Islands line (DL, north portion), Southbound

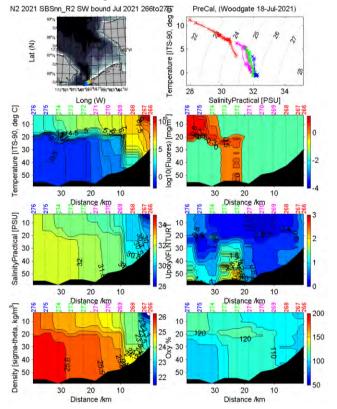


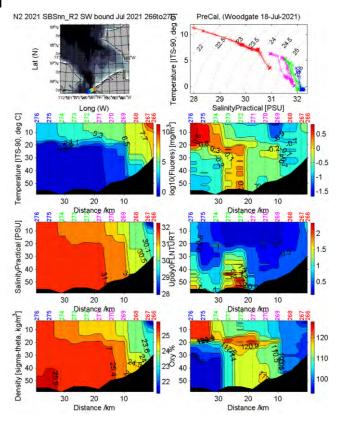
13) Bering Strait (BS) - repeat, Southeastward





14) South Bering Strait (new) (SBSnn) - southeastward



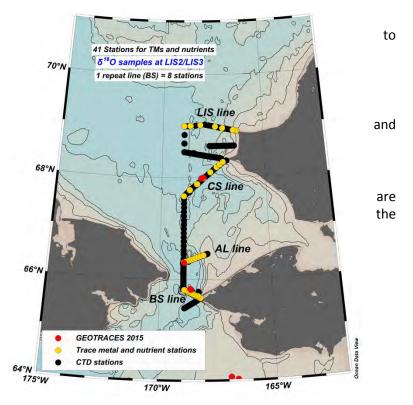


BERING STRAIT 2021 TRACE METAL AND NUTRIENT PUMPING AND DELTA O18 REPORT (Laramie Jensen)

Summary: 41 stations (33 separate locations) were sampled for trace metals and nutrients (yellow dots in map below), 78 trace metal samples and 76 nutrient samples collected at the surface (5m) and lower layer (variable depending on bottom depth), 2 samples for δ^{18} O (LIS2 and LIS3 surface only).

Background: The objective of this sampling is take high quality/high resolution trace metal (iron, zinc, nickel, copper, cadmium, manganese, lead) and macronutrient (nitrate, phosphate, silicate) samples alongside the CTD and mooring temperature salinity sampling. Trace metals (found in small or trace concentrations, ~10⁻⁹mol/L) may be useful in deciphering water mass circulation or provenance. Many, like iron, biologically important for phytoplankton in surface waters. Importantly, the Bering and Chukchi shelves provide a large source of these trace metals to the Western Arctic Ocean.

Moreover, the inventory of these trace metals appears to increase moving from the North Pacific/Bering Sea through the Bering Strait and onto the Chukchi Shelf. Sources for these metals are primarily sediment



resuspension (export of organic matter to the sediments releases trace metals through diagenesis or non-reductive dissolution) or riverine input. Freshwater intrusions (salinity <30psu) were observed frequently through the CTD transects, especially along the Alaskan coast at Stations LIS1-3. Rivers may act as a source or diluent for metals and nutrients. Variations in temperature and salinity indicate the presence of multiple water masses along the CTD lines sampled. The major objective of the high-resolution sampling is to assess if or to what extent trace metals and nutrients vary across these different water masses feeding into the Bering Strait, both spatially and in time. Trace metals could be used to trace water mass movement further north where currents are complicated by bathymetric features and become more difficult to track.

Pump sampling of trace metals: Sampling was done using a trace metal clean PTFE double diaphragm pump (manufacturer: Wilden, see picture below) with a maximum flow capacity of 56 liters/minute using the ship's 125 psi air supply. Tubing both in and out of the water was Grainger 1/2in OD (polyethylene) connected to the pump with PVDF 1/2in compression fittings (all acid cleaned prior to the cruise). Tubing was cut to ~70m and marked with tape up to 60m from the surface and attached along its length to 3/8in Nylon line. An 8lb kettleball weight was attached directly to the Nylon rope and a RBR Concerto³ CTD (measuring temperature, conductivity, pressure and oxygen every 0.125 s) was lashed to the rope below the end of the pipe with Dynacon line (see figure). Thus the end of the tubing sat approximately 1.5m above the kettleball weight. The depth of the end of the tubing in the water was estimated from the length of tube placed in the water, and post-cast, ascertained from the pressure record of the RBR CTD. Typically, the desired "bottom" depth was 5m shallower than the bottom depth as determined by the ship altimeter.

Air was supplied by the ship service air connection on the starboard side and pressure was ultimately controlled using an air regulator (see picture) before entering the pump. Pumping at maximum capacity, the pump cleared the pipe in 60-70 seconds, this being estimated by introducing a bubble before each cast to mark "new water" being sampled. Thus, before each surface and deep sample the pump was flushed for at least 65 seconds at maximum capacity/speed.

At every station the tube/rope/CTD/weight apparatus was lowered to the desired depth and the pump was turned, pushing water through the tubing via the diaphragm pump. After the flush had occurred, the clamps on the C-flex tubing were adjusted such that the flow of seawater from the pump was directed primarily through the Acropak capsule filter (described below). Immediately following collection of the trace metal and nutrient samples (both filtered) the pump was turned off on deck and the tubing apparatus was either recovered or moved to a new depth location (ie after the surface sample at 5m, tubing apparatus was moved directly to the "bottom" depth). After both casts (surface and bottom) the tubing apparatus was recovered back on deck, the pump was turned off, and the filter was placed back into the bag. The entire system was left on deck during a sampling line. Location and times of stations samples are marked Laramie stations in the cruise event log attached to this report.

Water was filtered before collection in sample bottles to remove particulates and organic material. Both the filtered and unfiltered flow were attached to the main Grainger tubing via a plastic Y-split connected to acid-cleaned C-flex tubing. Connections along the C-flex were reinforced with zipties and plastic hose clamps. Flow between the two was controlled by opening and shutting plastic snap clamps around the C-flex. Early in the cruise, it was determined that the maximum capacity of the pump would exceed the pressure capacity of the Acropak-200 0.2 μ m filter (shown below). Thus, after flushing the system, pressure was reduced to ~80 psi via the regulator and the filtered flow was only slightly restricted so that the Acropak filter could be filled and flowing enough to sample but not creating significant back pressure. When the filter was significantly clogged (particularly along LIS line) the gas lock of the filter capsule was opened to help alleviate pressure. The filter was stored in two small polybags and another larger poly bag with the rest of the outflow tubing (see figure below) to reduce contamination.

Filtered samples (trace metals (TM) and nutrients (nuts)) were filtered directly into 250 mL (TMs) and 60 mL (nuts) Nalgene bottles (pre-cleaned) following 2-3 10% volume rinses as water budget allowed. Samples were double bagged in poly bags. Nutrient samples were placed in -20°C freezer inside another poly bag within 4 hours of sampling. Trace metal samples were double bagged in poly bags in increments of 12. Nutrient samples remained frozen until they could be analyzed in the Marine Chemistry Lab at the University of Washington. Trace metal samples were all acidified to pH 1.8 using 500 μ L of Optima HCl (12M) under a Class 100 laminar flow hood (OSB 443) on 7/18/2021. Note that volume was estimated for incomplete samples (clearly less than 250 mL volume) and acidification volume was adjusted accordingly (i.e., if only 50 mL of seawater was collected, 100 μ L of Optima HCl was used). This occurred for the following samples: AL18.5 surf, CS12 surf, and BS13 (repeat) surf due to sample loss during sampling/storage.

Trace metal samples will be analyzed at the University of Washington in the Bundy Lab in the Fall of 2021.

O18 samples: Given the remarkable freshness of water around the east end of the LIS line, 2 opportunistic samples were taken for delta O18 analysis. Two samples, both surface, were collected in 250 mL low density polyethylene bottles (Nalgene). The bottles were acid cleaned with hydrochloric and nitric acid (and thoroughly rinsed with MQ water) before the cruise. Samples taken from the surface pumping at LIS2 and LIS3. Bottles were rinsed three times, filled to overflow, and sealed with parafilm, and stored at room temperature. These samples were analyzed by Andy Schauer at the ISOLAB in the Earth and Space Science (ESS) department of the University of Washington and reported below. Data suggests more freshwater in LIS3 surface sample compared to LIS2 but high values overall.

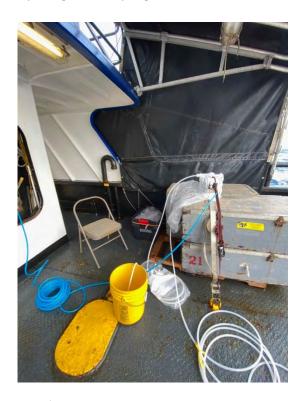
Date of analysis	Sample	Mean H2O (ppmv)	StdDev	Mean dD VSMOW	StdDev	Mean d180 VSMOW	StdDev
8/3/21 22:12	LIS3	19566	166.5983	-33.3819	0.098396	<mark>-4.2915</mark>	0.019424
8/4/21 1:19	LIS2	19574.6	61.476	-23.657	0.16012	<mark>-3.0929</mark>	0.025762
8/4/21 22:03	LIS2	19615	106.066	-23.6629	0.094302	<mark>-3.1141</mark>	0.020107
8/5/21 1:09	LIS3	19544	57.8835	-32.6919	0.21168	<mark>-4.2751</mark>	0.015659
Average	LIS2	19594.8	122.594	-23.65995	0.18582594	<mark>-3.1035</mark>	0.03267984
	LIS3	19555	176.3675	-33.0369	0.23343135	<mark>-4.2833</mark>	0.02494987

The full Delta018 analysis is included as an appendix to this report.

Issues encountered during trace metal/nutrient sampling:

- **Back pressure on filters**: As described above, the max pressure output of 125 psi from the Wilden pump was too high for the Acropak capsule filters.
 - Solution(s) at sea: Reduced pressure to ~80 psi when actively sampling. Also, only slightly closed
 the unfiltered tubing so that some pressure was relieved via that route. Tubing was reinforced
 with zipties rather than plastic hose clamps.
 - o **In the future:** Larger capacity capsule filters (1500 vs 200 cm² effective filtration area) will help with this issue as well as stronger tubing that is pre-attached to the Y-split mechanism so time does not have to be spent changing the tubing and reinforcing the joints.
- Filters clogging: The Acropak capsule filters "took on color" and became noticeably clogged sometimes after only ~1L of water was passed through. This meant that the back pressure on the filter was increased causing the tubing to disconnect or form a pocket of seawater resembling a water balloon. Only four 200 size capsule filters were brought and every one of them was used. This problem was especially noticeable on the BS (repeat) and LIS lines.
 - Solution(s) at sea: Sometimes the airlock on the Acropak capsule filter was opened to help relieve the back pressure. Likewise, the unfiltered side was also opened to prevent the C-flex tubing from swelling. Filter use was budgeted for the most important lines.
 - o **In the future:** Larger capacity Acropak filters, while expensive, make more sense for this environment. Decreasing the pressure on the pump further may also help.
- End of tubing staying clean: The ship's crew did an excellent job of making sure the end of the tubing attached to the Nylon rope did not hit the side of the ship upon recovery. However, this meant that when recovering the weight/CTD/end of the tubing one must lean out over the side of the ship and not use the ship railing as a counterbalance.
 - In the future: As suggested by a crewmember, consider building some sort of plastic cage/enclosure to have on the very end so that the tubing could remain protected during recovery.
- Hauling in the apparatus: One 8lb weight plus the 1.5 kg (3.3 lbs) RBR CTD was about at the limit for one person to haul in comfortably and repeatedly However, sometimes the weight was not enough to get the tubing down to the desired depth.
 - o **In the future:** Reconsider using a block and A-frame for tubing sampling. This may not be possible for quick deployment/recovery purposes, and may in any case squash the tubing.
- Trace metal cleanliness: Ideally, sampling would be done in a clean, positive pressure environment, but this was not available on this ship. Occasionally, filter apparatus and sample bottles were exposed to seaspray, water on the deck, surfaces inside the ship, or ungloved hands.
 - Solutions at sea: Using plastic bags and gloves as much as possible to protect samples from potential contamination.

In the future: Trying to set up a small environment on the ship where samples could be rebagged or sorted in a clean way. Even better, creating a way for the entire sampling process to be done indoors in a clean space. Some ideas for this include having the tubing go through a window or other opening and sampling into the sink in a small "bubble" environment.



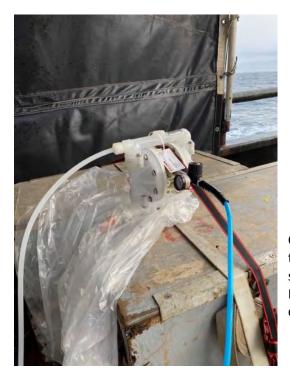
View of trace metal pump sampling on deck

View of trace metal pump sampling on deck





View of coiled rope and tubing with tape markings (left) and mini RBR CTD (red, white, black). Bucket used to collect unfiltered flow during flushing with shackle attached to restrict the "bouncing" of the white C-flex tubing that occurs due to the pump pressure.



Close up of pump with air regulator and air hose (blue) sitting on the mooring release pallets. It was necessary to use a ratchet strap to stabilize the pump so it did not move during sampling. Plastic bags were used as an extra precaution against contamination.



Clogged/used Acropak 200 (0.2um) filter. Top is the barbed connection that would be attached to the white C-flex tubing. To the right is the air valve that was opened during flushing to prevent bubbles from clogging the filter. Note that the folded Supor filter inside the capsule is dark green/brown after sampling.

BERING STRAIT 2021 UNDERWAY DATA REPORT – Woodgate (UW)

Underway CTD, ADCP and some meteorological data were collected during the cruise using the Norseman II's ship-based systems. These systems are set up by the Norseman II crew at the start of the cruise. Action item: Pre-cruise, develop checksheets for the setup of these instruments to ensure settings are as desired. Check the setups as soon as the ship leaves port.

ADCP: This year, as last year, we collected data from the Norseman II's Teledyne RD Instruments 300kHz Workhorse Mariner ADCP (SN 19355), which is equipped with high accuracy bottom tracking. The ADCP is mounted 3m below the water line. This system was operational for the cruise, running with 1m bins and bottom track. The following file types are available for processing (file information copied from http://po.msrc.sunysb.edu/SBI/Healy_ADCPs.htm)

- *.ENR raw binary ADCP data which contains every ping
- *.ENS Binary ADCP data after the data has been preliminarily screened for backscatter and correlation
- *.ENX Binary ADCP data after screening and rotation to earth coordinates
- *.STA Binary ADCP ensemble data that has been averaged into short term averages
- *.LTA Binary ADCP ensemble data that has been averaged into long term averages
- *.N1R Raw NMEA ASCII data from the primary navigation source
- *.N2R Raw NMEA ASCII data from the secondary navigation source, if available, and which should include Ashtech heading data
- *.NMS Binary screened and averaged navigation data
- *.VMO This ASCII file is a copy of the *.ini options file that was used during the data collection
- *.LOG ASCII file containing a log of any errors the ADCP detected during the session

Preliminary data plots will be added to this report once available. Bottom track data was logging during this deployment. Action item: Ensure that bottom tracking is turned on. Process ADCP data. Note also that since heading information is given by the ship's GPS position, it is not necessary to correct for magnetic declination. Action item: Check prior data for magnetic declination issue.

MET DATA: The Norseman2 had South Central Radar install a new Meteorological sensor package this year, as the previous sensors failed. The new version is an Airmar 220WX instrument Weather caster 153 (https://www.airmar.com/weather-description.html?id=153, https://www.airmar.com/uploads/InstallGuide/17-461-01.pdf) running WeatherCaster 3 software. Although the system was not logging data on the transit from Homer to Nome, by Nome logging of the 1s NMEA string was enabled. On the morning of the 7th July 2021 (before the science party arrived), the Norseman2 performed a compass calibration of the system off Nome. calibration calls for calm seas, which were not available, but is believed to have delivered a direction calibration good to about 10deg. The system is designed to provide apparent and theoretical (i.e. true?) wind speed and direction, air and wind chill temperature, pressure and (optional but included) humidity, using acoustic sensors and its own 3D compass. This information is sent in the NMEA \$IMDA string. Since the navigation NMEA strings are also stored, it should be possible to extract this information in conjunction with ship's motion information. From the hourly observations of wind, the consensus on the ship was that the speed readings may be too high. Also, temperature and wind chill temperature were always the same, suggesting some problem in these data streams. Further investigation was not possible at sea.

Action items: Extract desired information from stored NMEA strings. Quality control especially wind speed and temperature data where possible (e.g., where ship changes direction). Compare against weather prediction models.

For most of the cruise with brief exceptions during the AL and LIZ lines, the winds appeared to be mostly from the south, with extreme weather experienced during the CS line, before the final BS line and during the final BS and SBSnn lines and on the transit back to Nome at the end of the cruise.

Action item: Add meteorological data plots to this report.

AFT A-FRAME GPS: Two issues were encountered with the Aft Aframe GPS;

- a) wiring to the Aframe was faulty, Thus early in the cruise the GPS was remounted on the aft rail of the O1 deck.
- b) the GPS unit was reporting dates in November 2001 instead of 2021. This appears to be the GPS week number roll over issue, viz. an ambiguity in date because of the GPS week counter is only stored to a certain number of digits. Thus, for most systems (CTD, and underway), the forward GPS position was used.

UNDERWAY TEMPERATURE AND CONDUCTIVITY DATA: The Norseman II used an Seabird SBE21 temperature conductivity sensor mounted 3.4m below the water line (slightly to port of the ship's ADCP, in the center of the ship) to collect underway data throughout the cruise, also logging position information and depth. A separate temperature sensor (SBE38) is placed closer to the intake to measure the temperature (recorded as temperature 2) before it is warmed by the ship. Action item: Ensure depth is always logged in this file. An hourly watch was kept on these data to ensure no loss of data. Action item: Continue hourly monitoring of underway data while at sea. Check the temperature and salinity data to the CTD casts.

During the transit to Nome, when the system was originally turned on, the SBE38 data stream appeared to be all dummy values. However, without making any apparently significant change, the data stream appeared to correct itself and was being correctly recorded for the main cruise period. Action item: Investigate.

As for some of the transit to Nome this system used the aft-GPS, correction must be made on those data for the GPS week number roll over issue. Additionally, at times the system time was not set to UTC. However this string is only recorded in the header file of the data - the timestamp of the data is taken from the NMEA string, which always had the correct UTC time, but sometimes the wrong date. **Action item: Correct calibrated data for clock issues.**

The calibration file used was the December 2016 calibration. **Action item: Ensure the most recent calibration is used in the field.** Data were logged every 3 seconds.

Preliminary plots of the underway temperature and salinity data are given below.

It is very important to remember when interpreting these data, that they are taken over the many days of the cruise, and the oceanographic conditions change significantly during this time, as is evidenced by the plots of the various crossings of the Bering Strait also shown below. **Action item: Examine surface salinities and temperatures, especially in conjunction with prior data.**

For dates and times, see cruise schedule at start of report.

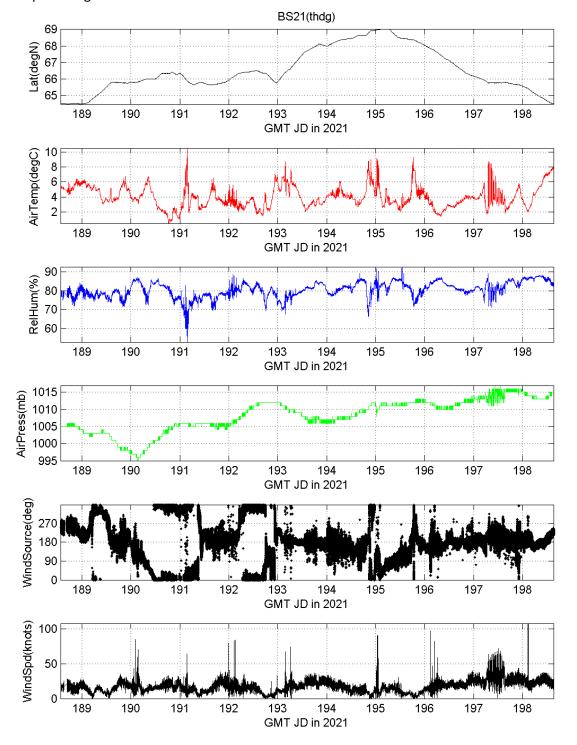
BERING STRAIT 2021 METEOROLOGICAL DATA PLOTS

Preliminary analysis (and comparison to ERA, JRA and NCEPdata suggests in this year are reading:

- too high for wind speed (by about 2m/s on average, i.e., about 4 knots)
- too low for temperature (by about 2degC on average)
- too low for pressure (by ~ 2hPa).

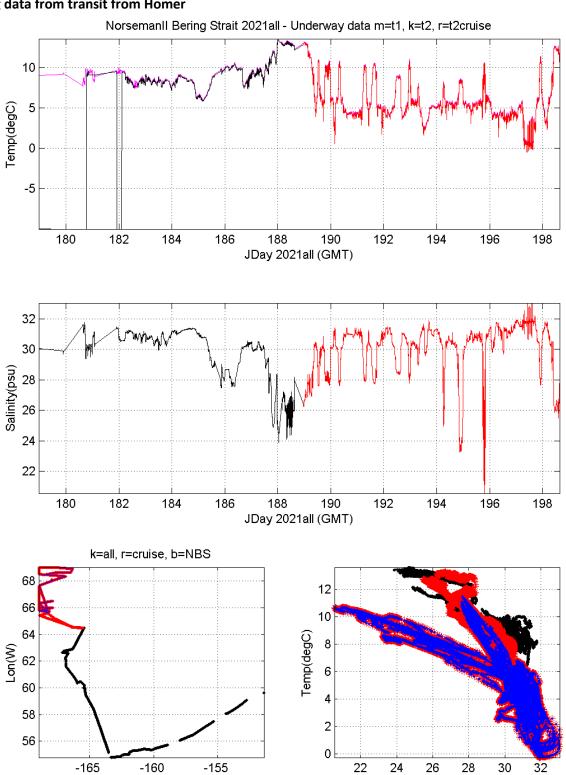
These differences are all greater than the stated accuracy of the sensor https://www.airmar.com/weather-description.html?id=153 (0.5m/s for speed; 1.1degC for temperature, 0.5hPa for pressure).

Note the nstrument calculates true wind direction and speed (and this is not reproducible exactly from relative wind and ship heading



BERING STRAIT 2021 UNDERWAY TEMPERATURE SALINITY DATA

Including data from transit from Homer

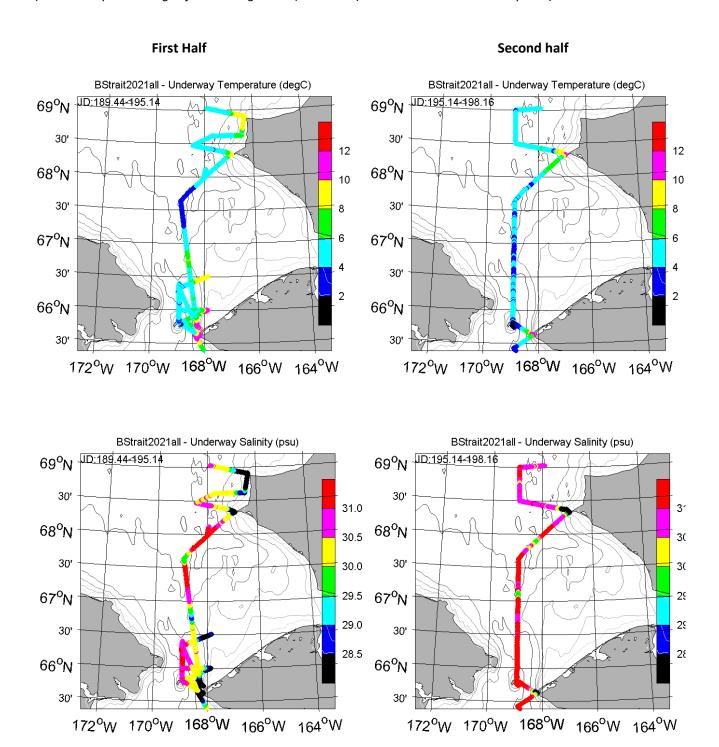


Lat(N)

Salinity(psu)

BERING STRAIT 2021 UNDERWAY TEMPERATURE SALINITY DATA (continued)

(Note multiple runnings of the Bering Strait (and other) lines are masked in these plots.)

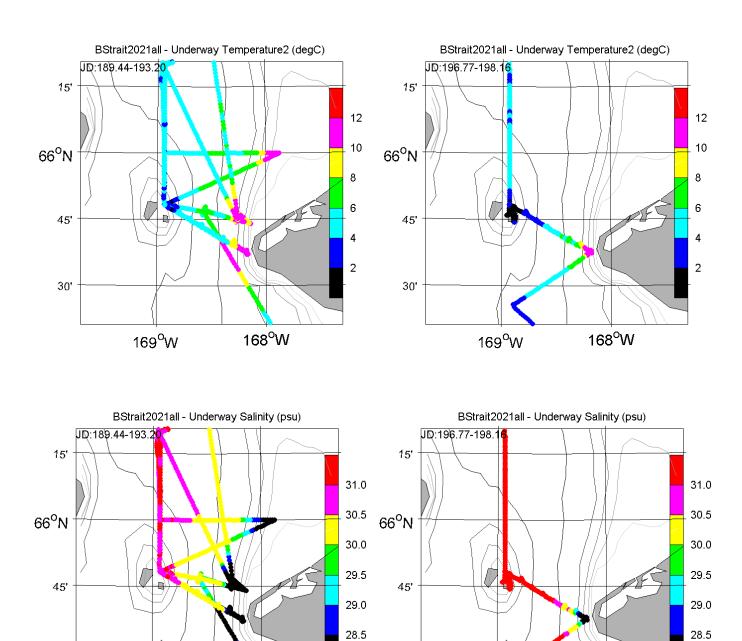


30'

169°W



Second half



30'

169⁰W

168°W

168°W

BERING STRAIT 2021 TARGET CTD POSITIONS

```
% Stations for BStrait Mooring Cruise 2021 NorsemanII
% Vers: 25<sup>th</sup> July 2021
%
% US-Russian convention line is at 168deg 58.7'W.
% All stations in this file are in US waters.
% (Let me know if any points are too close to border for you.)
%
% Time estimates are based on the 2013 NorsemanII cruise.
% INCLUDING NEW LINES FROM 2017 CRUISE, viz
% - higher res DL north
% - higher res A3L
% - higher res SBS
% - LIS redone to avoid cable at LIS9
% ***** MOORING POSITIONS *****
% In likely order of servicing, i.e.,
% - recoveries from east to west in strait, then northern site;
% - deployments northern site, the west to east in strait.
% == 3 moorings to recover
% == 3 moorings to deploy
%-----
% RECOVERIES of moorings deployed in 2019
%-----
%NAME
        Lat(N)
                Long (W) Water Top
     deg min deg min
                     depth Float
% A3-19 66 19.604 168 57.046 57m
                               8m
% A2-19 65 46.855 168 34.070
                          56m
                               16m
% A4-19 65 44.748 168 15.765 48m 16m
% RECOVERIES of moorings deployed in 2020
%-----
%NAME Lat(N)
               Long (W) Water Top
                      depth Float
     deg min
              deg min
%
% A3-20 66 19.604 168 57.604 57m
                               43m
% A2-20 65 46.858 168 34.598
                          56m
                               46m
% A4-20 65 44.750 168 16.310 50m 37m
%-----
% DEPLOYMENTS for this 2021 cruise
%-----
% Target same as 2012 positions.
%NAME Lat(N)
              Long (W)
                       Water
    deg min
             deg min
                     depth
% A3-21 66 19.61 168 57.05 58m
% A2-21 65 46.86 168 34.07 56m
```

```
% A4-21 65 44.75 168 15.77 49m
%-----
% INTERMOORING DISTANCES
%-----
% A2 - A4 ~ 8nm
%-----
% To A3 from
%-----
% A2 - 34nm
% A4 - 39nm
%-----
% To Nome from
%-----
% A4 - 120nm
% CS1 - 200-220nm
% ***** HISTORIC CTD SECTIONS *****
% There are 14 historic CTD lines here.
% These are the same positions as suggested in 2017, with
% the addition of 3 lines run in 2017 and the moving of
% one line (a change also made on the 2017 cruise).
% We may not have time for all of these, in which case
% we will do a subset. But I've included
% them all, so you have the positions in advance.
% If operations/science dictate, then there
% might be different lines proposed while at sea.
% Naming is based on historic data.
% "+net" also refers to historic operations and
% is not relevant for this cruise.
% "no bottles" refers to historic operations and
% is not relevant for this cruise. (No bottles
% will be taken on any CTD casts of this cruise.)
% Known Hazards are indicated.
%
% Stay a safe distance (300m?) from all deployed
% moorings.
% Except for around moorings or for mooring work,
% within 200m is ok for positions.
%
% BS = Bering Strait Line (US portion)
% - 15 stations
% - station spacing generally ~ 2nm
```

```
% Distances: - BS11-BS22 21.7nm
       - BS22-BS24 3.1nm
% Total length 24.8nm
%--
% Time from NorsemanII, 6 hrs running W, 5 hrs running E
% Time from Khromov 10.5hrs
% Lat (N) Long (W) Lat (N) Long (W) Name
           deg min deg min
 65.805 168.933 65 48.31 168 55.96 % BS11
 65.788 168.860 65 47.26 168 51.62 % BS12
 65.772 168.794 65 46.33 168 47.64 % BS13
 65.755 168.721 65 45.28 168 43.29 % BS14
 65.739 168.663 65 44.35 168 39.80 % BS15
 65.722 168.591 65 43.29 168 35.46 % BS16 + net
 65.704 168.521 65 42.23 168 31.28 % BS17
 65.695 168.486 65 41.70 168 29.16 % BS17S
 65.686 168.449 65 41.18 168 26.94 % BS18
 65.672 168.391 65 40.35 168 23.44 % BS19
 65.655 168.318 65 39.29 168 19.09 % BS20
 65.642 168.250 65 38.53 168 14.97 % BS21
 65.625 168.177 65 37.48 168 10.63 % BS22 + net
 65.599 168.161 65 35.96 168 9.66 % BS23
 65.582 168.117 65 34.91 168 7.00 % BS24
%
%This might also be run at the extra high resolution
% of 2014, viz:
65.805 168.933
                     65
                            48.31
                                   168
                                           55.96
                                                 %
                                                         BS11
65.797 168.897
                     65
                            47.79
                                                         BS11.5
                                   168
                                           53.79
                                                  %
65.788 168.86 65
                     47.26 168
                                    51.62 %
                                                  BS12
                            46.8
65.780 168.827
                     65
                                    168
                                           49.63
                                                  %
                                                         BS12.5
65.772 168.794
                            46.33
                                           47.64 %
                     65
                                   168
                                                         BS13
65.764 168.758
                     65
                            45.81
                                   168
                                           45.47
                                                 %
                                                         BS13.5
65.755 168.721
                     65
                            45.28
                                   168
                                           43.29
                                                 %
                                                         BS14
65.747 168.692
                     65
                            44.82
                                   168
                                           41.55
                                                  %
                                                         BS14.5
65.739 168.663
                            44.35
                                           39.8
                     65
                                   168
                                                  %
                                                         BS15
                            43.82
                                           37.63
65.731 168.627
                     65
                                   168
                                                  %
                                                         BS15.5
65.722 168.591
                     65
                            43.29
                                   168
                                           35.46 %
                                                         BS16
65.713 168.556
                     65
                            42.76
                                   168
                                           33.37
                                                  %
                                                         BS16.5
65.704 168.521
                     65
                            42.23
                                   168
                                           31.28 %
                                                         BS17
65.695 168.486
                     65
                            41.7
                                    168
                                           29.16
                                                 %
                                                         BS17.5
                            41.18
65.686 168.449
                     65
                                   168
                                           26.94
                                                  %
                                                         BS18
65.679 168.42 65
                     40.77
                            168
                                    25.19
                                           %
                                                  BS18.5
                            40.35
65.672 168.391
                     65
                                   168
                                           23.44
                                                  %
                                                         BS19
65.664 168.355
                     65
                            39.82
                                   168
                                           21.27
                                                  %
                                                         BS19.5
65.655 168.318
                     65
                            39.29
                                   168
                                           19.09
                                                  %
                                                         BS20
65.649 168.284
                     65
                            38.91
                                   168
                                           17.03
                                                  %
                                                         BS20.5
                            168
65.642 168.25 65
                     38.53
                                    14.97
                                           %
                                                  BS21
65.634 168.214
                            38.01
                     65
                                   168
                                           12.8
                                                  %
                                                         BS21.5
65.625 168.177
                     65
                            37.48
                                   168
                                           10.63
                                                  %
                                                         BS22
```

```
65.599 168.161
                  65
                         35.96 168
                                     9.66
                                            %
                                                  BS23
65.582 168.117
                   65
                         34.91 168
                                     7
                                            %
                                                  BS24
%
%
%===========
% AL = A3 Line (US portion)
%==========
% Hazards on this line:
% == First station on this line is at mooring A3-17, so exact
% position needs to be altered to be a safe distance (300m?)
% from mooring A3-17 site.
%-----
% - 13 stations including cast at A3mooring site
% - station spacing ~ 1.9nm
% Distance: - A3 to AL24 = 22.2nm
% --
% Time from NorsemanII ~5.5hrs
% Time from Khromov ~9hrs
%-----
% Lat (N) Long (W) Lat (N) Long (W) Name
          deg min
                  deg min
 66.327 168.951 66 19.61 168 57.05 % A3-17
% *** Adjust this first position to be safe distance (300m?) from A3-17
 66.340 168.895 66 20.39 168 53.71 % AL13
 66.352 168.823 66 21.09 168 49.40 % AL14
 66.363 168.752 66 21.80 168 45.09 % AL15
 66.375 168.680 66 22.51 168 40.78 % AL16
 66.387 168.608 66 23.21 168 36.47 % AL17 + net
 66.399 168.536 66 23.92 168 32.16 % AL18
 66.410 168.464 66 24.63 168 27.84 % AL19
 66.422 168.392 66 25.33 168 23.53 % AL20
 66.434 168.320 66 26.04 168 19.22 % AL21
 66.446 168.249 66 26.75 168 14.91 % AL22 + net
 66.458 168.177 66 27.45 168 10.60 % AL23
 66.469 168.105 66 28.16 168 6.29 % AL24
%
%
% CS = Cape Serdtse Kamen to Point Hope Line (US portion)
% Hazards on this line:
% == Final station CS19 is shallow. Check on
% modern charts to see if deep enough for Norseman II.
% (this station was too shallow for the Khromov, but
% was ok for the NorsemanII in 2013).
%-----
% - 16 or 17 stations
% - station spacing ~ 5nm in the central Chukchi,
         ~ 2.2nm near the coast
% Distances: - CS10US to CS18 60.8nm
```

```
%
      - CS18 to CS19 2.2nm
%--
% Time from NorsemanII (toCS19) ~ 10.5 hrs
% Time from Khromov (toCS18) ~12hrs
%-----
% Lat (N) Long (W)
                    Name
% deg min deg min
0 0 67 38.1 168 56.0 % CS10US + net
0 0 67 41.7 168 48.1 % CS10.5 - no bottles
0 0 67 45.3 168 39.9 % CS11
0 0 67 48.9 168 29.4 % CS11.5 - no bottles
0 0 67 52.5 168 18.8 % CS12 + net
0 0 67 55.9 168 9.1 % CS12.5 - no bottles
0 0 67 59.3 167 59.4 % CS13
0 0 68 2.7 167 49.7 % CS13.5 - no bottles
0 0 68 6.1 167 39.9 % CS14 + net
0 0 68 9.1 167 30.7 % CS14.5 - no bottles
0 0 68 12.1 167 21.4 % CS15
0 0 68 13.6 167 16.8 % CS15.5 - no bottles
0 0 68 15.0 167 12.2 % CS16
0 0 68 16.6 167 7.6 % CS16.5 - no bottles
0 0 68 18.0 167 2.9 % CS17 + net
0 0 68 18.9 166 57.6 % CS18
0 0 68 19.9 166 52.3 % CS19 *** SHALLOW **
%
        CS19 too shallow for Khromov.
%
%
% DL = Diomede Line (US only, 1nm east of border)
% This line is to map eddying area north of the Diomedes
% - 19 stations
% - station spacing ~ 1nm in South,
         ~ 2.5nm in north
% Distance: - DL1 to DL19 28.7nm
%--
% Time from NorsemanII - 5.5 hrs running N; 9hrs running S
% Time from Khromov to DL19 ~10hrs
%-----
% Lat (N) Long (W) Name
% deg min deg min
0 0 65 49.28 168 56.2 % DL1
0 0 65 50.26 168 56.2 % DL2
0 0 65 51.23 168 56.2 % DL3
0 0 65 52.21 168 56.2 % DL4 + net
0 0 65 53.18 168 56.2 % DL5 - no bottles
0 0 65 54.15 168 56.2 % DL6
0 0 65 55.13 168 56.2 % DL7 - no bottles
0 0 65 56.10 168 56.2 % DL8
0 0 65 57.08 168 56.2 % DL9 - no bottles
```

```
0 0 65 58.05 168 56.2 % DL10
0 0 65 59.03 168 56.2 % DL11- no bottles
0 0 66 0.00 168 56.2 % DL12
0 0 66 2.55 168 56.2 % DL13- no bottles
0 0 66 5.10 168 56.2 % DL14
0 0 66 7.65 168 56.2 % DL15- no bottles
0 0 66 10.19 168 56.2 % DL16
0 0 66 12.74 168 56.2 % DL17- no bottles
0 0 66 15.29 168 56.2 % DL18
0 0 66 17.84 168 56.2 % DL19- no bottles
%
%
% DL A and B lines (Diomede A and B lines)
% These lines, with DL, form a grid to map
% eddying N of the Diomedes.
% - each line 12 stations
% - station spacing ~ 1nm
% Distances: - each line ~ 11nm
%--
% Estimate for NorsmanII for each line ~3.5hrs
% Time from Khromov for each line ~5hrs
%-----
  Lat (N)
            Long (W) Name
  deg min
             deg min
% Northbound leg
0 0 65 49.30 168 52.2 % DLa 1
0 0 65 50.27 168 52.2 % DLa 2
0 0 65 51.25 168 52.2 % DLa 3
0 0 65 52.22 168 52.2 % DLa 4
0 0 65 53.19 168 52.2 % DLa 5
0 0 65 54.16 168 52.2 % DLa 6
0 0 65 55.14 168 52.2 % DLa 7
0 0 65 56.11 168 52.2 % DLa 8
0 0 65 57.08 168 52.2 % DLa 9
0 0 65 58.05 168 52.2 % DLa 10
0 0 65 59.03 168 52.2 % DLa 11
0 0 66 0.00 168 52.2 % DLa 12
% Southbound leg
0 0 66 0.00 168 48.2 % DLb 12
0 0 65 59.03 168 48.2 % DLb 11
0 0 65 58.05 168 48.2 % DLb 10
0 0 65 57.08 168 48.2 % DLb 9
0 0 65 56.11 168 48.2 % DLb 8
0 0 65 55.14 168 48.2 % DLb 7
0 0 65 54.16 168 48.2 % DLb 6
0 0 65 53.19 168 48.2 % DLb 5
0 0 65 52.22 168 48.2 % DLb 4
0 0 65 51.25 168 48.2 % DLb 3
```

```
0 0 65 50.27 168 48.2 % DLb 2
0 0 65 49.30 168 48.2 % DLb 1
%
%
% AS = from AL to CS Line
% Across-topography line linking Al line with CS
% - 20 stations (counting first of CS line)
% - station spacing
%
     AS1-7 at ~ 4nm spacing.
%
     AS7-14 at 2nm spacing,
%
     A14 to end 4nm
% Distances: - AS1 to CS10 64.7nm
%--
% Time from Khromov (12casts, odds+2&18) ~11hrs
% Estimate for NorsmanII 20 casts ~ 12hrs
% Estimate for Khromov 20 casts ~ 14hrs
  Lat (N)
            Long (W)
                       Name
   deg min
             deg min
0 0 66 41.47
             167 38.86 % AS 1
0 0 66 45.01
             167 43.78 % AS 2-no bottles
0 0 66 48.55
             167 48.70 % AS 3
0 0 66 52.09
             167 53.62 % AS 4-no bottles
0 0 66 55.63
             167 58.55 % AS 5
0 0 66 59.17 168 3.47 % AS 6-no bottles
0 0 67 2.71 168 8.39 % AS 7
            (2nm spacing over slope)
0 0 67 4.48
            168 10.85 % AS 8-no bottles
0 0 67 6.25 168 13.31 % AS 9
0 0 67 8.02
            168 15.77 % AS 10-no bottles
0 0 67 9.78
             168 18.23 % AS 11
0 0 67 11.55
             168 20.69 % AS 12-no bottles
0 0 67 13.32
             168 23.15 % AS 13
0 0 67 16.86 168 28.07 % AS 14
            (back to 4nm spacing)
0 0 67 20.40 168 32.99 % AS 15-no bottles
0 0 67 23.94 168 37.92 % AS 16
0 0 67 27.48 168 42.84 % AS 17-no bottles
0 0 67 31.02
             168 47.76 % AS 18
0 0 67 34.56
             168 52.68 % AS 19-no bottles
0 0 67 38.10 168 56.00 % CS10US
%
%=============
% LIS = Cape Lisburne Line
%===========
% - 17 stations (including first of CCL line)
% - station spacing ~ 2nm near coast,
```

```
%
        ~ 3nm and ~ 5nm away from coast
% Distances: - LIS1 to CCL22 57.2nm
%--
% Time from NorsemanII, ~ 10hrs
% Time from Khromov ~11hrs
%-----
% Lat (N)
             Long (W) Name
   deg min
              deg min
0 0 68 54.40 166 19.80 % LIS 1 + net
0 0 68 54.80 166 25.15 % LIS 2
0 0 68 55.20 166 30.51 % LIS 3
0 0 68 55.80 166 38.54 % LIS 4
0 0 68 56.40 166 46.57 % LIS 5
0 0 68 57.00 166 54.60 % LIS 6 + net
0 0 68 57.60 167 1.95 % LIS 6.5 - no bottles
0 0 68 58.20 167 9.30 % LIS 7
0 0 68 58.80 167 16.65 % LIS 7.5 - no bottles
0 0 68 59.40 167 24.00 % LIS 8
0 0 69 0.60 167 38.70 % LIS 9
0 0 69 1.80 167 53.40 % LIS 10 + net
0 0 69 1.35 168 7.95 % LIS 11
0 0 69 0.90 168 22.50 % LIS 12
0 0 69 0.45 168 37.05 % LIS 13
0 0 69 0.23 168 46.62 % LIS 14n + net
0 0 69 0.00 168 56.00 % CCL22n % was 56.2
%
%
%============
% CCL = Chukchi Convention Line
%===========
% Hazards on this line:
% == First station on this line is the same as last station
% included in the LIS line above. It does not need to be
% repeated.
% == Last station on this line is at mooring A3-14, so exact
% position needs to be altered to be a safe distance (300m?)
% from mooring A3-14 site.
% == There are 2 JAMSTEC moorings ~ 3nm east of station
% CCL16 on this line. Those positions are:
% SCH13 68 2.002N 168 50.028W
% SCH13w 68 3.006N 168 50.003W
%-----
% Line running from northern most point
% due south, ~ 1nm US side of conventionline
% - 20 stations (counting arriving at A3-14)
% - station spacing ~ 10nm until CCL8,
   then reducing to ~5nm and ~2.5nm
% Distances: - CCL22 to A3-13 ~ 161nm
% Time from NorsemanII, 21.5hrs
```

```
% Time from Khromov ~26hrs
%-----
  Lat (N)
            Long (W) Name
%
   deg min
           deg min
0 0 69 0.0 168 56.0 % CCL22
0 0 68 50.0 168 56.0 % CCL21
0 0 68 40.0 168 56.0 % CCL20
0 0 68 30.0 168 56.0 % CCL19
0 0 68 20.0 168 56.0 % CCL18 + Net
0 0 68 10.0
            168 56.0 % CCL17
            168 56.0 % CCL16
0.00
0 0 67 50.0
            168 56.0 % CCL15
0 0 67 38.1
            168 56.0 % CCL14 (same as CS10US) + Net + Prod
%
            168 56.0 % CCL13
0 0 67 30.0
0 0 67 20.0
            168 56.0 % CCL12
0 0 67 10.0 168 56.0 % CCL11
0 0 67 00.0
            168 56.0 % CCL10 + Net
0 0 66 50.0 168 56.0 % CCL9
0 0 66 40.0 168 56.0 % CCL8
%
     - spacing now 5nm
0 0 66 35.0 168 56.0 % CCL7
0 0 66 30.0 168 56.0 % CCL6
0 0 66 25.0 168 56.0 % CCL5
    - spacing now 2.5nm
%
0 0 66 22.3 168 56.0 % CCL4
0 0 66 19.61 168 57.05 % A3-17
% *** Adjust this position to be safe distance (300m?) from A3-17
% Higher RES CCL Line S from CS10US
% (halves from 8.5 to 13.5 are new)
% 73nm ..
0 0 67 35.0 168 56.0 % CCL13.5
0 0 67 30.0 168 56.0 % CCL13
0 0 67 25.0
            168 56.0 % CCL12.5
0 0 67 20.0 168 56.0 % CCL12
0 0 67 15.0
            168 56.0 % CCL11.5
0 0 67 10.0 168 56.0 % CCL11
0 0 67 05.0 168 56.0 % CCL10.5
0 0 67 00.0 168 56.0 % CCL10 + Net
0 0 66 55.0
            168 56.0 % CCL9.5
0 0 66 50.0
            168 56.0 % CCL9
0 0 66 45.0
            168 56.0 % CCL8.5
0 0 66 40.0
            168 56.0 % CCL8
     - spacing now 5nm
%
0 0 66 35.0
            168 56.0 % CCL7
0 0 66 30.0
            168 56.0 % CCL6
0 0 66 25.0
            168 56.0 % CCL5
```

```
%
      - spacing now 2.5nm
0 0 66 22.3 168 56.0 % CCL4
0 0 66 19.61 168 57.05 % A3-17
% *** Adjust this position to be safe distance (300m?) from A3-17
%
% NBS - North Bering Strait line
% Hazards on this line:
% == Section crosses shallow waters.
% Beware of shallows from NBS9 and eastwards.
% (Helix diverted N to avoid shallows between
% stations NBS10 and NBS11)
% == Consider terminating line at NBS9
%-----
% Another cross strait line, run previously
% at lower resolution (i.e. without the 0.5 stations).
% - stations 9 (NBS1-9) to 16 (NBS1-9 with 0.5s)
% to 21 (full section, including shallows).
% - station spacing (with 0.5s) ~ 1.7nm
% Distance: - NBS1-9 25.8nm
%
      - NBS1-14 44.1nm
%--
% Time from Helix to NBS9, 9 casts ~5.5hrs
% - Estimate for NorsemanII to NBS9, 9 casts, 6hrs
% - Estimate for NorsemanII to NBS9, 16 casts, 7.5hrs
% - Estimate Khromov to NBS9, 9 casts ~6.5hrs
% - Estimate Khromo to NBS9, 16 casts ~8hrs
% Time from Helix to NBS14, 14 casts ~8.5hrs
% - Estimate for NorsemanII to NBS14, 14 casts, 9hrs
% - Esimate for NorsemanII to NSB14, 21 casts, 10.5hrs
% - Estimate Khromov to NBS14, 14 casts ~10hrs
% - Estimate Khromov to NBS14, 21 casts ~13hrs
   Lat (N)
             Long (W) Name
%
%
    deg min deg min
0 0 66 0.0 168 56.0 % NBS1 % was 58.1
0 0 66
        0.0 168 53.0 % NBS1.5
0 0 66
        0.0 168 49.9 % NBS2
0 0 66
        0.0 168 45.8 % NBS2.5
0 0 66
        0.0 168 41.6 % NBS3
0 0 66
        0.0 168 37.4 % NBS3.5
        0.0 168 33.2 % NBS4
0 0 66
0 0 66
        0.0 168 29.1 % NBS4.5
0 0 66
        0.0 168 25.0 % NBS5
0 0 66
        0.0 168 20.7 % NBS5.5
             168 16.4 % NBS6
0 0 66
        0.0
        0.0 168 12.4 % NBS6.5
0 0 66
0 0 66
        0.0 168 8.4 % NBS7
```

```
0 0 66
       0.0 168 4.2 % NBS7.5
0 0 66
        0.0 168 0.0 % NBS8 - 34m water
0 0 66 0.0 167 55.1 % NBS9 - 20m water
% (consider terminating line here)
0 0 66
        0.0
            167 52.0 % NBS10 - 12m water
% (Helix diverted N to avoid shallows between these stations)
0 0 66
        0.0 167 40.1 % NBS11 - 15m water
0 0 66
        0.0 167 29.1 % NBS12 - 18m water
00 66
        0.0 167 18.1 % NBS13 - 13m water
0 0 66 0.0 167 10.2 % NBS14 - 10m water
%
%
% MBSn = Mid Bering Strait line
% Just north of the Bering Strait line
% - 14 stations
% - station spacing 1.7nm, less near coast
% Distance: - 21.0nm total
%--
% Time from Helix (8casts only) ~2.5hrs
% - Estimate NorsemanII (8 casts only) ~ 4hrs
% - Estimate NorsemanII (14 casts) ~ 6hrs
% - Estimate Khromov (8casts only)~5.5hrs
% - Estimate Khromov (14casts) ~7hrs
  Lat (N)
            Long (W)
                     Name
%
   deg min
             deg min
0 0 65 52.1
             168 56.0 % MBSn1 % was 57.0
0 0 65 52.0
            168 52.5 % MBSn1.5
0 0 65 51.9
             168 49.1 % MBSn2
0 0 65 51.8
             168 45.0 % MBSn2.5
0 0 65 51.7
             168 40.9 % MBSn3
0 0 65 51.6
             168 36.4 % MBSn3.5
0 0 65
       51.5
             168 31.9 % MBSn4 % was 51.6
0 0 65 51.4
             168 27.5 % MBSn4.5
0 0 65 51.3
             168 23.0 % MBSn5 % was 51.4
0 0 65 51.2
             168 18.5 % MBSn5.5
0 0 65
       51.1
             168 13.9 % MBSn6
0 0 65 51.1
             168 10.4 % MBSn6.5
             168 6.9 % MBSn7
0 0 65 51.0
0 0 65 50.9
             168 5.0 % MBSn8
%
%
% North North Bering Strait Line (NNBS)
% A section across the ACC and main flow between
% the A3L line and the NBS line.
% With the 0.5s, at 1.76nm spacing
```

```
% 22.8nm length
%-----
% Run for the first time in 2015 - check water depths on
% the eastern (NNBS7.5) end)
% Dovetails with DL line. NNBS1 is the same as DL16
66.170 168.937 66 10.19 168 56.20 %NNBS1
66.170 168.865 66 10.19 168 51.88 %NNBS1.5
66.170 168.793 66 10.19 168 47.55 %NNBS2
66.170 168.721 66 10.19 168 43.23 %NNBS2.5
66.170 168.648 66 10.19 168 38.91 %NNBS3
66.170 168.576 66 10.19 168 34.58 %NNBS3.5
66.170 168.504 66 10.19 168 30.26 %NNBS4
66.170 168.432 66 10.19 168 25.94 %NNBS4.5
66.170 168.360 66 10.19 168 21.62 %NNBS5
66.170 168.288 66 10.19 168 17.29 %NNBS5.5
66.170 168.216 66 10.19 168 12.97 %NNBS6
66.170 168.144 66 10.19 168 8.65 %NNBS6.5
66.170 168.072 66 10.19 168 4.32 %NNBS7
66.170 168.000 66 10.19 168 0.00 %NNBS7.5
% Two new lines to map the ACC as and after it rounds Point Hope
% NPH - North Point Hope Line
%-----
% Crossing from Point Hope to the ENE roughly.
% - 11 stations,
% from 1-5 and 1.25nm spacing
% for the rest of the line at 2.5nm
% - Distance 21nm
% - new in 2016
% - ** CHECK DEPTH OF SHALLOWEST NPH1
% Run from east (NPH1) to west (NPH11)
% - estimate 3hrs 15min
%-----
% Lat (N) Long (W) Name
% deg min deg min
0 0 68 22.40 167 07.93 % NPH1
0 0 68 22.64 167 11.31 % NPH2
0 0 68 22.87 167 14.68 % NPH3
0 0 68 23.11 167 18.06 % NPH4
0 0 68 23.35 167 21.44 % NPH5
0 0 68 23.83 167 28.19 % NPH6
0 0 68 24.30 167 34.95 % NPH7
0 0 68 24.77 167 41.71 % NPH8
```

```
0 0 68 25.25 167 48.46 % NPH9
0 0 68 25.73 167 55.22 % NPH10
0 0 68 26.20 168 01.97 % NPH11
%
%
% CD- Cape Dyer
%-----
% Crossing east west, midway between Point Hope
% and Cape Lisburne (near Cape Dyer) and trying
% to avoid some topographic irregularites just
% N of the line on the charts.
% - 14 stations, 2nm spacing
% - Distance 26nm
% - new in 2016
% - ** CHECK DEPTH OF SHALLOWEST CD1
%-----
% Lat (N) Long (W) Name
% deg min deg min
0 0 68 37.00 167 41.0 % CD14
0 0 68 37.00 167 35.5 % CD13
0 0 68 37.00 167 29.9 % CD12
0 0 68 37.00 167 24.4 % CD11
0 0 68 37.00 167 18.8 % CD10
0 0 68 37.00 167 13.3 % CD9
0 0 68 37.00 167 7.8 % CD8
0 0 68 37.00 167 2.2 % CD7
0 0 68 37.00 166 56.7 % CD6
0 0 68 37.00 166 51.2 % CD5
0 0 68 37.00 166 45.6 % CD4
0 0 68 37.00 166 40.1 % CD3
0 0 68 37.00 166 34.5 % CD2
0 0 68 37.00 166 29.0 % CD1
% DL = Diomede Line EXTRAS(US only, 1nm east of border)
% This line is to map eddying area north of the Diomedes
% - 19 stations
% - station spacing ~ 1nm in South,
%
        ~ 2.5nm in north
% Distance: - DL1 to DL19 28.7nm
%--
% Time from NorsemanII - 5.5 hrs running N; 9hrs running S
% Time from Khromov to DL19 ~10hrs
% (The info about is withOUT the 0.5)*******
% Lat (N) Long (W) Name
% deg min
           deg min
```

```
0 0 66 0.00 168 56.2 % DL12
0 0 66 1.28 168 56.2 % DL12.5
0 0 66 2.55 168 56.2 % DL13
0 0 66 3.83 168 56.2 % DL13.5
0 0 66 5.10 168 56.2 % DL14
0 0 66 6.38 168 56.2 % DL14.5
0 0 66 7.65 168 56.2 % DL15
0 0 66 8.92 168 56.2 % DL15.5
0 0 66 10.19 168 56.2 % DL16
0 0 66 11.47 168 56.2 % DL16.5
0 0 66 12.74 168 56.2 % DL17
0 0 66 14.02 168 56.2 % DL17.5
0 0 66 15.29 168 56.2 % DL18
0 0 66 16.57 168 56.2 % DL18.5
0 0 66 17.84 168 56.2 % DL19
0 0 66 18.73 168 56.2 % DL19.5
%
%
%============
% AL = A3 Line (US portion) - with extras
%==========
% Hazards on this line:
% == First station on this line is at mooring A3-17, so exact
% position needs to be altered to be a safe distance (300m?)
% from mooring A3-15 site.
%-----
% - 13 stations including cast at A3mooring site
% - station spacing ~ 1.9nm
% Distance: - A3 to AL24 = 22.2nm
% --
% Time from NorsemanII ~5.5hrs
% Time from Khromov ~9hrs
% (The info about is withOUT the 0.5)******
%-----
% Lat (N) Long (W) Lat (N) Long (W) Name
          deg min
                  deg min
%
 66.3270 168.9510 66 19.6100 168 57.0500 % A3-17
% *** Adjust this first position to be safe distance (300) from A3-17
 66.3335 168.9230 66 20.0000 168 55.3800 % new AL12.5
 66.3400 168.8950 66 20.3900 168 53.7100 % AL13
 66.3460 168.8590 66 20.7400 168 51.5550 % new AL13.5
 66.3520 168.8230 66 21.0900 168 49.4000 % AL14
 66.3575 168.7875 66 21.4450 168 47.2450 % new AL14.5
 66.3630 168.7520 66 21.8000 168 45.0900 % AL15
 66.3690 168.7160 66 22.1550 168 42.9350 % new AL15.5
 66.3750 168.6800 66 22.5100 168 40.7800 % AL16
```

```
66.3810 168.6440 66 22.8600 168 38.6250 % new AL16.5
 66.3870 168.6080 66 23.2100 168 36.4700 % AL17
 66.3940 168.5657 66 23.6400 168 33.9400 % new AL17.5 % AND MOVED OFF Q CABLE
 66.3990 168.5360 66 23.9200 168 32.1600 % AL18
 66.4045 168.5000 66 24.2750 168 30.0000 % new AL18.5
 66.4100 168.4640 66 24.6300 168 27.8400 % AL19
 66.4160 168.4280 66 24.9800 168 25.6850 % new AL19.5
 66.4220 168.3920 66 25.3300 168 23.5300 % AL20
 66.4280 168.3560 66 25.6850 168 21.3750 % new AL20.5
 66.4340 168.3200 66 26.0400 168 19.2200 % AL21
 66.4400 168.2845 66 26.3950 168 17.0650 % new AL21.5
 66.4460 168.2490 66 26.7500 168 14.9100 % AL22
 66.4520 168.2130 66 27.1000 168 12.7550 % new AL22.5
 66.4580 168.1770 66 27.4500 168 10.6000 % AL23
 66.4635 168.1410 66 27.8050 168 8.4450 % new AL23.5
 66.4690 168.1050 66 28.1600 168 6.2900 % AL24
%
%Then these are new
 66.4745 168.0690 66 28.5150 168 4.1350 % new AL24.5
 66.4800 168.0330 66 28.8700 168 1.9800 % AL25
 66.4855 167.9970 66 29.2250 167 59.8200 % new AL25.5
 66.4910 167.9610 66 29.5800 167 57.6650 % AL26
 66.4965 167.9250 66 29.9350 167 55.5100 % new AL26.5
 66.5020 167.8890 66 30.2900 167 53.3550 % AL27
 66.5075 167.8530 66 30.6450 167 51.2000 % new AL27.5
%
%===========
% LIS = Cape Lisburne Line (redone to avoid Qcable at Lis9)
%============
% - 18 stations (including first of CCL line)
% - station spacing ~ 2nm near coast,
       ~ 3nm and ~ 5nm away from coast
% Distances: - LIS1 to CCL22 57.2nm
% Time from NorsemanII, ~ 10hrs
% Time from Khromov ~11hrs
% Times different now added stations
  Lat (N)
            Long (W)
                      Name
   deg min
             deg min
 0 0
         68 54.40 166 19.80 % LIS 1 + net
         68 54.80 166 25.15 % LIS 2
 0 0
         68 55.20 166 30.51 % LIS 3
 0 0
 0 0
         68 55.80 166 38.54 % LIS 4
 0 0
         68 56.40 166 46.57 % LIS 5
 0 0
         68 57.00 166 54.60 % LIS 6 + net
 0 0
         68 57.60
                   167 1.95 % LIS 6.5 - no bottles
 0 0
         68 58.20 167 9.30 % LIS 7
         68 58.80 167 16.65 % LIS 7.5 - no bottles
   0
```

```
68 59.40 167 24.00 % LIS 8
69.0033 167.5633 69 00.20 167 33.8 % NEW ** LIS 8.5
%
%DO NOT DO LIS 9
          %DO NOT DO LIS 9
%
69.0167 167.7267 69 1.00 167 43.60 % NEW ** LIS 9.5
 0 0
        69 1.80 167 53.40 % LIS 10 + net
 0 0
        69 1.35 168 7.95 % LIS 11
        69 0.90 168 22.50 % LIS 12
 0 \quad 0
 0 0
        69 0.45 168 37.05 % LIS 13
 0 0
        69 0.23 168 46.62 % LIS 14n + net
 0 0
        69 0.00 168 56.00 % CCL22n % was 56.2
% - South Bering Strait section
% First ran in 2014 and 2015 and then only partly
% Run in full in 2017
%
% To catch ACC before it enters the strait
% 22.5nm long
% 21 stations including halves
% Lat(N) Lon (W)
                 Lat (N)
                          Lon (W)
                                  NAME
% decdeg decdeg
                deg min deg min
65.5818 168.1167
                                    7.00
                  65
                        34.91 168
                                          % SBS1 = BS24
65.5736 168.1571
                  65
                        34.42 168
                                    9.43 % SBS1.5
                        33.93 168
65.5655 168.1975
                  65
                                    11.85 % SBS2
                  65
                        33.44 168
                                    14.28 % SBS2.5
65.5573 168.2379
65.5491 168.2784
                  65
                        32.95
                             168
                                    16.70 % SBS3
65.5409 168.3188
                  65
                        32.45 168
                                    19.13 % SBS3.5
65.5327 168.3592
                  65
                        31.96 168
                                    21.55 % SBS4
                        31.47 168
65.5245 168.3997
                                    23.98 % SBS4.5
                  65
                        30.98 168
                                    26.40 % SBS5
65.5163 168.4401
                  65
65.5081 168.4805
                  65
                        30.49
                             168
                                    28.83 % SBS5.5
65.5000 168.5209
                  65
                        30.00
                             168
                                    31.26 % SBS6
65.4918 168.5614
                  65
                        29.51 168
                                    33.68 % SBS6.5
65.4836 168.6018
                  65
                        29.02 168
                                    36.11 % SBS7
65.4754 168.6422
                        28.52 168
                                    38.53 % SBS7.5
                  65
65.4672 168.6826
                  65
                        28.03 168
                                    40.96 % SBS8
                        27.54 168
                                    43.38 % SBS8.5
65.4590 168.7231
                  65
65.4508 168.7635
                  65
                        27.05
                             168
                                    45.81 % SBS9
65.4426 168.8039
                  65
                        26.56
                             168
                                    48.24 % SBS9.5
65.4345 168.8444
                  65
                        26.07 168
                                    50.66 % SBS10
                        25.58
65.4263 168.8848
                  65
                              168
                                    53.09 % SBS10.5
65.4181 168.9252
                  65
                        25.09
                             168
                                    55.51 % SBS11
```

```
% CS = Cape Serdtse Kamen to Point Hope Line (US portion)
% - with extras.
% Hazards on this line:
% == Final station CS19 is shallow. Check on
% modern charts to see if deep enough for NorsemanII.
% (this station was too shallow for the Khromov, but
% was ok for the NorsemanII in 2013).
% == NOAA mooring at:
      67 54.712N, 168 11.628W
%-----
% - 27 stations
% - station spacing ~ 2.5nm in the central Chukch (0.25 stations)
         ~ 2.2nm near the coast
%
% Distances: - CS10US to CS18 60.8nm
     - CS18 to CS19 2.2nm
% Time from NorsemanII (toCS19) ~ 11hrs
%-----
% Lat (N) Long (W)
                    Name
% deg min deg min
0 0 67 38.1 168 56.0 % CS10US + net
0 0 67 39.9 168 52.0 % new CS10.25
0 0 67 41.7 168 48.1 % CS10.5 - no bottles
0 0 67 43.5 168 44.0 % new CS10.75
0 0 67 45.3 168 39.9 % CS11
0 0 67 47.1 168 34.6 % new CS11.25
0 0 67 48.9 168 29.4 % CS11.5 - no bottles
0 0 67 50.7 168 24.1 % new CS11.75
0 0 67 52.5 168 18.8 % CS12 + net
0 0 67 54.2 168 13.9 % new CS12.25
0 0 67 55.9 168 9.1 % CS12.5 - no bottles
0 0 67 57.6 168 4.2 % new CS12.75
0 0 67 59.3 167 59.4 % CS13
0 0 68 1.0 167 54.5 % new CS13.25
0 0 68 2.7 167 49.7 % CS13.5 - no bottles
0 0 68 4.4 167 44.8 % new CS13.75
0 0 68 6.1 167 39.9 % CS14 + net
0 0 68 7.6 167 35.3 % new CS14.25
0 0 68 9.1 167 30.7 % CS14.5 - no bottles
0 0 68 10.6 167 26.0 % new CS14.75
0 0 68 12.1 167 21.4 % CS15
0 0 68 13.6 167 16.8 % CS15.5 - no bottles
0 0 68 15.0 167 12.2 % CS16
0 0 68 16.6 167 7.6 % CS16.5 - no bottles
0 0 68 18.0 167 2.9 % CS17 + net
0 0 68 18.9 166 57.6 % CS18
0 0 68 19.9 166 52.3 % CS19 *** SHALLOW **
```

% North North Bering Strait Line (NNBS)

```
%
% Add a shallower station to NNBS ...
% A section across the ACC and main flow between
% the A3L line and the NBS line.
% With the 0.5s, at 1.76nm spacing
% 22.8nm length
%-----
% Run for the first time in 2015 - check water depths on
% the eastern (NNBS7.5) end)
% Dovetails with DL line. NNBS1 is the same as DL16
66.170 168.937 66 10.19 168 56.20 %NNBS1
66.170 168.865 66 10.19 168 51.88 %NNBS1.5
66.170 168.793 66 10.19 168 47.55 %NNBS2
66.170 168.721 66 10.19 168 43.23 %NNBS2.5
66.170 168.648 66 10.19 168 38.91 %NNBS3
66.170 168.576 66 10.19 168 34.58 %NNBS3.5
66.170 168.504 66 10.19 168 30.26 %NNBS4
66.170 168.432 66 10.19 168 25.94 %NNBS4.5
66.170 168.360 66 10.19 168 21.62 %NNBS5
66.170 168.288 66 10.19 168 17.29 %NNBS5.5
66.170 168.216 66 10.19 168 12.97 %NNBS6
66.170 168.144 66 10.19 168 8.65 %NNBS6.5
66.170 168.072 66 10.19 168 4.32 %NNBS7
66.170 168.000 66 10.19 168 0.00 %NNBS7.5
66.170 168.000 66 10.19 167 55.70 %NNBS8 *** NEW
% NPH - North Point Hope Line (Extended)
%-----
% Crossing from Point Hope to the ENE roughly.
% ===== 2019
% - updated to add an extra 20nm and 8 stations,
% with extras at 2.5nm space to CCL
% - now have 19 stations, and 40nm
% Run from east (NPH1) to west (NPH11)
% - estimate 3hrs 15min to NPH11 and then another
% - 4 hrs for the rest
% Lat (N) Long (W) Name
% deg min deg min
0 0 68 22.40 167 07.93 % NPH1
0 0 68 22.64 167 11.31 % NPH2
0 0 68 22.87 167 14.68 % NPH3
0 0 68 23.11 167 18.06 % NPH4
0 0 68 23.35 167 21.44 % NPH5
0 0 68 23.83 167 28.19 % NPH6
```

```
0 0 68 24.30 167 34.95 % NPH7
0 0 68 24.77 167 41.71 % NPH8
0 0 68 25.25 167 48.46 % NPH9
0 0 68 25.73 167 55.22 % NPH10
0 0 68 26.20 168 01.97 % NPH11
% NEW
0 0 68 26.68 168 08.72 % NPH11.5
0 0 68 27.15 168 15.47 % NPH12
0 0 68 27.63 168 22.23 % NPH12.5
0 0 68 28.10 168 28.98 % NPH13
0 0 68 28.58 168 35.74 % NPH13.5
0 0 68 29.05 168 42.49 % NPH14
0 0 68 29.53 168 49.25 % NPH14.5
0 0 68 30.00 168 56.00 % CCL19
%End of new
% CD- Cape Dyer (extended)
%_____
% Crossing east west, midway between Point Hope
% and Cape Lisburne (near Cape Dyer) and trying
% to avoid some topographic irregularites just
% N of the line on the charts.
% - 27 stations, 2nm spacing
% - first 14 due west to match 2016 line, now
% then angles to meet CCL20 at the Convention line
% - Distance 54nm
% - 27 stations
% - ** CHECK DEPTH OF SHALLOWEST CD1
%-----
% Lat (N) Long (W) Name
  deg min deg min
0 0 68 40.00 168 56.0 % CCL20
%**NEW
0 0 68 39.79 168 50.6 % CD27
0 0 68 39.57 168 45.3 % CD26
0 0 68 39.36 168 39.9 % CD25
0 0 68 39.14 168 34.6 % CD24
0 0 68 38.93 168 29.2 % CD23
0 0 68 38.71 168 23.9 % CD22
0 0 68 38.50 168 18.5 % CD21
0 0 68 38.29 168 13.1 % CD20
0 0 68 38.07 168 7.8 % CD19
0 0 68 37.86 168 2.4 % CD18
0 0 68 37.64 167 57.1 % CD17
0 0 68 37.43 167 51.7 % CD16
0 0 68 37.21
            167 46.4 % CD15
%*END OF NEW, carry on with 2016 stations
```

```
0 0 68 37.00 167 41.0 % CD14
0 0 68 37.00 167 35.5 % CD13
0 0 68 37.00 167 29.9 % CD12
0 0 68 37.00 167 24.4 % CD11
0 0 68 37.00 167 18.8 % CD10
0 0 68 37.00 167 13.3 % CD9
0 0 68 37.00 167 7.8 % CD8
0 0 68 37.00 167 2.2 % CD7
0 0 68 37.00 166 56.7 % CD6
0 0 68 37.00 166 51.2 % CD5
0 0 68 37.00 166 45.6 % CD4
0 0 68 37.00 166 40.1 % CD3
0 0 68 37.00 166 34.5 % CD2
0 0 68 37.00 166 29.0 % CD1
% SAS = S extension of AS line
% Adding another 8 stations at 4nm spacing south
% from AS1 to the coast.
%--
% Estimate for NorsemanII 8 casts ~ 4hrs
% Not run vet
%-----
% Lat (N) Long (W)
                    Name
% deg min deg min
0 0 66 37.91 167 34.00 % SAS 1
0 0 66 34.35 167 29.14 % SAS 2
0 0 66 30.79 167 24.29 % SAS 3
0 0 66 27.23 167 19.43 % SAS 4
0 0 66 23.68 167 14.57 % SAS 5
0 0 66 20.12 167 9.72 % SAS 6
0 0 66 16.56 167 4.86 % SAS 7
0 0 66 13.00 167 0.00 % SAS 8
% - South Bering Strait section redone - SBSnn
% First ran in 2014 and 2015 and then only partly
% Run in full in 2017
% Re aligned in 2019 to start from BS22
% 2019 stations slightly off this (SBSn)
% To catch ACC before it enters the strait
% 22.5nm long
% 21 stations including halves
%-----
% Lat(N) Lon (W) Lat (N)
                      Lon (W)
                              NAME
% decdeg decdeg deg min deg min
```

```
168 10.63 % SBSnn1 = BS22
65.614 168.215
                65 36.86
                          168 12.87 % SBSnn1.5
65.604 168.252
               65 36.24
                          168 15.12 % SBSnn2
65.594 168.289
                65 35.62
                          168 17.36 % SBSnn2.5
65.583 168.327
               65 35.00
                          168 19.61 % SBSnn3
               65 34.38
                          168 21.85 % SBSnn3.5
65.573 168.364
65.563 168.402
               65 33.76
                          168 24.09 % SBSnn4
65.552 168.439
                65 33.14
                          168 26.34 % SBSnn4.5
65.542 168.476
                65 32.52
                          168 28.58 % SBSnn5
65.532 168.514
               65 31.90
                          168 30.83 % SBSnn5.5
65.521 168.551
                65 31.29
                          168 33.07 % SBSnn6
65.511 168.589
               65 30.67
                          168 35.31 % SBSnn6.5
                65 30.05
                          168 37.56 % SBSnn7
65.501 168.626
65.490 168.663
               65 29.43
                          168 39.80 % SBSnn7.5
65.480 168.701
                65 28.81
                          168 42.05 % SBSnn8
65.470 168.738
               65 28.19
                          168 44.29 % SBSnn8.5
                          168 46.53 % SBSnn9
               65 27.57
65.459 168.776
65.449 168.813
               65 26.95
                          168 48.78 % SBSnn9.5
                          168 51.02 % SBSnn10
65.439 168.850
                65 26.33
65.428 168.888
                65 25.71
                          168 53.27 % SBSnn10.5
65.418 168.925
               65 25.09
                          168 55.51 % SBSnn11
%
% NCD - North Cape Dyer Line
% 2nm near the coast NCD1-16
% 2.5nm on out to CCL21 (which is NCD 26)
% Length to CCL21 is 55.4nm
% Lat(N) Lon (W) Lat (N)
                          Lon (W)
                                   NAME
% decdeg decdeg deg min deg min
68.753 166.422 68 45.20 166 25.30 %NCD1
68.757 166.513 68 45.39
                          166 30.78 %NCD2
68.760 166.604
               68 45.59
                          166 36.26 %NCD3
               68 45.78
                          166 41.74 %NCD4
68.763 166.696
                68 45.97
                          166 47.22 %NCD5
68.766 166.787
68.769 166.878
               68 46.17
                          166 52.70 %NCD6
68.773 166.970
                68 46.36
                          166 58.18 %NCD7
68.776 167.061
               68 46.55
                          167 3.66 %NCD8
                          167 9.14 %NCD9
68.779 167.152
                68 46.75
                          167 14.62 %NCD10
68.782 167.244
               68 46.94
                          167 20.10 %NCD11
68.786 167.335
                68 47.13
                68 47.33
                          167 25.58 %NCD12
68.789 167.426
68.792 167.518
                68 47.52
                          167 31.06 %NCD13
68.795 167.609
                68 47.71
                          167 36.54 %NCD14
                68 47.91
                          167 42.02 %NCD15
68.798 167.700
68.802 167.792
                68 48.10
                          167 47.50 %NCD16 2nm up to here, 2.5nm after
68.805 167.906
                68 48.29
                          167 54.35 %NCD17
68.808 168.020
                68 48.48
                          168 1.20 %NCD18
```

65.625 168.177

65 37.48

68.811 168.134	68	48.67	168	8.05 %NCD19
68.814 168.248	68	48.86	168	14.90 %NCD20
68.817 168.363	68	49.05	168	21.75 %NCD21
68.821 168.477	68	49.24	168	28.60 %NCD22
68.824 168.591	68	49.43	168	35.45 %NCD23
68.827 168.705	68	49.62	168	42.30 %NCD24
68.830 168.819	68	49.81	168	49.15 %NCD25
68.833 168.933	68	50.00	168	56.00 %NCD26

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% Bering Strait 2021 NORSEMAN2 log CTD			
%Date Time 1 Cast NO DovDepth (Lat (deg) Lat (min) Lon (deg) Lon(min) Altimeter		WindspecWind Oper Fog WaterCl	
%Please fill in all data for every event (CTD/net tow) 0=bad 1=go	6	knots 0 = cle 0=clear,	1=noclear
,	6		
	6		
%Ty=Type: 1=CTD / 2=Net tow/4=prod cast x; 5=Pumping cast for Trace Metals Altimeter	-	Fog Watercla	arity
%#,Number is consecutive for that event type %In/out (I/O): 1=In / 2=Out	6		
%Dep=waterdepth(m) from Furuno readout by CTD which is depth below keel, keel is 3m (10ft)	6		
	6		
	6		
%St is the name of the station (Line ID then station number) % SS = CTD operator estimate of sea state (Beaufort Scale)	6		
%WSp=wind speed in m/s: WD=Wind direction from bridge			
%Op=CTD operator			
% when 3 lines for NET, dep indicates wire out for net			
% Altimeter = 0 if complete rubbish, 0.5 if some good readings, 1 if good both up and down %Fill in any comments if needed.	6	KNOTS	
	6 dry test	3.4 217 atn	dry test to learn CTD driving
	6 dry test		AR: m VISIBLE
	6 0.1	16.6 187 atn	500 7400 14 50 15 15 15 15 15 15 15 15 15 15 15 15 15
20140703 645 1 20 2 52.5 65 41.235 168 26.937 %%%%%%%%%% STARTING HERE FOR 2021 AND GET A WIRE TO CLEAN PUMPS WHEN NEEDED	6 BS18 Wire Out	16.8 184 atn	BStrait14020.hdr file: put Station=BS20 by mistake, should be Station=BS18 as shown here in StationID
SET LAPTOP TIME TO GMT	l suc suc	Wind Water	
%Date Time 1 Cast NO Dov Depth (Lat (deg) Lat (min) Lon (deg) Lon(min) Altimeter			Comments
	6 dry test 6 shallow wet test	21.2 68 KC 18.9 87 KC	dry test on deck to check the CTD termination (re-terminated by Robert) and setup; Aft GPS is non-functional so we will use the forward GPS in future casts.
	6 shallow wet test	23 50 KC	just a soak (5-10m, not going to depth) to test the termination; took a long moment for the pump to turn on, but otherwise all clear
	6 A2-20 recovery precast 218 268		pre-mooring recovery cast, A2-20; also the first full cast
	6 A2-20 recovery precast	16.3 163 KC	
	6 A2-19 recovery precast 217 267 6 A2-19 recovery precast	57 13 161 KC 0 5m 12.7 177 KC	pre-mooring recovery cast, A2-19; moved in small increments down at bottom to get below 51m
	6 A4-20 recovery precast 217 278		pre-mooring recovery cast, A4-20; adjusted computer time to better match UTC prior to this cast (previously a ~43s offset)
20210708 1917 1 4 2 46.5 65 45.45 168 16.086 0	6 A4-20 recovery precast	27 244 RJD	
	6 A4-19 recovery precast 217 299 6 A4-19 recovery precast	9 23 230 RJD 0 1m 24 144 RJD	pre-mooring recovery cast, A4-19; lots of line paid out, strong current. Speed was slightly slow.
	6 dry test post A2-21	24 144 RJD KC	dry test on deck. Cleaned vent plugs and ran FW through C cell
	6 A2-21 calibration cast 217 267	57 21 154 JG 0 5 m	some discrepancy in oxygen sensors and "strangeness" in Salinity; cleaned vent plugs and ran FW through C cell again
	6 A2-21 calibration cast	JG	
	6 Laramie pump test 0 40 6 A3-20 recovery precast A 217 265		rainy and windy, test cast was done during transit from A2 to A3. pumped roughly 2.5 Gal to the surface. Just a downcast included here, will do upcasts as well in th Figuring out CTD issues with pump (vent plug cleaned): go down slowly, stay at bottom for 10 counts, come up to surface and then recast without taking out of wat
	6 A3-20 recovery precast A	KC STEEL	The state of the s
	6 A3-20 recovery precast B 217 267		Second cast to diagnose CTD pump problems on upcast; same protocol as previous cast
	6 A3-20 recovery precast B 6 A3-19 recovery precast A 217 272	20 345 KC 72 19.4 11 KC 0 3m	pre-mooring recovery cast A3-19; moved p2 temperature sensor up slightly to match output level
	6 A3-19 recovery precast A 217 272	KC 15.4 11 KC 0 5111	pre-mouning recovery cast A3-13, moved by temperature sensor up signify to match output rever
	6 A3-19 recovery precast B 217 266		pre-mooring recovery cast A3-19 B; ran cast without pump for sensor diagnostics
	6 A3-19 recovery precast B 6 A3-21 calibration 218 269	21.1 342 KC i9 18.2 351 JG 2m	A3-21 post deployment calibration cast, replumbed CTD as well for connecting T and C.
	6 A3-21 calibration 218 269	17.8 350 JG	A3-22 post deployment cambration cast, replumbed CTD as well for connecting 1 and C.
20210710 1552 1 12 1 29.5 65 37.4 168 10.542 0.5	6 BS22 214 255		BS22 - time is just an estimate, forgot to write it down
	6 BS22	14.2 175 JG	
	6 BS22-Laramie 6 BS22 Laramie	JG 3m	1st Laramie cast
	6 BS21.5 214 254		algae
20210710 1623 1 13 2 37 65 38.178 168 12.823	6 BS21.5	9 174 JG	
	6 BS21 217 244		
	6 BS21 6 BS20.5 216 262	17.5 199 JG 52 20.8 149 JG	Cleaned vent plugs before cast
	6 BS20.5	20.6 183 JG	
	6 BS20.5 Laramie	JG	2nd Laramie Cast
	6 BS20.5 Laramie 6 BS20 218 265	JG 55 18.8 193 JG 0 3m	Depth not recorded
	6 BS20 218 205	19.5 230 JG	
20210710 1742 1 17 1 48.7 65 39.791 168 21.293	6 BS19.5 218 263		chunky vis
	6 BS19.5	20.9 208 JG	
	6 BS19 217 265 6 BS19	55 10 181 JG 5m 19.4 171 JG	
	6 BS 19 Laramie	JG 4m	
20210710 1813 5 3 2 50.4 65 40.984 168 23.359	6 BS19 Laramie	21.3 268 RJD	
	6 BS18.5 217 267		
	6 BS18.5 6 BS18 217 280	20 188 RJD 30 22 181 RJD 5m	
	6 BS18	22 186 RJD	
	6 BS17.5 217 275		
	6 BS17.5 6 BS17.5 Laramie	20 158 RJD JG	
	6 BS17.5 Laramie 6 BS17.5	JG JG	
2012			

20210710 1907 1			52.9	65	42.154	168	31.224 0.5		217	2/8		200 JG	0 5m	
20210710 1911 1		2		65	42.28	168	31.273	% BS17				161 JG		
20210710 1920 1		1	50.2	65	42.719	168	33.379	% BS16.5	217	2/6		183 JG		
20210710 1922 1		2	50.1	65	42.868	168	33.253 0	% BS16.5				192 JG	0	
20210710 1933 1	1 24	1	49.9	65	43.233	168	35.534	% BS16	218	270		150 RJD	0 5m	
0210710 1936 1	1 24	2	50	65	43.325	168	35.547	% BS16			25	153 RJD	0	
0210710 1938 5	5 5	1	49.9	65	43.478	168	35.475	% BS16 Laramie			20	161 RJD	0 5m	
	5 5	2	50	65	43.734	168	35.244	% BS16 Laramie				RJD	0	
210710 2012 1		1	50.3	65	43.767	168	37.516	% BS15.5	218	270	21	181 RJD	0 5m	
			50.3		43.858	168			210	270			0	
210710 2015 1		2		65			37.468	% BS15.5				188 RJD		
210710 2029 1		1	49.9	65	44.242	168	39.791	% BS15	218			170 RJD	0 5m	
210710 2033 1		2	50.3	65	44.353	168	39.795	% BS15				170 RJD	0	
0210710 2040 1	1 27	1	50.6	65	44.774	168	41.58	% BS14.5	218	281	25	171 RJD	0 5m	
0210710 2045 1	1 27	2	50.4	65	44.911	168	41.595	% BS14.5			23	170 RJD	0	
0210710 2047 5	5 6	1	51.3	65	45.106	168	41.666	% BS14.5 Laramie			24	160 RJD	0 5m	
0210710 2047 5	5 6	2	51.2	65	45.21	168	43.171	% BS14.5				RJD	0	Recovery time missing
0210710 2103 1		1	51.4	65	45.387	168	43.365	% BS14	217	271	21	181 RJD	0 5m	Vent plugs cleaned
0210710 2108 1		2	51.4	65	45.387	168	43.365	% BS14				180 RJD	0	Tell plags dealled
0210710 2116 1		1	51.3	65	45.781	168	45.505	% BS13.5	217	2/5		181 RJD	0 5m	
0210710 2120 1		2	51.1	65	45.9	168	45.999	% BS13.5				190 RJD	0	
0210710 2128 1	1 30	1	50.3	65	46.198	168	47.563	% BS13	218	282	20	208 RJD	0 5m	Vent plugs cleaned
0210710 2133 1	1 30	2	50.1	65	46.366	168	47.695	% BS13			22	171 RJD	0	
210710 2135 5		1	50.5	65	46.545	168	47.546	% BS13 Laramie				185 RJD	0 5m	
0210710 2143 5		2		65	46,601	168	47.78	% BS13 Laramie				RJD	0	
210710 2143 1		1	48.6	65	46.802	168	49.702	% BS12.5	217	277	22	200 RJD	0 5m	Vent plugs cleaned
			48.0				49.702		21/	2//		200 RJD		vent plugs deemed
210710 2155 1		2		65	46.949	168		% BS12.5					0	
210710 2200 1		1	43.2	65	47.178	168	51.611	% BS12	217	261		180 RJD	0 4m	
210710 2205 1	1 32	2	43	65	47.251	168	51.785	% BS12				175 RJD	0	
210710 2213 1	1 33	1	46	65	47.673	168	53.816	% BS11.5	217	265	24	165 RJD	0 4m	Vent plugs cleaned
210710 2217 1	1 33	2	46.1	65	47.682	168	53.855	% BS11.5			22	170 RJD	0	
210710 2218 5		1	46.3	65	47.702	168	53.89	% BS11.5 Laramie				172 RJD	0	
210710 2225		2	46.3	65	47.702	168	53.89	% BS11.5 Laramie				210 RID	0	Recovery postion missing - set to be same as deploy
0210710 2223 1	-	1	44.9	65	48.196	168	55.863	% BS11.5 Earlanne	217	270		181 RJD	0 2m	necovery position missing - set to be same as deploy
		2	44.9						217	270			0 2111	
0210710 2238 1				65	48.25	168	55.905	% BS11				180 RJD	_	
0210710 2245 1		1		65	49.211	168	56.095	% DL1	217	268		181 RJD	0 4m	Vent plugs cleaned
210710 2250 1	1 35	2	45.7	65	49.436	168	56.189	% DL1			27	184 RJD	0	
210710 2256 1	1 36	1	45.8	65	50.154	168	56.381	% DL2	217	262	27	172 RJD	0 3m	
210710 2300 1	1 36	2	45.9	65	50.289	168	56.5	% DL2			13	180 RJD	0	
210710 2308 1	1 37	1	47.1	65	51.188	168	56.12	% DL3			27	171 RJD	0 3m	
210710 2312 1		2	47	65	51.328	168	56.213	% DL3				188 RJD	0	
0210710 2312 1			44.7		52.097	168		% DL4	217	250		169 KC	Ü	Mantalian depend
		1		65					217				0 3m	Vent plugs cleaned
0210710 2322 1		2	44.3	65	52.14	168	56.299 0	% DL4				190 KC		
0210710 2329 1		1	46.3	65	53.064	168	56.185 0	% DL5	217	258 2		168 KC	0 3m	
0210710 2334 1	1 39	2	46.5	65	53.093	168	56.159 0	% DL5				190 KC		
0210710 2342 1	1 40	1	47.8	65	54.092	168	56.205 0	% DL6	217	258 1	16.5	181 KC	0 4m	Vent plugs cleaned
20210710 2346 1	1 40	2	47.8	65	54.136	168	56.158 0	% DL6				210 KC		
20210710 2355 1	1 41	1	47.9	65	55.169	168	56.238 0	% DI7	217			189 KC	0 5m	
0210710 2358 1		2	47.9	65	55.23	168	56.227 0	% DL7				199 KC	0 5	
		1	48.7			168		% DL8	217				0 6m	Vest alice also and complete and company in a company in
				65	56.112				217			174 KC	0 ьт	Vent plugs cleaneed; arge hysteresis on downcast in oxygen; keeping an eye on it for the next cast
0210711 10 1		2	48.5	65	56.169	168	56.209 0	% DL8				198 KC		
0210711 17 1		1	49.6	65	57.046	168	56.233 0	% DL9	218			177 KC	0 7m	Vent plugs cleaned; still mismatch between oxygens on the downcast
0210711 21 1		2	49.5	65	57.112	168	56.187 0	% DL9				180 KC		
0210711 30 1	1 44	1	50.5	65	58.042	168	56.273 0	% DL10	217	263 1	19.3	176 KC	0 4m	
210711 34 1		2	50.6	65	58.089	168	56.307 0	% DL10				215 KC		
0210711 41 1		1	50.9	65	58.983	168		% DL11	217			195 KC	0 4m	
0210711 41 1		2	51.1	65	59.071	168	56.151 0	% DL11	21/			214 KC	5 -7111	
									246				0.4	
0210711 53 1		1	51.3	65	59.983	168	56.203 0	% DL12	216			188 KC	0 4m	
210711 57 1		2	51.4	66	0.061	168	56.227 0	% DL12				214 KC		
0210711 105 1		1	51	66	1.236	168		% DL12.5	217			181 KC	0 4m	Huge spike in fluorescence; mislabeled in station name for seasave (DL13 rather than DL12.5)
210711 111 1	1 47	2	50.8	66	1.471	168	56.212 0	% DL12.5		2	20.9	212 KC		
		1	51.8	66	2.524	168	56.212 0	% DL13	218			182 KC	0 4m	New winch driver: extremely fast for the first part of down cast (15m in 2 sec), asked to slow down and speed seemed okay; data seemed okay too - move on to
0210711 120 1		2	51.8	66	2.603	168	56.178 0	% DL13				204 KC		
		1	51.9	66	3.805	168	56.202 0.5		218			177 KC	0 4m	
210711 125 1	1 40	2	51.9	66	3.885	168	56.202 0.5		210			177 KC	0 4111	
210711 125 1 210711 134 1	1 49							,					0.2	
210711 125 1 210711 134 1 210711 139 1	1 49			66	5.065	168	56.22 0.5	% DL14	217			167 KC	0 3m	
210711 125 1 210711 134 1 210711 139 1 210711 148 1	1 49 1 50	1												
210711 125 1 210711 134 1 210711 139 1 210711 148 1 210711 152 1	1 49 1 50 1 50		53.9	66	5.176	168	56.254 0.5					185 KC		
10711 125 1 10711 134 1 10711 139 1 10711 148 1 10711 152 1	1 49 1 50 1 50	1		66 66	5.176 6.432	168 168	56.254 0.5 56.103 0.5		217			185 KC 190 RJD	0 2m	Went equal speeds on upcast and downcast, resolved difference in measurements
10711 125 1 10711 134 1 10711 139 1 10711 148 1 10711 152 1 10711 209 1	1 49 1 50 1 50 1 51	1 2	53.9					% DL14.5	217		16		0 2m	Went equal speeds on upcast and downcast, resolved difference in measurements
210711 125 2 210711 134 2 210711 139 2 210711 148 2 210711 152 2 210711 209 2 210711 216 2	1 49 1 50 1 50 1 51 1 51	1 2 1 2	53.9 53.4 53.4	66 66	6.432 6.526	168 168	56.103 0.5 56.928 0.5	% DL14.5 % DL14.5		260	16 10	190 RJD 208 RJD		
210711 125 1 210711 134 1 210711 139 1 210711 148 1 210711 152 1 210711 209 1 210711 216 1 210711 227 1	1 49 1 50 1 50 1 51 1 51 1 52	1 2 1 2	53.9 53.4 53.4 53.2	66 66	6.432 6.526 7.636	168 168 168	56.103 0.5 56.928 0.5 56.269 0	% DL14.5 % DL14.5 % DL15	217	260 267 2	16 10 20.8	190 RJD 208 RJD 189 KC	0 2m 0 2.5m	Went equal speeds on upcast and downcast, resolved difference in measurements Again, equal speeds on up and down
210711 125 2 210711 134 1 210711 139 1 210711 148 1 210711 152 2 210711 209 1 210711 216 1 210711 227 1 210711 234 1	1 49 1 50 1 50 1 51 1 51 1 52 1 52	1 2 1 2 1 2	53.9 53.4 53.4 53.2 53.4	66 66 66	6.432 6.526 7.636 7.711	168 168 168 168	56.103 0.5 56.928 0.5 56.269 0 56.225 0	% DL14.5 % DL14.5 % DL15 % DL15	217	260 267 2	16 10 20.8 17.3	190 RJD 208 RJD 189 KC 188 KC	0 2.5m	Again, equal speeds on up and down
210711 125 2 210711 134 1 210711 139 2 120711 152 1 210711 152 2 210711 209 1 210711 216 1 210711 227 2 210711 234 1 210711 243 2	1 49 1 50 1 50 1 51 1 51 1 52 1 52 1 53	1 2 1 2 1 2 1 2	53.9 53.4 53.4 53.2 53.4 53.5	66 66 66 66	6.432 6.526 7.636 7.711 8.911	168 168 168 168 168	56.103 0.5 56.928 0.5 56.269 0 56.225 0 56.22 0.5	% DL14.5 % DL14.5 % DL15 % DL15 % DL15.5		267 2 267 1 267 1	16 10 20.8 17.3 19.9	190 RJD 208 RJD 189 KC 188 KC 178 KC		
210711 125 2 210711 134 1 210711 139 1 210711 148 2 210711 152 2 210711 209 2 210711 216 1 210711 227 2 210711 234 2 210711 234 2 210711 248 2	1 49 1 50 1 50 1 51 1 51 1 52 1 52 1 53 1 53	1 2 1 2 1 2	53.9 53.4 53.4 53.2 53.4 53.5 53.7	66 66 66 66 66	6.432 6.526 7.636 7.711 8.911 9.986	168 168 168 168 168 168	56.103 0.5 56.928 0.5 56.269 0 56.225 0 56.22 0.5 56.178 0.5	% DL14.5 % DL14.5 % DL15 % DL15 % DL15.5 % DL15.5	217	267 2 267 1 267 1	16 10 20.8 17.3 19.9 26.3	190 RJD 208 RJD 189 KC 188 KC 178 KC 204 KC	0 2.5m 0 3m	Again, equal speeds on up and down
210711 125 2 210711 134 1 210711 139 1 210711 148 1 210711 152 2 210711 209 2 210711 216 1 210711 227 2 210711 234 2 210711 248 2	1 49 1 50 1 50 1 51 1 51 1 52 1 52 1 53 1 53	1 2 1 2 1 2 1 2	53.9 53.4 53.4 53.2 53.4 53.5	66 66 66 66	6.432 6.526 7.636 7.711 8.911	168 168 168 168 168	56.103 0.5 56.928 0.5 56.269 0 56.225 0 56.22 0.5	% DL14.5 % DL14.5 % DL15 % DL15 % DL15.5 % DL15.5	217	267 2 267 1 267 1	16 10 20.8 17.3 19.9 26.3	190 RJD 208 RJD 189 KC 188 KC 178 KC	0 2.5m	Again, equal speeds on up and down
210711 125 2 210711 134 2 210711 139 2 210711 148 2 210711 152 2 210711 209 2 210711 216 2 210711 227 2 210711 234 2 210711 243 2 210711 248 2 210711 248 2	1 49 1 50 1 50 1 51 1 51 1 52 1 52 1 53 1 53	1 2 1 2 1 2 1 2	53.9 53.4 53.4 53.2 53.4 53.5 53.7	66 66 66 66 66	6.432 6.526 7.636 7.711 8.911 9.986	168 168 168 168 168 168	56.103 0.5 56.928 0.5 56.269 0 56.225 0 56.22 0.5 56.178 0.5	% DL14.5 % DL15.5 % DL15.5 % DL15.5 % DL15.5 % DL16.6	217	267 2 267 2 267 2 267 2	16 10 20.8 17.3 19.9 26.3 29.4	190 RJD 208 RJD 189 KC 188 KC 178 KC 204 KC	0 2.5m 0 3m	Again, equal speeds on up and down
125 125	1 49 1 50 1 50 1 51 1 51 1 52 1 52 1 53 1 53 1 54	1 2 1 2 1 2 1 2 1 2	53.9 53.4 53.2 53.4 53.5 53.7 54.2 53.9	66 66 66 66 66 66 66	6.432 6.526 7.636 7.711 8.911 9.986 10.157 10.245	168 168 168 168 168 168 168	56.103 0.5 56.928 0.5 56.269 0 56.225 0 56.22 0.5 56.178 0.5 56.263 0.5 56.215 0.5	% DL14.5 % DL14.5 % DL15 % DL15 % DL15.5 % DL15.5 % DL16 % DL16	217 217 217	267 2 267 1 267 1 267 2 267 2	16 10 20.8 17.3 19.9 26.3 29.4 22.7	190 RJD 208 RJD 189 KC 188 KC 178 KC 204 KC 189 KC 203 KC	0 2.5m 0 3m 0 2m	Again, equal speeds on up and down Attempting 1.5x speed on up compared to down - works well, implementing from this point. Cleaned vent plugs after this cast.
1210711 125 1210711 134 1210711 134 139 1210711 148 1210711 152 1210711 152 1210711 152 1210711 126 1210711 127 1210711 127 1210711 127 1210711 128 1210711 128 1210711 128 1210711 128 1210711 128 1210711 128 1210711 128 1210711 133 1210711 313 131 13	1 49 1 50 1 50 1 51 1 51 1 52 1 52 1 53 1 53 1 54 1 54 1 55	1 2 1 2 1 2 1 2 1 2 1 2	53.9 53.4 53.4 53.2 53.4 53.5 53.7 54.2 53.9	66 66 66 66 66 66 66 66	6.432 6.526 7.636 7.711 8.911 9.986 10.157 10.245 11.437	168 168 168 168 168 168 168 168	56.103 0.5 56.928 0.5 56.269 0 56.225 0 56.22 0.5 56.178 0.5 56.263 0.5 56.215 0.5 56.213 0	% DL14.5 % DL15 % DL15 % DL15 % DL15 % DL15.5 % DL16 % DL16 % DL16 % DL16.5	217	267 2 267 1 267 1 267 2 267 2	16 10 20.8 17.3 19.9 26.3 29.4 22.7 23.8	190 RJD 208 RJD 189 KC 188 KC 178 KC 204 KC 189 KC 203 KC 191 KC	0 2.5m 0 3m	Again, equal speeds on up and down
1210711 125 1 1210711 134 1 1210711 139 1 1210711 148 1 1210711 152 1 1210711 109 1 1210711 209 1 1210711 216 1 1210711 234 1 1210711 248 1 1210711 248 1 1210711 258 1 1210711 303 1 1210711 303 1 1210711 313 1	1 49 1 50 1 50 1 51 1 51 1 51 5 51 1 52 1 53 1 53 1 54 1 54 1 55 1 55	1 2 1 2 1 2 1 2 1 2 1 2 1 2	53.9 53.4 53.4 53.2 53.4 53.5 53.7 54.2 53.9 55	66 66 66 66 66 66 66 66	6.432 6.526 7.636 7.711 8.911 9.986 10.157 10.245 11.437 11.518	168 168 168 168 168 168 168 168 168	56.103 0.5 56.928 0.5 56.269 0 56.225 0.5 56.178 0.5 56.263 0.5 56.213 0 56.208 0	% D114.5 % D114.5 % D115 % D115 % D115 % D115.5 % D116 % D116 % D116.5 % D116.5	217 217 217 217	267 2 267 1 267 2 267 2 267 2 268 2	16 10 20.8 17.3 19.9 26.3 29.4 22.7 23.8 21	190 RJD 208 RJD 189 KC 188 KC 178 KC 204 KC 189 KC 203 KC 191 KC 205 KC	0 2.5m 0 3m 0 2m	Again, equal speeds on up and down Attempting 1.5x speed on up compared to down - works well, implementing from this point. Cleaned vent plugs after this cast.
210711 125 210711 134 210711 139 210711 139 210711 148 210711 152 210711 299 210711 296 210711 243 210711 248 210711 258 210711 258 210711 318 210711 318 210711 318 210711 318 210711 318 210711 318 210711 318 210711 318 210711 318 210711 318 210711 318 32 320711 318 32 320711 327 327	1 49 1 50 1 50 1 51 1 51 1 51 1 52 1 52 1 53 1 53 1 54 1 54 1 55 1 55 1 56	1 2 1 2 1 2 1 2 1 2 1 2 1 2	53.9 53.4 53.4 53.2 53.4 53.5 53.7 54.2 53.9 55 55.2 56.2	66 66 66 66 66 66 66 66 66	6.432 6.526 7.636 7.711 8.911 9.986 10.157 10.245 11.437 11.518 12.704	168 168 168 168 168 168 168 168 168 168	56.103 0.5 56.928 0.5 56.269 0 56.225 0 56.22 0.5 56.178 0.5 56.263 0.5 56.215 0.5 56.213 0.5 56.213 0.5 56.213 0.5 56.208 0 56.189 0.5	% D114.5 % D115 % D115 % D115 % D115.5 % D115.5 % D116.5 % D116.5 % D116.5 % D116.5 % D116.5 % D116.5 % D117	217 217 217	260 267 267 267 267 267 268 268 269 269	16 10 20.8 17.3 19.9 26.3 29.4 22.7 23.8 21 21.5	190 RJD 208 RJD 189 KC 188 KC 178 KC 204 KC 189 KC 203 KC 191 KC 205 KC	0 2.5m 0 3m 0 2m	Again, equal speeds on up and down Attempting 1.5x speed on up compared to down - works well, implementing from this point. Cleaned vent plugs after this cast.
210711 25 210711 134 210711 139 210711 148 210711 148 210711 209 210711 216 227 210711 227 210711 228 210711 248 210711 248 210711 248 210711 248 210711 248 210711 303 210711 313 210711 318 210711 318 210711 327 210711 327 210711 327 210711 327 32 210711 328 210711 327 32 210711 327 32 210711 327 32 32 32 32 32 32 32 32 32 32 32 32 32	1 49 1 50 1 50 1 51 1 51 1 51 1 52 1 52 1 53 1 53 1 54 1 55 1 55 1 56	1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2	53.9 53.4 53.4 53.2 53.4 53.5 53.7 54.2 53.9 55 55.2 56.2 56.3	66 66 66 66 66 66 66 66 66 66	6.432 6.526 7.636 7.711 8.911 9.986 10.157 10.245 11.437 11.518 12.704 12.777	168 168 168 168 168 168 168 168 168 168	56.103 0.5 56.928 0.5 56.269 0 56.225 0 56.225 0.5 56.178 0.5 56.213 0.5 56.213 0 56.208 0.5 56.139 0.5	% D114.5 % D114.5 % D115 % D115 % D115 % D115.5 % D116 % D116 % D116.5 % D116.5 % D117	217 217 217 217 217	260 267 267 267 267 268 268 269 269	16 10 20.8 17.3 19.9 26.3 29.4 22.7 23.8 21 21.5 18.6	190 RJD 208 RJD 189 KC 188 KC 178 KC 204 KC 189 KC 203 KC 191 KC 205 KC 180 KC 202 KC	0 2.5m 0 3m 0 2m 0 2m	Again, equal speeds on up and down Attempting 1.5x speed on up compared to down - works well, implementing from this point. Cleaned vent plugs after this cast.
210711 125 210711 134 210711 139 210711 139 210711 148 210711 152 210711 299 210711 296 210711 243 210711 248 210711 258 210711 258 210711 318 210711 318 210711 318 210711 318 210711 318 210711 318 210711 318 210711 318 210711 318 210711 318 210711 318 32 320711 318 32 320711 327 327	1 49 1 50 1 50 1 51 1 51 1 51 1 52 1 52 1 53 1 53 1 54 1 55 1 55 1 56	1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2	53.9 53.4 53.4 53.2 53.4 53.5 53.7 54.2 53.9 55 55.2 56.2	66 66 66 66 66 66 66 66 66	6.432 6.526 7.636 7.711 8.911 9.986 10.157 10.245 11.437 11.518 12.704	168 168 168 168 168 168 168 168 168 168	56.103 0.5 56.928 0.5 56.269 0 56.225 0 56.225 0.5 56.178 0.5 56.213 0.5 56.213 0 56.208 0.5 56.139 0.5	% D114.5 % D115 % D115 % D115 % D115.5 % D115.5 % D116.5 % D116.5 % D116.5 % D116.5 % D116.5 % D116.5 % D117	217 217 217 217	260 267 267 267 267 268 268 269 269	16 10 20.8 17.3 19.9 26.3 29.4 22.7 23.8 21 21.5 18.6	190 RJD 208 RJD 189 KC 188 KC 178 KC 204 KC 189 KC 203 KC 191 KC 205 KC	0 2.5m 0 3m 0 2m	Again, equal speeds on up and down Attempting 1.5x speed on up compared to down - works well, implementing from this point. Cleaned vent plugs after this cast.

20210711 357	1	58	1 56.3	66	15.257	168	56.217	0	% DL18	216	269	23.3	196 KC	0 2m	
0210711 402			2 56.3	66		168	56.207	0	% DL18				201 KC		
210711 412			1 55.9	66		168	56.189		% DL18.5	217	268		209 KC	0 3m	
			2 55.7	66		168	56.141		% DL18.5				236 KC		
			1 55.6	66		168	56.173		% DL19	217			210 KC	0 3m	
210711 431	_		2 55.5	66		168	56.098	-	% DL19				241 KC		
	1		1 55.7	66		168			% DL19.5	216	267		210 KC	0 3m	End of the DL line
0210711 443 0210711 451	1		2 55.6	66		168 168			% DL19.5 % A3 mooring site	216	260		226 KC 223 KC	0 3m	
0210711 451			1 55.3 2 55.4	66		168			% A3 mooring site % A3 mooring site	210	208		243 KC	0 3111	
0210711 504			1 55.5	66		168			% AL12.5	216	268		240 KC	0 3m	
			2 55.4	66		168	55.257		% AL12.5	210			260 KC	0 3111	
0210711 510			1 55.4	66		168			% AL12.5 Laramie	5			264 KC		Starting to record amount of piping that is put into the water in tht ewire in/out columns here. Surface is where the surface sample is taken. Bot is where the bott
0210711 518	5	9	2 55.3	66		168	55.288		% AL12.5 Laramie				312 KC		
0210711 527	1	64	1 55.4	66	20.398	168	53.777	0	% AL13	216	269	16	292 KC	0 3m	
0210711 532	1	64	2 55.5	66	20.472	168	53.835	0	% AL13			12.6	311 KC		
0210711 541	1	65	1 53.9	66	20.708	168	51.488	0.5	% AL13.5	216	265	5.5	302 KC	0 3m	
			2 53.8	66		168			% Al13.5				302 KC		
0210711 554			1 54.3	66		168	49.488		% AL14	216	267		301 KC	0 3m	
			2 54.2	66		168	49.551	0	% AL14				300 KC		
			1 54.3	66		168	49.58		% AL14 Laramie	5	45		293 KC		
			2 54.3	66 66		168	49.55	0	% AL14 Laramie	240	200		302 KC	0.2	
			1 54.3 2 54.2	66		168 168	47.292 47.266		% AL14.5 % AL14.5	218			295 KC 307 KC	0 3m	
			1 46.4	66		168	45.137	-	% AL14.5	217			311 KC	0.3m	
0210711 635			2 46.2	66		168	45.106		% AL15	21/			316 KC	0 3111	
0210711 644			1 50.9	66		168	42.995	-	% AL15.5	217			320 KC	0 3m	
			2 50.9	66		168	42.99		% AL15.5				327 KC		
0210711 650	5		1 50.8	66	22.211	168	42.999		% AL15.5 Laramie	5	45	10.2	317 KC		
			2 50.8	66		168	42.967		% AL15.5 Laramie				8.3 KC		
0210711 709	1	70	1 56.7	66	22.512	168	40.789		% AL16	216	270	14	314 JG	0.5 3m	
			2 56.5	66		168	40.835		% AL16				323 JG		
0210711 723			1 56.4	66		168	38.644		% AL16.5	216	270		343 JG	0.5 3m	
0210711 728			2 56.5	66		168	38.645		% AL16.5				336 JG		
			1 54.8	66		168	36.534		% AL17	217	268		336 JG	0 3m	
			2 55	66		168 168	36.54 36.529	0	% AL17	-	45	18	346 JG		
0210711 743 0210711 750			1 55.1 2 55	66 66		168	36.529		% AL17 Laramie % AL17 Laramie	5	45		JG		
0210711 750			1 54.3	66		168		0	% AL17.5	216	268	19.3	322 JG	0 3m	
0210711 739			2 54.5	66		168	34.861		% AL17.5	210			350 JG	5 5111	
0210711 804			1 52.6	66		168	32.222		% AL18	217			359 JG	0 3m	
			2 52.7	66		168	32.306	0	% AL18				1.9 JG		
			1 53	66		168	29.86		% AL18.5	216	267		19 JG	0 3m	
	1	75	2 52.9	66	24.207	168	29.89	0	% AL18.5				12.7 JG		
20210711 836			1 53	66		168	29.925		% AL18.5 Laramie	5	45		JG		
			2 53.1	66		168	29.94		% AL18.5 Laramie				JG		
20210711 854			1 53.3	66		168	27.852		% AL19	217	267		337 JG	0 4m	
			2 53.3	66		168	27.974		% AL19				350 JG		
0210711 908 0210711 912			1 52.4 2 52.1	66 66		168 168	25.587 25.658		% AL19.5 % AL19.5	216	265	13.8	7.4 JG 2 JG	0 4m	
20210711 912 20210711 922			2 52.1 1 52.3	66		168			% AL19.5 % AL20				2 JG 354 JG	0 4m	
0210711 922			2 52.3	66		168	23.556		% AL20 % AL20				354 JG 352 JG	0 4111	
0210711 928			1 52.2	66		168	23.554		% AL20 Laramie	5	45	20.5	JG		
0210711 935			2 52.1	66		168	23.533		% AL20 Laramie		-13		JG		
0210711 1020			1 50.8	66		168	21.283	0	% AL20.5	216	263	12.9	13.6 JG	0 3m	
0210711 1025			2 50.7	66		168	21.184		% AL20.5				359 JG		
0210711 1031	1	80	1 47.4	66	26.036	168	19.211	0	% AL21	216	261	7.9	5.8 JG	0 3m	
0210711 1036	1		2 47.3	66	26.045	168	19.294	0	% AL21			15	354 JG		
0210711 1046			1 43	66		168			% AL21.5	217	256		4.5 JG	0 3m	
			2 42.9	66		168	17.068	0	% AL21.5			14	354 JG		
0210711 1051			1 43.1	66		168	17.058		% AL21.5 Laramie	5	40		JG		
0210711 1058			2 42.8	66		168	16.99		% AL21.5 Laramie		255	0.0	JG	0 -	
0210711 1109			1 40.1	66		168			% AL22	217	253		8.4 JG	0 3m	
0210711 1113			2 40.1 1 36.5	66		168 168	14.958		% AL22 % AL22.5	21.0	250	16 17	5 JG 6.4 JG	0.3.5m	
			1 36.5 2 36.5	66 66		168	12.668	0	% AL22.5 % AL22.5	216	250		6.4 JG 349 JG	U 3.5M	
			1 32.3			168	10.459		% AL23	216	245		6.1 JG	0 3m	forgot to turn pump on, cast delayed slightly
			2 32.3	66		168	10.435		% AL23	210	2.13		7.2 JG	5 5111	
0210711 1142			1 31.9	66		168	10.328		% AL23 Laramie	5	30		JG		
0210711 1149			2 31.8	66		168	10.323		% AL23 Laramie				JG		
0210711 1157			1 28.6	66		168		0	% AL23.5	217	240	10.4	4 JG	0 3m	
0210711 1201			2 28.7	66		168	8.561		% AL23.5				JG		
0210711 1211			1 26.4	66		168	6.298		% AL24	217	241	16.6		0 3m	
0210711 1214			2 26.2	66		168	6.233		% AL24				350 JG		
0210711 1222			1 24.2	66		168			% AL24.5	217	239		6.2 JG	0 2m	
0210711 1226			2 24.2	66		168	4.078		% AL24.5				334 JG		
0210711 1234			1 22.7	66		168			% AL25	217			22.1 JG	0 2m	
0210711 1237			2 22.6	66		168	1.886	1	% AL25			12.9	356 JG		
0210711 1237			1 22.6	66		168	1.886		% AL25 Laramie				JG		
0210711 1237			2 22.6	66	28.777	168	1.886		% AL25 Laramie				JG		

20210711 1250 1	1 89	1	21.8	66	29.114	167	59.853	0	% AL25.5	217	237	11.3	6.2 JG	0 2m	
20210711 1254 1				66	29.066	167	59.794		% AL25.5				357 JG		
20210711 1302 1	1 90	1	21.5	66	29.454	167	57.663	1	% AL26	216	236	15.4	10.6 JG	0 2m	
20210711 1306 1				66	29.443	167	57.571	1	% AL26				354 JG		
20210711 1314 1			21.6	66	29.776	167			% AL26.5	216	236		19.8 JG	0 2m	
0210711 1317 1		2	21.4	66	29.75	167			% AL26.5				11.7 JG		
0210711 1325 1				66	30.115	167			% AL27	216	236		15.9 JG	0 2m	
0210711 1328 1				66	30.068	167	53.262		% AL27				22.8 JG		
0210711 1337 1			22.1	66 66	30.439	167 167			% AL27.5	216	236		16 JG	0.5 3m	
20210711 1341 1			22.1 45.8		30.409		51.255 15.558		% AL27.5	216	262		18.5 JG	0.2.5	hafter and relead author trust arranged an
20210711 2329 1 20210711 2334 1			45.5	65 65	44.921 45.066	168 168			% A4-21 post-deployment calil % A4-21 post-deployment calil		202		201 KC 227 KC	0 2.5111	before cast, raised system two's pump ~1 cm
20210711 2334 1		1	49.3	67	38.057	168	56,002		% CS10US		264		214 JG	0 4m	
20210712 1330 1			48.9	67	38.153	168	55.982		% CS10US	217	204		184 JG	0 4111	
0210712 1332 5			48.9	67	38.184	168	55.991		% CS10US Laramie	5	45		JG		
0210712 1338 5	5 18	2	48.9	67	38.32	168	56.018		% CS10US Laramie				JG		
0210712 1357 1	1 96	1	48.5	67	39.859	168	52.058	0	% CS10.25	217	264	24.2	197 JG	0 4m	
20210712 1401 1	1 96	2	48.6	67	39.929	168	51.997	0	% CS10.25				JG		
20210712 1430 1	1 97	1	48.4	67	41.552	168	48.235	0	% CS10.5	218	265	24.9	206 JG	0 3m	
0210712 1434 1		2	48.7	67	41.64	168	48.211	0	% CS10.5				193 JG		
0210712 1452 1			48.4	67	43.381	168	43.952	0	% CS10.75	218	265	24.7	174 JG	0 3m	
	1 98		48.6	67	43.526	168	43.795	0	% CS10.75				161 JG		
0210712 1513 1		1	48.5	67	43.301	168	39.945		% CS11	217	268		200 RJD	0 4m	Vent plug cleaned
0210712 1520 1		2		67	45.258	168	39.73	0	% CS11				190 RJD	0 -	
0210712 1520 5			48.5	67	45.245	168	39.725		% CS11 Laramie	5			198 RJD	0 4m	
0210712 1532 5			48.7	67	45.701	168	39.325	0	% CS11 Laramie	240	262		185 RJD	0.4	
0210712 1549 1 0210712 1552 1	1 100		48.5 48.8	67 67	47.065 47.147	168 168	34.596 34.533	0	% CS11.25 % CS11.25	218	262		200 RJD 175 RJD	0 4m	
20210712 1552 1 20210712 1611 1			48.8	67	47.147	168	29.589		% CS11.25 % CS11.5	719	267		209 RJD	0 5m+	
0210712 1611 1			49.1	67	48.746	168	29.589		% CS11.5	218	207		171 RJD	0 3111+	
0210712 1010 1			51.5	67	50.632	168	24.162		% CS11.75	218	264		198 RJD	0 5m+	
0210712 1638 1				67	50.744	168	23.949		% CS11.75		-5-		178 RJD	2 3	
0210712 1655 1			54.9	67	52.27	168	18.186		% CS12	217	262	24	202 RJD	0 5m	
0210712 1701 1			55.1	67	52.393	168	19.13		% CS12				204 RJD		
20210712 1702 5	5 20	1	55.2	67	52.416	168	19.138		% CS12 Laramie	5		26	198 RJD	0 5m	
0210712 1719 5	5 20	2	55.4	67	52.556	168	18.045		% CS12 Laramie			25	177 RJD		
0210712 1732 1	1 104	1	56.8	67	54.151	168	13.825	0	% CS12.25	218	267		197 RJD	0 5m	
20210712 1736 1			56.7	67	54.254	168	13.767		% CS12.25				181 RJD		
20210712 1754 1			57.5	67	55.779	168	9.093		% CS12.5	217	273		212 RJD	0 5m+	
20210712 1757 1			57	67	55.929	168	8.937	0	% CS12.5				170 RJD		
20210712 1816 1			60.2	67	57.496	168	4.317		% CS12.75				190 RJD	0 5m	
20210712 1821 1			60.1	67	57.601	168	4.287		% CS12.75	247	264		172 RJD	0.5	
20210712 1840 1 20210712 1845 1			53.6 53.3	67 67	59.224 59.35	167 167	59.388 59.287		% CS13 % CS13	21/	264		211 RJD 177 RJD	0 5m	
20210712 1845 1 20210712 1846 5			53.3	67	59.35	167	59.287	-	% CS13 Laramie		45		177 RJD 190 RJD	0 5m	Stopped operations due to sea state
20210712 1855 5			53.1	67	59.353	167	59.273	U	% CS13 Laramie	3	43		187 RJD	0 3111	Recovery postion missing - set to be same as deploy did have lon at 167 59.23
20210712 1035 2			53.9	67	59.242	167		Λ	% CS13 caranne	217	265		201 KC	0 5m	Operatings are back on Il Repeat station for CS13. Placed zip ties on exhaust end of SBE 43 system 2 to secure them better (as per suggested by Seabird)
	1 108		53.5	67	59.318	167	59,424		% CS13	217	203		211 KC	0 3	operations are stated in inspect stated in the Gasting in the Gast
	1 109		51.1	68	0.904	167			% CS13.25	217	263		195 KC	0 5m	
20210713 51 1	1 109	2	51.3	68	0.976	167	54.626	0	% CS13.25			25.4	170 KC		
	1 110		52.7	68	2.63	167	49.819	0	% CS13.5	218	267		219 KC	0 4m	Had one of the larger rolls we've seen in the cruise so far (knocked a viny float out of the wire basket on the 01 deck, could hear it rolling around from the lab). No
113 1	1 110		53.1	68	2.72	167	49.82		% CS13.5				184 KC		
20210713 132 1			52.6	68	4.339	167	44.873	0	% CS13.75	217	266		189 KC	0 3m	
	1 111		53	68	4.417	167	44.854		% CS13.75				174 KC		
20210713 155 1			51.7	68	6.061	167			% CS14	217	265		216 KC	0 4m	
	1 112		51.6	68	6.158	167		0.5	% CS14				196 KC		
	5 22		51.2	68	6.171	167	40.079		% CS14 Laramie	5	45		203 KC	0	
0210713 203 3	5 22	2	50.5	68	6.37	167	40.165		% CS14 Laramie				193 KC		
20210713 225 1				68	7.54	167			% CS14.25	218	261		209 KC	0 4m	Swell seems to be shrinking a bit; hopeful the trend will continue
	1 113		48.9	68	7.624	167	35.4	0	% CS14.25	247	222		179 KC	0.4	CTD areas and of the number before active drawn Datasead to each death and days.
20210713 246 1 20210713 249 1			47.8 47.8	68 68	9.049 9.095	167 167	30.863 30.945	0	% CS14.5 % CS14.5	217	222		166 KC 145 KC	0 4m	CTD came out of the water before going down. Returned to soak depth and started a new cast to be safe.
	1 114		47.8 47.8	68	9.095	167	30.945		% CS14.5 % CS14.5	217	261		145 KC 145 KC	0 4m	Data coopy all good own after surface breach in cost before
20210713 249 1 20210713 255 1			47.8	68	9.095	167	30.945		% CS14.5 % CS14.5	21/	201		145 KC	U 4M	Data seems all good even after surface breach in cast before
0210713 255 1				68	10.564	167	26.18	-	% CS14.75	218	261		198 KC	0 4m	
	1 116		47.1	68	10.564	167	26.187		% CS14.75	210	201		151 KC	0 4111	
0210713 316 1			46.9	68	12.039	167	21.467		% CS15.	218	261		151 KC	0 4m	CTD moved a bit under the stern, but we couldn't "bump forward" since the pumping sample had already started.
	1 117			68	12.149	167	21.546		% CS15				183 KC		, , , , , , , , , , , , , , , , , , , ,
	5 23		46.9	68	12.145	167	21.543		% CS15 Laramie	5	45		185 KC		
0210713 347 5		2	46.8	68	12.301	167	21.665		% CS15 Laramie				179 KC		
0210713 403 1			44.4	68	13.548	167	16.686	0	% CS15.5	217	256		187 KC	0 4m	
	1 118		45.1	68	13.653	167	16.706	0	% CS15.5				154 KC		
20210713 424 1			43.3	68	14.955	167	12.324		% CS16	217	261		174 KC	0 4m	
	1 119		43.5	68	15.09	167	12.505	0	% CS16				147 KC		
	5 24		43.5	68	15.106	167	12.514		% CS16 Laramie	5	40		124 KC	0 4m	
	5 24	2	44	68	15.302	167	12.513		% CS16 Laramie				121 KC		
20210713 457 1				68	16.572	167			% CS16.5	217	252		134 KC	0 4m	
20210713 501 1			40.4	68	16.649	167	7.622		% CS16.5				166 KC		
20210713 518 1				68	17.94	167			% CS17	217	249		146 KC	0 3m	Pt. Hope visible
20210713 522 1			36.9	68	18.002	167	3.065	Ω	% CS17			16.5	141 KC		

20210713 523 5			36.7	68	18.021	167	3.066		% CS17 Laramie	5	35		139 KC	0 3m	
20210713 531 5			37.2	68	18.161	167	3.105		% CS17 Laramie				137 KC		
	1 122		32.4	68	18.854	166			% CS18	216	247		151 KC	0 2m	
20210713 555 1	1 122	2	33	68	18.902	166	58.159	0	% CS18			20.8	144 KC		
20210713 620 1	1 123	1	25.7	68	19.873	166	52.483	0	% CS19	217	241	15.7	134 KC	0 1.5m	
	1 123	2	26.2	68	19.928	166	52.843	0	% CS19			18.8	148 KC		
0210713 712 1	1 124	1	35.4	68	22.411	167	8.09	0	% NPH1	217	250	20	137 JG	0 2m	
0210713 715 1	1 124	2	35.7	68	22,555	167	8.235	0	% NPH1				179 JG		
	1 125	1	40	68	22.662	167		•	% NPH2	217	256		175 JG	0 2m	
	1 125	2	39.7	68	22.791	167			% NPH2	21/	230		141 JG	0 2111	
	1 126	1	39.8	68	22.871	167			% NPH3	217	256		148 JG	0 3m	
	1 126	2	39.6	68	22.952	167			% NPH3				141 JG		
0210713 755 1		1	40.1	68	23.11	167			% NPH4	217	256		136 JG	0 3m	
0210713 759 1	1 127	2	39.6	68	23.218	167	18.001	0	% NPH4			19.5	178 JG		
0210713 811 1	1 128	1	41.8	68	23.357	167	21.527	0	% NPH5	216	258	10.1	129 JG	0 3m	
0210713 815 1	1 128	2	41.2	68	23.49	167	21.5	0	% NPH5			19.3	172 JG		
0210713 835 1	1 129	1	46	68	23.804	167	28.167	0	% NPH6	217	263	17.8	138 JG	0 3m	
0210713 839 1	1 129	2	46.1	68	23.882	167	28.26	0	% NPH6			15.1	166 JG		
	1 130	1	49.1	68	24.284	167			% NPH7	216	264		145 JG	0 4m	
	1 130	2	49.3	68	24.36	167			% NPH7	210	201		137 JG	0 -1111	
	1 131	1	51.3	68	24.768	167			% NPH8	217	267		135 JG	0 3m	Wildfire smaller mark of the marries
										21/	207			0 3111	Wildfire smoke most of the morning
	1 131	2	51.2	68	24.885	167	41.713		% NPH8		262		186 JG		
0210713 1012 1			52.5	68	25.195	167			% NPH9	217	268		140 JG	0 4m	
0210713 1017 1		2	52.7	68	25.274	167			% NPH9				128 JG		
0210713 1036 1			52.7	68	25.728	167			% NPH10	217	268		143 JG	0 4m	
0210713 1041 1	1 133	2	53	68	25.851	167	55.151	0	% NPH10			14.5	120 JG		
0210713 1102 1	1 134	1	52.1	68	26.229	168	1.927	0	% NPH11	217	267	17.1	169 JG	0 4m	
0210713 1107 1		2	51.8	68	26.306	168			% NPH11				153 JG		
0210713 1127 1	1 135	1	51	68	26.704	168	8.796	0	% NPH11.5	217	265	15.9	154 JG	0 4m	Vent plug for T1/C1 didn't drain. Cleaned both after Cast 135
0210713 1132 1		2	50.7	68	26.809	168			% NPH11.5				161 JG		
0210713 1151 1		1	50.7	68	27.132	168			% NPH12	217	264		121 JG	0 4m	Vent plug drained after cleaning
20210713 1151 1		2	50.4	68	27.132	168			% NPH12	-11	204		138 JG	U -#111	
					27.181	168			% NPH12.5	247	264		111 JG	0 4m	
0210713 1215 1			51.3	68						21/	264			0 4m	
20210713 1220 1		2	51.2	68	27.672	168			% NPH12.5				121 JG		
0210713 1239 1			50.7	68	28.948	168			% NPH13	216	264		141 JG	0 4m	
0210713 1244 1		2	50.6	68	28.997	168			% NPH13				123 JG		
0210713 1509 1		1	50.8	68	37.036	167			% CD14	217	262		135 RJD	1 2M	
0210713 1518 1	1 139	2	50.8	68	37.121	167	40.991	0	% CD14			11	162 RJD		
20210713 1533 1	1 140	1	49.4	68	36.884	167	35.696	0	% CD13	218	261	9	157 RJD	1 3m	
0210713 1537 1	1 140	2	49.3	68	36.894	167	35.641	0	% CD13			8	153 RJD		
20210713 1553 1	1 141	1	47.5	68	36.96	167	29.911	0	% CD12	218	261		148 RJD	1 3m	
20210713 1557 1		2	47.8	68	37.027	167			% CD12	210	201		131 RJD	2 5	
20210713 1613 1		1	45.1	68	36.961	167			% CD11	218	257		137 RJD	1 2m	
		2	45.1	68	37.012	167			% CD11	210	231		140 RJD	1 2111	
20210713 1618 1										240	25.4			4 2	
20210713 1634 1			42.3	68	37.011	167	18.65			218	254		155 RJD	1 3m	
20210713 1640 1		2	42.1	68	37.001	167			% CD10				120 RJD		
20210713 1654 1		1	38.8	68	36.946	167			% CD9	218	252		174 RJD	1 2m	
20210713 1658 1		2	39	68	37.024	167			% CD9				18 RJD		
20210713 1713 1		1	36.1	68	36.98	167	7.749	0	% CD8	218	249		151 RJD	1 2m	
20210713 1718 1		2	36.1	68	37.05	167			% CD8				120 RJD		
20210713 1731 1	1 146	1	34.7	68	36.962	167	2.269	0	% CD7	218	246	10	167 RJD	1 2m	
20210713 1735 1		2	34.7	68	37.027	167			% CD7				142 RJD		
20210713 1750 1		1	33.4	68	36.958	166			% CD6	218	248		145 RJD	1 2m	
20210713 1754 1		2	33.4	68	37.006	166			% CD6				170 RJD		
										210	245			1 2m	
0210713 1810 1		1	32.4	68	36.982	166			% CD5	218	245		178 RJD	1 3m	
0210713 1814 1		2	32.3	68	37.032	166			% CD5				121 RJD		
0210713 1829 1			31.8	68	36.982	166	45.49			218	246		180 RJD	1 3m	
0210713 1833 1			31.6	68	37.024	166			% CD4				178 RJD		
0210713 1845 1		1	31	68	37.001	166			% CD3	218	246		180 RJD	1 3m	
0210713 1850 1	1 150	2	31.1	68	37.082	166	39.619	0	% CD3			12	160 RJD		
0210713 1902 1	1 151	1	30.1	68	36.975	166	34.521	0	% CD2	218	245	9	190 RJD	1 3m	
0210713 1906 1	1 151	2	30	68	37.046	166	34.174	0	% CD2			10	167 RJD		
0210713 1919 1		1	26.7	68	37.02	166			% CD1	218	242		180 RJD	1 2m	
0210713 1919 1		2	26.7	68	37.146	166			% CD1	210	242		170 RJD	1 2111	
0210/13 1923										210	240			0.1	
0210712 2127				68	54.374	166	19.948			218	240		17 RJD	0 1m	
		2	26.7	68	54.394	166		-	% LIS1			3	47 RJD		
0210713 2130 1		1	26.5	68	54.4	166	20.051		% LIS1 Laramie	5	25	3		0 1m	Put out 30m of tubing by mistake, hit the bottom. Pulled up to 25m before turning on pump
0210713 2130 1 0210713 2131 5	5 26		26.4	68	54.394	166	20.011		% LIS1 Laramie			4	16 RJD		
0210713 2130 1 0210713 2131 5 0210713 2140 5	5 26 5 26	2					24.958	1	% LIS2	218	244		14 RJD	0 1m	
0210713 2130 1 0210713 2131 5 0210713 2140 5	5 26 5 26	2	31.2	68	54.756	166						2	340 RJD		
0210713 2130 1 0210713 2131 5 0210713 2140 5 0210713 2153 1	5 26 5 26 1 154	2		68 68	54.756 54.753	166		1	% LIS2					0 1m	018 water sample as well as a nutrient/trace metal sample.Laramie/Rebecca
0210713 2127 2 0210713 2130 2 0210713 2131 2 0210713 2140 2 0210713 2153 2 0210713 2156 2 0210713 2200 5	5 26 5 26 1 154 1 154	2 1 2	31.2 31.3	68	54.753	166	25.138			5	5	2	27 RID		
0210713 2130 1 0210713 2131 5 0210713 2140 5 0210713 2153 1 0210713 2156 1 0210713 2200 5	5 26 5 26 1 154 1 154 5 27	2 1 2 0	31.2 31.3 31.3	68 68	54.753 54.753	166 166	25.138 25.138		% LIS2 Laramie + water sample				27 RJD		
0210713 2130 : 0210713 2131 : 0210713 2140 : 0210713 2153 : 0210713 2156 : 0210713 2200 : 0210713 2200 :	5 26 5 26 1 154 1 154 5 27 5 27	2 1 2 0 0	31.2 31.3 31.3 31.3	68 68 68	54.753 54.753 54.753	166 166 166	25.138 25.138 25.138		 LIS2 Laramie + water sample LIS2 Laramie + water sample 	5	5	2	27 RJD	0 1m	Surface sample, so no finish position
0210713 2130 2 0210713 2131 5 0210713 2140 5 0210713 2153 2 0210713 2156 1 0210713 2200 5 0210713 2200 5 0210713 2200 5 0210713 2215 1	5 26 5 26 1 154 1 154 5 27 5 27 1 155	2 1 2 0 0	31.2 31.3 31.3 31.3 32.4	68 68 68 68	54.753 54.753 54.753 55.144	166 166 166 166	25.138 25.138 25.138 30.365	1	% LIS2 Laramie + water sample % LIS2 Laramie + water sample % LIS3	5		2 4	27 RJD 277 RJD		
0210713 2130 2 0210713 2131 5 0210713 2140 5 0210713 2153 1 0210713 2153 2 0210713 2200 5 0210713 2200 5 0210713 2215 2 0210713 2215 2	5 26 5 26 1 154 1 154 5 27 5 27 1 155 1 155	2 1 2 0 0 1 2	31.2 31.3 31.3 31.3 32.4 32.7	68 68 68 68 68	54.753 54.753 54.753 55.144 55.145	166 166 166 166 166	25.138 25.138 25.138 30.365 30.503	1	 LIS2 Laramie + water sample LIS2 Laramie + water sample LIS3 LIS3 	5 218	5 241	2 4 5	27 RJD 277 RJD 300 RJD	0 1m 0 1m	Surface sample, so no finish position
0210713 2130 2 0210713 2131 5 0210713 2141 5 0210713 2155 2 0210713 2156 2 0210713 2200 5 0210713 2200 5 0210713 2215 2 0210713 2215 2 0210713 2219 5	5 26 5 26 1 154 1 154 5 27 5 27 1 155 1 155 5 28	2 1 2 0 0 1 2	31.2 31.3 31.3 31.3 32.4 32.7 32.7	68 68 68 68 68 68	54.753 54.753 54.753 55.144 55.145 55.146	166 166 166 166 166	25.138 25.138 25.138 30.365 30.503 30.525	1	 LIS2 Laramie + water sample LIS2 Laramie + water sample LIS3 LIS3 LIS3 LIS3 Laramie+watersample 	5 218	5	2 4 5 7	27 RJD 277 RJD 300 RJD 300 RJD	0 1m	
0210713 2130 2 0210713 2131 5 0210713 2141 5 0210713 2155 2 0210713 2156 2 0210713 2200 5 0210713 2200 5 0210713 2215 2 0210713 2215 2 0210713 2219 5	5 26 5 26 1 154 1 154 5 27 5 27 1 155 1 155 5 28	2 1 2 0 0 1 2	31.2 31.3 31.3 31.3 32.4 32.7	68 68 68 68 68 68 68	54.753 54.753 54.753 55.144 55.145	166 166 166 166 166	25.138 25.138 25.138 30.365 30.503	1	 LIS2 Laramie + water sample LIS2 Laramie + water sample LIS3 LIS3 	5 218	5 241	2 4 5 7	27 RJD 277 RJD 300 RJD	0 1m 0 1m	Surface sample, so no finish position
0210713 2130 2 0210713 2131 5 0210713 2140 5 0210713 2153 2 0210713 2156 1 0210713 2200 5 0210713 2200 5 0210713 2200 5 0210713 2215 1	5 26 5 26 1 154 1 154 5 27 5 27 1 155 1 155 5 28 5 28	2 1 2 0 0 1 2 1 2	31.2 31.3 31.3 31.3 32.4 32.7 32.7	68 68 68 68 68 68	54.753 54.753 54.753 55.144 55.145 55.146	166 166 166 166 166	25.138 25.138 25.138 30.365 30.503 30.525 30.515	1	 LIS2 Laramie + water sample LIS2 Laramie + water sample LIS3 LIS3 LIS3 LIS3 Laramie+watersample 	5 218	5 241 25	2 4 5 7 6	27 RJD 277 RJD 300 RJD 300 RJD	0 1m 0 1m	Surface sample, so no finish position
0210713 2130 2 0210713 2131 5 0210713 2131 5 0210713 2153 3 0210713 2156 2 0210713 2200 5 0210713 2215 2 0210713 2215 2 0210713 2215 2 0210713 2219 5 0210713 2219 5	5 26 5 26 1 154 1 154 5 27 5 27 1 155 1 155 5 28 5 28 1 156	2 1 2 0 0 1 2 1 2	31.2 31.3 31.3 31.3 32.4 32.7 32.7 32.6	68 68 68 68 68 68 68	54.753 54.753 54.753 55.144 55.145 55.146 55.161	166 166 166 166 166 166	25.138 25.138 25.138 30.365 30.503 30.525 30.515 38.374	1 1 0.5	LIS2 Laramie + water sample LIS2 Laramie + water sample LIS3 LIS3 LIS3 LIS3 LIS3 Laramie+watersample LIS3 Laramie+water sample	5 218 5	5 241 25	2 4 5 7 6 2	27 RJD 277 RJD 300 RJD 300 RJD 310 RJD	0 1m 0 1m 0 1m	Surface sample, so no finish position
0210713 2130 2 0210713 2140 5 0210713 2140 5 0210713 2156 2 0210713 2156 2 0210713 2200 5 0210713 2200 5 0210713 2219 2 0210713 2219 2 0210713 2219 2 0210713 2219 2 0210713 2219 2 0210713 2219 2	5 26 5 26 1 154 1 154 5 27 5 27 1 155 1 155 5 28 5 28 1 156 1 156	2 1 2 0 0 1 2 1 2	31.2 31.3 31.3 31.3 32.4 32.7 32.7 32.6 39.7	68 68 68 68 68 68 68 68	54.753 54.753 54.753 55.144 55.145 55.146 55.161 55.789	166 166 166 166 166 166 166 166	25.138 25.138 25.138 30.365 30.503 30.525 30.515 38.374 38.494	1 1 0.5	LIS2 Laramie + water sample LIS2 Laramie + water sample LIS3 LIS3 LIS3 LIS3 Laramie+water sample LIS4 Laramie+water sample LIS4	5 218 5 218	5 241 25	2 4 5 7 6 2 2	27 RJD 277 RJD 300 RJD 300 RJD 310 RJD 312 RJD	0 1m 0 1m 0 1m	Surface sample, so no finish position

20210713														
			1 4		8 56.992	166			% LIS6	217	259	9.9 79.2 K		Spike in one of the oxygen sensor on the way down. The rest of the data seemed fine. Pumps were draining fine after.
20210713			2 4			166		-	% LIS6			11.9 105 K	-	
20210714	10 1	159	1 45	.2 6	8 57.603	167	1.888	0 9	% LIS6.5	217	261	9.1 81.4 K	1 2m	
20210714	15 1	159	2 45	i.3 6	8 57.66	167	2.041	0 9	% LIS6.5			25.2 120 KG	2	
20210714	16 5	29	1 45	i.3 6	8 57.668	167	2.058		% LIS6.5 Laramie	5	40	23 128 KG	1 2m	Started pouring rain at the end of the cast, pretty much cleared up during transit to next cast
20210714	23 5	29	2 4	.2 6	8 57.712	167	2.29		% LIS6.5 Laramie			19.3 118 KG		
20210714	42 1		1 4		8 58.186	167	9.285	0 9	% LIS7	217	261	11.3 114 KG		
20210714			2 4			167	9.5		% LIS7	217	201	17.6 122 KG		
	105 1		1 45		8 58.789	167			% LIS7.5	21/	261	16 113 K		
20210714	110 1		2 45			167			% LIS7.5			14.8 115 K		
20210714	130 1	162	1 46	5.1 6	8 59.42	167	23.9	0 9	% LIS8	217	259	12.4 114 KG	1 2m	
20210714	134 1	162	2 46	i.2 6	8 59.41	167	23.975	0 9	% LIS8			9.1 108 KG	:	
20210714	135 5		1 45			167	23.981		% LIS8 Laramie	5	40	9.5 115 KG		
	143 5		2 4			167	24.023		% LIS8 Laramie		-10	3.7 87.2 KG		
										247	204			Clare to the facility of other times and times and times and times and times are the clare to th
	211 1		1 46		9 0.197	167			% LIS8.5	217	261	5.4 344 KG		Skipping LIS9 for the Q cable LIS8.5 and LIS9.5 instead
	216 1		2 46			167		-	% LIS8.5			9.8 30.1 K	-	
20210714	243 1	164	1 4	'.6 6	9 0.979	167	43.598	0 9	% LIS9.5	217	261	9.7 10.4 K	1 3m	
20210714	248 1	164	2 4	'.6	9 1.069	167	43.665	0 9	% LIS9.5			11.3 50.7 KG		
20210714	317 1		1 4			167	53.397		% LIS10	217	260	16.2 50.3 KG		
20210714	321 1		2 4			167	53.464		% LIS10			18.5 44.3 KG		
		166	1 48		9 1.334	168			% LIS11	216	261	18.4 43.5 KG		
						168			% LISTI % LISTI	210	201	18.6 32.1 KG		
20210714	405 1							-						
20210714	406 5		1 48		9 1.384	168			% LIS11 Laramie	5	45	16.9 45.3 KG		
	414 5		2 48			168	8.291		% LIS11 Laramie			19.5 56.1 KG		
20210714	450 1	167	1 49).2	9 0.882	168	22.5	0	% LIS12	216	262	15.5 73.3 KG	0.5 4m	Noticed the upcast was about equal speed (or slower) to downcast. When asked to speed up a bit, the winch seemed resistant to the idea. There was a slight hiccu
20210714	455 1	167	2 49).3 E	9 0.91	168	22.633	0 9	% LIS12			16.2 70.9 KG		
20210714	535 1	168	1 50	0.6	9 0.431	168	37.034	0	% LIS13	217	263	15.4 63.6 KG		Fog has cleared up into a fairly nice evening. Cast shows a nice cold/salty/turbid bottom layer in the last 5m or so.
20210714	540 1		2 50			168			% LIS13	217		14.8 71 KG		,,,,,,,,,,,,,,,,,,,
20210714	541 5		1 50		9 0.489	168			% LIS13 Laramie	5	5	14.5 67.4 KG		Filter tubing kept coming off when trying to sample at the surface, aborted bottom cast. No nutrient samples. Course of action: reattach same filter (to preserve a
						168				5	2			incer cooling kept coming on when trying to sample at the surface, aborted bottom cast, NO nutrient samples, Course or action: reattach same filter (to preserve a f
20210714	330 3					100	38.26		% LIS13 Laramie		26-	10.4 71.1 KG		
	613 1		1 5:			168			% LIS14n	217	265	12.4 45.8 KG		Still a nice little bottom layer showing up.
20210714	618 1		2 5:		9 0.255	168	46.835		% LIS14n			16.5 66 KG		
20210714	642 1		1 5		8 59.994	168			% CCL22n	216	265	15.5 77.4 KG		Interesting warm, salty bump around 20m; looking at coordinates, it seems we sampled at the old CCL22 location (168deg 56.2')
20210714	647 1		2 5			168			% CCL22n			15.6 68.5 KG		
20210714	649 5	33	1 5:	3 6	9 0.042	168	56.344	1	% CCL22n Laramie	45	45	17.6 75.7 KG	0 4m	Bottom sample only
20210714	654 5	33	2 5:	.3 6	9 0.065	168	56.553		% CCL22n Laramie			18.9 74.6 KG		
20210714	811 1	171	1 5	8 6	8 49.939	168	55.852	0	% CCL21	217	265	15.9 99.9 JO	1 4m	
20210714	816 1	171	2	52 6	8 49.944	168	55.948	0 9	% CCL21			15.5 77.9 JG	i	
20210714	930 1		1 5			168	55.975		% CCL20	217	264	15 107 JG		Fishy cast but cleared up on the upcast. Redid CTD cast at station. Next cast looks much cleaner. Missed a screenshot of 172
20210714	935 1		2 5:			168	55.984		% CCL20			11.9 98.9 JO		
	937 1		1 5:		8 39.995	168	56.046		% CCL20 redo	217	264	9.6 90.7 J		T/C 1 not draining. Cleaned vent plug after this cast.
	943 1		2 5:			168	56.261		% CCL20 redo	217	204	8.6 86.4 JO		176 I not draining. Cleaned vent plug arter this cast.
			1 5			168				247	200			
20210714									% CCL19	21/	266	14.1 112 JO		
20210714			2 5			168 168	56.06 49.368		% CCL19 % NPH14.5	247	265	9.6 244 JG		
										21/	205			
20210714			2 52		8 29.564	168	49.579		% NPH14.5			10.7 101 JC		
20210714					8 29.069	168	42.57		% NPH14	217	266	6.3 99.8 JO		
20210714				52 6		168	42.753		% NPH14			7 94.7 JO		
20210714	1223 1	177	1 5	.1 6	8 28.6	168	35.755	0 7	% NPH13.5	217	265	7.2 150 JG	i 1 4m	
20210714			2 5			168	35.779	-	% NPH13.5			10.7 121 JO	i	
20210714	1250 1	178	1 50	0.6	8 28.045				ALDULA D					
	1255 1					168	29.082	0 9	% NPH13	21/	265	5 67.8 JG	0 4m	
20210714										21/	265			
					8 28.046	168 168	29.082 29.338 22.181	0 9	% NPH13 % NPH13 % NPH12.5		265	8.8 145 JO	i	
	1321 1	179	1 5	3 6	8 28.046 8 27.613	168 168	29.338 22.181	0 9	% NPH13 % NPH12.5			8.8 145 JG 7.9 148 JG	i 0 4m	
20240744	1321 1	179 179	1 5: 2 5:	3 6	8 28.046 8 27.613 8 27.677	168 168 168	29.338 22.181 22.266	0 9	% NPH13 % NPH12.5 % NPH12.5	217	265	8.8 145 JG 7.9 148 JG 4.8 105 JG	i 0 4m	
	1343 1	179 179 180	1 5: 2 5: 1 50	3 6 3 6	8 28.046 8 27.613 8 27.677 8 27.096	168 168 168 168	29.338 22.181 22.266 15.418	0 9	% NPH13 % NPH12.5 NPH12.5 % NPH12	217		8.8 145 JG 7.9 148 JG 4.8 105 JG 4.2 112 JG	0 4m	
20210714	1343 1 1348 1	179 179 180 180	1 5: 2 5: 1 5: 2 5:	3 6 3 6 3 6 4 6	8 28.046 8 27.613 8 27.677 8 27.096 8 27.137	168 168 168 168	29.338 22.181 22.266 15.418 15.681	0 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	% NPH13 % NPH12.5 % NPH12.5 % NPH12 % NPH12	217	265 264	8.8 145 JG 7.9 148 JG 4.8 105 JG 4.2 112 JG 7 106 JG	i 0 4m	
20210714 20210714	1343 1 1348 1 1410 1	179 179 180 180 181	1 5: 2 5: 1 5: 2 5: 1 5: 1 5:	3 6 3 6 3 6 4 6 7 6	8 28.046 8 27.613 8 27.677 8 27.096 8 27.137 8 26.673	168 168 168 168 168	29.338 22.181 22.266 15.418 15.681 8.7	0 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	% NPH13 % NPH12.5 % NPH12.5 % NPH12 % NPH12 % NPH11.5	217	265	8.8 145 JG 7.9 148 JG 4.8 105 JG 4.2 112 JG 7 106 JG 7.3 142 JG	0 4m 0 4m 0 5m	
20210714 20210714	1343 1 1348 1 1410 1	179 179 180 180 181	1 5: 2 5: 1 5: 2 5:	3 6 3 6 3 6 4 6 7 6	8 28.046 8 27.613 8 27.677 8 27.096 8 27.137 8 26.673	168 168 168 168	29.338 22.181 22.266 15.418 15.681 8.7	0 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	% NPH13 % NPH12.5 % NPH12.5 % NPH12 % NPH12	217	265 264	8.8 145 JG 7.9 148 JG 4.8 105 JG 4.2 112 JG 7 106 JG	0 4m 0 4m 0 5m	
20210714 20210714 20210714	1343 1 1348 1 1410 1 1415 1	179 179 180 180 181 181	1 5: 2 5: 1 5: 2 5: 1 5: 1 5:	3 6 3 6 3 6 4 6 7 6	8 28.046 8 27.613 8 27.677 8 27.096 8 27.137 8 26.673 8 26.752	168 168 168 168 168	29.338 22.181 22.266 15.418 15.681 8.7	0 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	% NPH13 % NPH12.5 % NPH12.5 % NPH12 % NPH12 % NPH11.5	217 217 217	265 264	8.8 145 JG 7.9 148 JG 4.8 105 JG 4.2 112 JG 7 106 JG 7.3 142 JG	0 4m 0 4m 0 5m	
20210714 20210714 20210714 20210714	1343 1 1348 1 1410 1 1415 1 1435 1	179 179 180 180 181 181 181	1 5: 2 5: 1 50 2 50 1 50 2 50 1 5:	3 6 3 6 3 6 4 6 7 6 7 6	8 28.046 8 27.613 8 27.677 8 27.096 8 27.137 8 26.673 8 26.752 8 26.177	168 168 168 168 168 168	29.338 22.181 22.266 15.418 15.681 8.7 8.611 1.947	0 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	% NPH13 % NPH12.5 % NPH12.5 % NPH12 % NPH12 % NPH12 % NPH11.5 % NPH11.5 % NPH11.5	217 217 217	265 264 265	8.8 145 JG 7.9 148 JG 4.8 105 JG 4.2 112 JG 7 106 JG 7.3 142 JG 6.5 130 JG 6.2 168 JG	0 4m 0 4m 0 5m 0 5m	
20210714 20210714 20210714 20210714 20210714 20210714 20210714	1343 1 1348 1 1410 1 1415 1 1435 1 1441 1	179 179 180 180 181 181 181 182 182	1 5: 2 5: 1 5(2 5(1 5(2 5(1 5: 2 5(2 5:	3 6 3 6 3 6 4 6 7 6 7 6 8 6	8 28.046 8 27.613 8 27.677 8 27.096 8 27.137 8 26.673 8 26.752 8 26.177 8 26.238	168 168 168 168 168 168 168 168	29.338 22.181 22.266 15.418 15.681 8.7 8.611 1.947 1.873	0 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	% NPH13 % NPH12.5 % NPH12.5 % NPH12 % NPH12 % NPH11 % NPH11.5 % NPH11.5 % NPH11.5 % NPH11 % NPH11	217 217 217 217	265 264 265 266	8.8 145 JG 7.9 148 JG 4.8 105 JG 4.2 112 JG 7 106 JG 7.3 142 JG 6.5 130 JG 6.2 168 JG 5.6 134 JG	0 4m 0 4m 0 5m 0 5m	((G) input 10.5 as the SRF header. It's NPH10.
20210714 20210714 20210714 20210714 20210714 20210714	1343 1 1348 1 1410 1 1415 1 1435 1 1441 1 1501 1	179 179 180 180 181 181 181 182 182 183	1 5: 2 5: 1 5(2 5) 1 5(2 5) 2 5(2 5) 1 5: 2 5: 1 5:	3 6 3 6 3 6 4 6 7 6 7 6 8 6 9 6	8 28.046 8 27.613 8 27.677 8 27.096 8 27.137 8 26.673 8 26.752 8 26.177 8 26.238 8 25.751	168 168 168 168 168 168 168 168 168	29.338 22.181 22.266 15.418 15.681 8.7 8.611 1.947 1.873 55.188	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	% NPH13 NPH12.5 NPH12.5 NPH12.5 NPH12 NPH11 NPH11.5 NPH11.5 NPH11.5 NPH11 NPH10 NPH10	217 217 217 217	265 264 265	8.8 145 JG 7.9 148 JG 4.8 105 JG 7 106 JG 7.3 142 JG 6.5 130 JG 6.2 168 JG 5.6 134 JG 6.3 134 JG	0 4m 0 4m 0 5m 0 5m 0 5m	I (JG) input 10.5 as the SBE header. It's NPH10.
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20210714 20210714	1343 1 1348 1 1410 1 1415 1 1435 1 1441 1 1501 1 1506 1 1529 1 1535 1 1602 1 1627 1 1647 1 1650 1 1709 1 1709 1 1714 1 1724 1	179 179 180 181 181 182 183 183 184 185 186 187 188 188	1 5: 2 5: 1 50 2 5: 1 5: 2 5: 1 5: 2 5: 1 5: 2 5: 1 5: 2 5: 1 4: 2 4: 1 4: 2 4: 2 4: 2 4: 2 5: 1 4: 2 5: 2 5: 2 5: 2 5: 2 5: 2 5: 2 5: 2 5	3.3 6.3 6.3 6.3 6.3 6.4 6.5 6.5 6.5 6.5 6.5 6.5 6.5 6.5 6.5 6.5	8 28.046 8 27.613 8 27.677 8 27.096 8 27.137 8 26.673 8 26.752 8 26.177 8 26.238 8 25.251 8 25.234 8 25.254 8 24.872 24.872 24.872 24.872 24.872 23.871 8 23.847 8 23.847 8 23.848 8 23.848 8 23.848 8 23.849 8 23.849	168 168 168 168 168 168 168 168 168 167 167 167 167 167 167 167 167 167 167	29.338 22.181 22.266 15.418 15.681 8.7 8.611 1.947 1.873 55.188 55.245 48.441 48.372 41.604 41.457 34.751 28.083 27.961 21.362 21.265	O O O O O O O O O O O O O O O O O O O	% NPH13 NPH12.5 % NPH12.5 % NPH12.5 % NPH12 % NPH12 % NPH11.5 % NPH11.5 % NPH11.5 % NPH11 % NPH10 NPH10 % NPH10 % NPH10 % NPH5 % NPH5 % NPH8 % NPH7 % NPH6 % NPH6 % NPH5 % NPH5 % NPH5 % NPH5	217 217 217 217 218 218 218 217 218 218 218	265 264 265 266 267 265 263 262	8.8 145 JC 4.8 105 JC 4.8 105 JC 4.2 112 JC 7.3 142 JC 6.5 130 JC 6.6 134 JC 6.6 126 JC 6.7 111 R 6 12 R 8 121 R 8 121 R 8 121 R 10 190 R 10 191 R 6 153 R 6 154 JC 6 154 JC 6 147 R 8 144 R 8 144 R 8 144 R 8 144 R	0 4m 0 0 4m 0 0 5m	I (JG) input 10.5 as the SBE header. It's NPH10.
20210714 20210714	1343 1 1348 1 1410 1 1415 1 1435 1 1441 1 1501 1 1506 1 1529 1 1535 1 1602 1 1622 1 1627 1 1647 1 1650 1 1709 1 1714 1 1729 1	179 179 180 180 180 181 181 182 182 183 183 184 184 184 185 186 186 187 188 188 189	1 5: 2 5: 1 5: 2 5: 1 5: 2 5: 1 5: 2 5: 1 5: 2 5: 1 5: 2 5: 1 5: 2 4: 1 4: 2 4: 1 5: 1 5: 1 6: 1 6: 1 6: 1 6: 1 7: 1 7: 1 7: 1 7: 1 7: 1 7: 1 7: 1 7	3 6.3.3 6.	8 28.046 8 27.613 8 27.613 8 27.096 8 27.137 8 26.673 8 26.752 8 26.177 8 26.238 8 25.751 8 25.85 8 25.85 8 25.234 8 24.872 8 24.872 8 24.372 8 24.372 8 23.871 8 23.871 8 23.871 8 23.873 8 23.871 8 23.873 8 23.874 8 23.436	168 168 168 168 168 168 168 168 167 167 167 167 167 167 167 167 167 167	29.338 22.181 22.266 15.418 15.681 8.7 8.611 1.947 1.873 55.188 55.245 48.441 48.372 41.604 41.457 34.751 28.083 27.961 21.362 21.265 18.037 17.892		% NPH13 % NPH12.5 % NPH12.5 % NPH12.5 % NPH12 % NPH12 % NPH11.5 % NPH11.5 % NPH11.5 % NPH10 % NPH0 % NPH0 % NPH0 % NPH9 % NPH9 % NPH8 % NPH5 % NPH5 % NPH6 % NPH5 %	217 217 217 217 218 218 218 217 218 218 218 218	265 264 265 266 267 265 263 262 259 253	8.8 145 LG 4.8 105 LG 4.8 105 LG 4.2 112 LG 7.3 142 LG 6.5 130 LG 6.5 134 LG 6.6 134 LG 7.4 117 LG 6 12 RR 8 141 R. 6 137 R. 6 137 R. 6 137 R. 6 148 LG 7.4 111 LG 7.4 111 LG 8 141 R. 8 121 R. 6 137 R. 8 121 R. 8 121 R. 9 137 R. 9 138 LG 10 190 R.	0 4m 0 0 4m 0 0 5m 0 0 3m 0 0 3m	I (JG) input 10.5 as the SBE header. It's NPH10.
20210714 20210714	1343 1 1348 1 1410 1 1415 1 1435 1 1441 1 1501 1 1502 1 1529 1 1535 1 1602 1 1602 1 1627 1 1647 1 1650 1 1709 1 1714 1 1724 1 1729 1 1714 1	179 179 180 180 181 181 181 182 182 183 183 183 184 184 185 185 186 186 187 187 188 188 189	1 5: 2 5: 1 5: 2 5: 1 5: 2 5: 1 5: 2 5: 1 5: 2 5: 1 4: 2 4: 1 4: 2 4: 2 4: 2 4: 2 4: 2 4: 2 4: 2 4: 2	3 6.3.3 6.	8 28.046 8 27.613 8 27.677 8 27.096 8 27.137 8 26.673 8 26.673 8 26.572 8 26.238 8 25.751 8 25.85 8 25.258 8 24.872 24.872 24.872 23.871 8 23.847 8 23.847 8 23.848 8 23.368 8 23.088 8 23.144 8 23.966	168 168 168 168 168 168 168 168 168 167 167 167 167 167 167 167 167 167 167	29.338 22.181 22.266 15.418 15.681 15.681 1.947 1.873 55.188 55.245 48.441 48.372 41.604 41.457 34.873 27.961 21.362 21.265 18.037 17.892		% NPH13 NPH12.5 % NPH12.5 % NPH12.5 % NPH12 % NPH12 % NPH11.5 % NPH11.5 % NPH11.5 % NPH11 % NPH10 NPH10 % NPH10 % NPH10 % NPH5 % NPH5 % NPH8 % NPH7 % NPH6 % NPH6 % NPH5 % NPH5 % NPH5 % NPH5	217 217 217 217 218 218 218 217 218 218 218 218	265 264 265 266 267 265 263 262 259	8.8 145 JC 4.8 105 JC 4.8 105 JC 4.1 12 JC 7.3 142 JC 7.4 117 JC 6 142 R 8 141 R 8 121 R 6 127 R 10 190 R 10 190 R 10 191 R 8 208 R 7 192 R	i 0 4m i 0 4m i 0 5m i	I (IG) input 10.5 as the SBE header. It's NPH10.
20210714 20210714	1343 1 1348 1 1410 1 1415 1 1435 1 1441 1 1501 1 1502 1 1529 1 1535 1 1602 1 1602 1 1627 1 1647 1 1650 1 1709 1 1714 1 1724 1 1729 1 1714 1	179 179 180 180 181 181 181 182 182 183 183 183 184 184 185 185 186 186 187 187 188 188 189	1 5: 2 5: 1 5: 2 5: 1 5: 2 5: 1 5: 2 5: 1 5: 2 5: 1 4: 2 4: 1 4: 2 4: 2 4: 2 4: 2 4: 2 4: 2 4: 2 4: 2	3 6.3.3 6.	8 28.046 8 27.613 8 27.677 8 27.096 8 27.137 8 26.673 8 26.673 8 26.572 8 26.238 8 25.751 8 25.85 8 25.258 8 24.872 24.872 24.872 23.871 8 23.847 8 23.847 8 23.848 8 23.368 8 23.088 8 23.144 8 23.966	168 168 168 168 168 168 168 168 167 167 167 167 167 167 167 167 167 167	29.338 22.181 22.266 15.418 15.681 8.7 8.611 1.947 1.873 55.188 55.245 48.441 48.372 41.604 41.457 34.751 28.083 27.961 21.362 21.265 18.037 17.892		% NPH13 % NPH12.5 % NPH12.5 % NPH12.5 % NPH12 % NPH12 % NPH11.5 % NPH11.5 % NPH11.5 % NPH10 % NPH0 % NPH0 % NPH0 % NPH9 % NPH9 % NPH8 % NPH5 % NPH5 % NPH6 % NPH5 %	217 217 217 217 218 218 218 217 218 218 218 218	265 264 265 266 267 265 263 262 259 253	8.8 145 LG 4.8 105 LG 4.8 105 LG 4.2 112 LG 7.3 142 LG 6.5 130 LG 6.5 134 LG 6.6 134 LG 7.4 117 LG 6 12 RR 8 141 R. 6 137 R. 6 137 R. 6 137 R. 6 148 LG 7.4 111 LG 7.4 111 LG 8 141 R. 8 121 R. 6 137 R. 8 121 R. 8 121 R. 9 137 R. 9 138 LG 10 190 R.	i 0 4m i 0 4m i 0 5m i	I (JG) input 10.5 as the SBE header. It's NPH10.
20210714 20210714	1343 1 1348 1 1410 1 1415 1 1415 1 1435 1 1501 1 1506 1 1529 1 1535 1 1602 1 1622 1 1627 1 1647 1 1709 1 1709 1 1714 1 1724 1 1741 1	179 179 179 180 180 181 181 181 182 182 183 184 184 185 186 186 186 187 187 188 189 190	1 5: 2 5: 1 5: 2 5: 1 5: 2 5: 1 5: 2 5: 1 5: 2 5: 1 4: 2 4: 1 4: 2 4: 2 4: 2 4: 2 4: 2 4: 2 4: 2 4: 2	3 6.3.3 6.	8 28.046 8 27.613 8 27.677 8 27.096 8 27.137 8 26.673 8 26.752 8 26.752 8 26.238 8 25.751 8 25.85 8 25.234 8 25.254 8 24.872 24.872 8 24.372 8 24.372 8 23.369 8 23.436 8 23.436 8 23.436 8 23.144 8 23.968 8 23.968	168 168 168 168 168 168 168 168 168 167 167 167 167 167 167 167 167 167 167	29.338 22.181 22.266 15.418 15.681 15.681 1.947 1.873 55.188 55.245 48.441 48.372 41.604 41.457 34.873 27.961 21.362 21.265 18.037 17.892		% NPH13 NPH12.5 % NPH12.5 % NPH12.5 % NPH12 % NPH12 % NPH11.5 % NPH11.5 % NPH11.5 % NPH10 % NPH10 % NPH10 % NPH9 % NPH9 % NPH9 % NPH8 NPH8 NPH8 NPH7 % NPH7 % NPH7 % NPH6	217 217 217 217 218 218 218 218 218 218 218 218	265 264 265 266 267 265 263 262 259 253	8.8 145 JC 4.8 105 JC 4.8 105 JC 4.1 12 JC 7.3 142 JC 7.4 117 JC 6 142 R 8 141 R 8 121 R 6 127 R 10 190 R 10 190 R 10 191 R 8 208 R 7 192 R	i 0 4m i 0 4m i 0 5m b 0 5m D 0 0 3m D 0 0 3m D 0 0 2m D 0 0 2m	I (JG) input 10.5 as the SBE header. It's NPH10.
20210714 20210714 20210714 20210714 20210714 20210714 20210714 20210714 20210714	1343 1 1348 1 1410 1 1415 1 1435 1 1441 1 1506 1 1509 1 1529 1 1535 1 1602 1 1622 1 1627 1 1650 1 1714 1 1724 1 1729 1 1741 1 1744 1 1754 1	179 179 179 180 180 181 181 182 183 183 184 185 186 186 186 187 187 188 188 189 190 190	1 5: 2 5: 1 5: 2 5: 1 5: 2 5: 1 5: 2 5: 1 5: 2 5: 1 4: 2 4: 1 4: 2 5: 2 5: 1 5: 2 5: 2 5: 2 5: 2 5: 2 5: 2 5: 2 5: 2	3 6.3.3 6.	8 28.046 8 27.613 8 27.613 8 27.096 8 27.137 8 26.673 8 26.752 8 26.177 8 26.238 8 25.751 8 25.234 8 25.234 8 24.299 8 24.372 8 23.871 8 23.847 8 23.436 8 23.436 8 23.028 8 23.028 8 23.028	168 168 168 168 168 168 168 168 168 167 167 167 167 167 167 167 167 167 167	29.338 22.181 22.266 15.418 15.681 15.681 1.947 1.873 55.188 55.245 48.441 48.372 41.604 41.457 34.87 34.751 28.083 27.961 21.362 21.265 18.037 17.892 14.631		% NPH13 NPH12.5 % NPH12.5 % NPH12.5 % NPH12 % NPH12 % NPH11.5 % NPH11.5 % NPH11.5 % NPH11 % NPH10 NPH10 % NPH9 NPH9 % NPH9 % NPH9 % NPH9 % NPH8 % NPH	217 217 217 217 218 218 218 218 218 218 218 218	265 264 265 266 267 265 263 262 259 253 253	8.8 145 JC 4.8 105 JC 4.8 105 JC 4.1 105 JC 7.3 142 JC 6.5 130 JC 6.5 134 JC 6.6 134 JC 6.6 148 141 JC 6 137 R 6 142 R 7 111 R 8 121 R 8 121 R 10 190 R 10 191 R 6 163 R 7 12 R 7 12 R 8 208 R 7 12 R	i 0 4m i 0 4m i 0 5m i 0 5m i 0 5m i 0 0 4.5m i 0 0 5m i 0 0 5m D 0 5m D 0 5m D 0 0 5m D 0 0 3m D 0 0 3m D 0 0 3m D 0 0 2m D 0 1M	I (JG) input 10.5 as the SBE header. It's NPH10.
20210714 20210714	1343 1 1348 1 1410 1 1415 1 1435 1 1441 1 1501 1 1506 1 1529 1 1535 1 1555 1 1602 1 1627 1 1647 1 1650 1 1714 1 1714 1 1714 1 1714 1 1714 1 1714 1 1714 1 1714 1 1714 1 1714 1 1714 1 1714 1 1714 1 1714 1 1714 1 1714 1 1714 1 1714 1	179 179 179 180 180 181 181 182 182 183 184 184 185 186 187 187 187 188 189 190 191	1 5: 5: 5: 1 5: 5: 5: 1 5: 5: 1 5: 5: 1 5	.3 6 6.3 6 6.3 6 6.3 6 6 6 6 6 6 6 6 6 6	8 28.046 8 27.613 8 27.613 8 27.096 8 27.137 8 26.673 8 26.752 8 26.177 8 26.238 8 25.751 8 25.234 8 25.234 8 24.299 8 24.372 8 23.871 8 23.847 8 23.436 8 23.436 8 23.028 8 23.028 8 23.028	168 168 168 168 168 168 168 168 168 167 167 167 167 167 167 167 167 167 167	29.338 22.181 22.266 15.418 15.681 15.681 1.947 1.873 55.188 55.245 48.441 48.372 41.604 41.457 34.87 34.751 28.083 27.961 21.362 21.265 18.037 17.892 14.631 14.645 11.354		% NPH13 % NPH12.5 % NPH12.5 % NPH12.5 % NPH12 % NPH12 % NPH11.5 % NPH11.5 % NPH10 % NPH0 % NPH0 % NPH0 % NPH0 % NPH0 % NPH9 % NPH8 % NPH8 % NPH8 % NPH8 % NPH8 % NPH5 % NPH6 % NP	217 217 217 217 218 218 218 218 218 218 218 218 218	265 264 265 266 267 265 263 262 259 253 253	8.8 145 LG 4.8 105 LG 4.8 105 LG 4.2 112 LG 7.3 142 LG 7.3 142 LG 5.6 130 LG 5.6 134 LG 7.4 117 LG 6 142 R 7 111 R 8 141 R 8 121 R 6 137 R 6 137 R 6 137 R 6 137 R 7 111 R 8 121 R 8 121 R 8 121 R 8 121 R 9 137 R 9 1	i 0 4m i 0 4m i 0 5m i	I (JG) input 10.5 as the SBE header. It's NPH10.

20210714 1918 1			25.7	68	19.978	166		% CS19	218	241		270 RJD	0 1m	
20210714 1923 1			25.3	68	19.672	166	52.425 1	,				270 RJD		
20210714 1937 1			32.3	68	18.852	166		% CS18	217	250		307 RJD	0 1m	
20210714 1941 1	1 194	2	32.4	68	18.837	166		% CS18				275 RJD		
20210714 1956 1			36.4	68	17.976	167		% CS17	218	251		226 RJD	0 1m	
20210714 2000 1	1 195	2	36.8	68	17.957	167	2.968 0	% CS17			3	237 RJD		
0210714 2016 1	1 196	1	40.1	68	16.662	167	7.602 0	% CS16.5	218	257	3	197 RJD	0 1m	
20210714 2020 1	1 196	2	40.2	68	16.638	167	7.837 0	% CS16.5			2	198 RJD		
0210714 2038 1	1 197	1	43.8	68	15.009	167	11.995 0	% CS16	218	259	4	181 RJD	0 3m	
20210714 2042 1	1 197	2	43.7	68	15.025	167	11.94 0	% CS16				192 RJD		
20210714 2100 1	1 198	1	44.7	68	13.553	167	16.953 0	% CS15.5	218	259		186 RJD	0 5m+	
	1 198	2	44.9	68	13.549	167	16.927 0		210	233		200 RJD	0 3	
20210714 2122 1			46.5	68	12.146	167	21.48 0		218	261		156 RJD	0 3m	
20210714 2122 2			46.8	68	12.140	167	21.48 0		210	201		182 RJD	0 3111	
			47						240	204			0.5	And the leaf of the control of the c
20210714 2146 1				68	10.623	167		% CS14.75	218	261		170 RJD	0 5m+	Mislabeled in Seasave header: CS14.5 instead of CS14.75
20210714 2149 1		2	46.9	68	10.617	167	26.04 0	,				195 RJD		Dead whale (grey?) spotted around this/the next station
20210714 2222 1			47.6	68	9.126	167	30.722 0		218	261		147 RJD	0 5m	Mislabeled in Seasave header: CS14 instead of CS14.5
20210714 2227 1	1 201	2	47.6	68	9.082	167	30.852 0					159 RJD		
20210714 2245 1	1 202	1	48.6	68	7.722	167	35.272 0	% CS14.25	218	262	9	168 RJD	0 5m+	Mislabeled in Seasave header: CS13.5 instead of CS14.25
20210714 2250 1	1 202	2	48.9	68	7.79	167	35.249 0	% CS14.25			8	184 RJD		
20210714 2310 1	1 203	1	51.3	68	6.068	167	40.028 0	% CS14	218	265	8	167 RJD	0 5m+	Mislabeled in Seasave header: CS13 instead of CS14
20210714 2315 1		2	51.2	68	6.102	167	39.986 0					168 RJD		
20210714 2334 1	1 204	1	52.5	68	4.371	167	44.941 0	% CS13.75	218	267	9.4	164 KC	0 5m	
20210714 2338 1		2	52.4	68	4.339	167	44.963 0					178 KC		
20210714 2356 1			52.7	68	2.713	167		% CS13.5	219	267		159 KC	0 5m+	Lovely fluorescence peak
	1 205	2	52.6	68	2.731	167	50.035 0		-225			163 KC		
	1 206	1			0.977	167	54.724 0		219	266		155 KC	0 5m+	
20210715 19 1			51.3 51.4	68 68	0.977	167	54.724 0	,	219	200		155 KC 151 KC	0 3111+	
									246	200			0.5	
20210715 44 1			53.3	67	59.268	167		% CS13	219	269		146 KC	0 5m	
20210715 49 1		2	53.4	67	59.277	167	59.612 0	/0 0313		275		140 KC	0.5	
	1 208		59.7	67	57.562	168		% CS12.75	218	275		154 KC	0 5m+	
	1 208	2	60	67	57.58	168	4.431 0					148 KC		
	1 209	1	57.4	67	55.819	168	9.321 0		220	272		155 KC	0 5m+	
	1 209		57.6	67	55.826	168	9.425 0					147 KC		
20210715 156 1	1 210	1	56.5	67	54.216	168	14.015 0	% CS12.25	219	276	11.7	143 KC	0.5 4m	
20210715 202 1	1 210	2	56.4	67	54.32	168	14.18 0	% CS12.25			12.4	145 KC		
20210715 227 1	1 211	1	54.9	67	52.515	168	18.814 0	% CS12	219	269	15.8	137 KC	1 4m	Fog is rollin' in
20210715 232 1			54.8	67	52.501	168	18.908 0					142 KC		
20210715 256 1			51.3	67	50.684	168	24.154 0		218	267		119 KC	1 5m	
20210715 301 1	1 212	2	51.3	67	50.7	168	24.188 0	% CS11.75			14.1	97.1 KC		
	1 213		49.4	67	48.87	168	29.482 0		218	264		185 KC	1 5m	
	1 213	2	49.5	67	48.859	168	29.515 0		210	204		198 KC	1 5111	
	1 214			67	47.13	168		% CS11.25	210	263		160 KC	0 5m	Fog has blown out around this station
	1 214		48.7	67	47.144	168	34.699 0		210	203		164 KC	0 3111	rog has blown out allouid this station
	1 214		48.5	67	47.144	168		% CS11.25 % CS11	210	263		155 KC	1 5m	Fog is back in, interesting moving between banks of fog through here
	1 215	2	48.6	67	45.274	168	39.85 0		218	203		158 KC	1 5111	rog is back in, interesting moving between banks or log through nere
	1 216		48.5	67	43.5	168	44.083 0		218	263		137 KC	1 5m	
	1 216		48.5	67	43.526	168	44.089 0					144 KC		
	1 217	1	48.6	67	41.723	168		% CS10.5	218	263		145 KC	1 5m	
	1 217		48.7	67	41.757	168	48.241 0	,				150 KC		
	1 218		48.6	67	39.857	168		% CS10.25	218	264		150 KC	1 5m	
20210715 536 1	1 218	2	48.6	67	39.936	168	51.81 0					137 KC		
	1 219		48.8	67	38.101	168	55.819 0	,	218	263		182 KC	1 5m	
20210715 602 1	1 219	2	48.9	67	38.159	168	55.74 0	% CS10			15.6	148 KC		
	1 220		48.5	67	35.015	168	55.899 0		217	264		172 KC	1 4m	Fog is thickening even more now
	1 220	2	48.5	67	35.087	168	55.823 0					163 KC		
	1 221		48.6	67	29.97	168		% CCL13	219	264		185 JG	1 5m	Fog sucks
	1 221		48.6	67	30.053	168	55.987 0					182 JG		
	1 222		48.5	67	24.944	168	55.984 0		218	264		169 JG	1 4.5m	Got close to bottom, sensors and everything looked fine on recovery. Weird T/S inversion at base of mixed layer in all sensors down and upcasts. Flushed T1/C1 up
	1 222		48.5	67	25.014	168	55.984 0		210	204		155 JG	1 4.5111	
	1 223		48.2	67	19.969	168		% CCL12.5	217	264		163 JG	0 5m	Flushed T/C calls up not average with EM multiple times after this cost. Dida't notice anothing physics. Classed year plus-
	1 223	2	48.2	67	20.048	168	56.008 0		21/	204		154 JG	U SIII	Flushed T/C cells up past oxygen with FW multiple times after this cast. Didn't notice anything obvious. Cleaned vent plugs.
									217	264			0.4	
20210715 955 1		1	47.8	67	14.976	168	56.031 0		21/	264		167 JG	0 4m	
	1 224	2	47.4	67	15.041	168	56.051 0					167 JG		
20210715 1051 1			47.1	67	9.969	168		% CCL11	217	264		198 JG	0 5m	brief pause after cast to muck about in the engine room. Issue with air compressor for gear controls. Began motor to next station at 1123
	1 225	2	47.1	67	10.027	168	55.861 0					211 JG		
20210715 1217 1			46.8	67	4.984	168	55.98 0		218	263		190 JG	0 4m	Vent plug didn't drain on T2/C2. Cleaned vent plugs. Passed over a 1.2 PSU less fresh front at 1200 UTC via underway data
20210715 1222 1			47	67	5.072	168	55.903 0	% CCL10.5				215 JG		
20210715 1315 1	1 227	1	46.3	66	59.982	168	55.987 0	% CCL10	218	262	23.5	186 JG	0 4m	
20210715 1320 1	1 227	2	46.2	67	0.084	168	55.943 0	% CCL10			224.2	203 JG		
20210715 1408 1		1	45.4	66	54.956	168	55.997 0	% CCL9.5	219	261		194 JG	0 2m	
20210715 1413 1		2	44.9	66	55.047	168	55.916 0					173 JG		
20210715 1413 1			43.4	66	49.959	168	56.017 0		218	258		177 JG	0.2m	
20210715 1457 1			43.4	66	50.026	168	56.029 0		210	230		183 JG	0 2111	
					50.026 44.989	168			218	255			0 3m	
	1 230		41.1	66					218	255		171 RJD	U 3M	
		2	41.1	66	45.052	168	56.067 0	,				169 RJD		
20210715 1554 1	7 221	1	42	66	39.945	168		% CCL8	218	256		186 RJD	0 3m	
20210715 1645 1				66	40.013	168	56.107 0	% CCL8			17	173 RJD		
20210715 1645 1 20210715 1649 1	1 231		41.9											
20210715 1645 1	1 231 1 232	1	41.9 44.5 44.3	66 66	34.937 35.006	168 168	56.046 0	% CCL7 % CCL7	218	256		171 RJD 179 RJD	0 3m	

0210715 1834 1				66	29.922	168	56.052			218	269		185 RJD	0 3m	
0210715 1841 1		2	55.4	66	29.92	168			% CCL6				205 RJD		
0210715 1926 1			55.1	66	24.964	168			% CCL5	217	269		184 RJD	0 3m	
0210715 1933 1	1 234	2	55	66	24.99	168	56.124	0	% CCL5			18	162 RJD		
0210715 2000 1	1 235	1	54.3	66	22.25	168	56.121	0	% CCL4	217	270		171 RJD	0 3m	Vent plug clean pre-cast
0210715 2006 1	1 235	2	54	66	22.315	168	56.163	0	% CCL4			16	169 RJD		
0210715 2034 1	1 236	1	54.8	66	19.739	168	57.015	0	% A3-21	219	270	25	160 RJD	0 3m	CTD file has "A3-17" as name in header
0210715 2039 1		2	54.8	66	19.813	168			% A3-21				RJD		
0210715 2053 1			55.5	66	18.71	168	56.231			210	271	17	168 RJD	0 2m	
										210	2/1			0 2111	
0210715 2059 1		2	55.2	66	18.799	168			% DL19.5				164 RJD		
0210715 2113 1		1	55.2	66	17.809	168	56.286	0	% DL19	218	271		140 RJD	0 3m	
0210715 2119 1	1 238	2	55.3	66	17.89	168	56.304	0	% DL19			27	165 RJD		
0210715 2136 1	1 239	1	55.5	66	16.576	168	56.223	0	% DL18.5	218	272	26	167 RJD	0 3m	
0210715 2142 1	1 239	2	55.7	66	16.671	168	56.23	0	% DL18.5			28	171 RJD		
0210715 2203 1	1 240	1	56.5	66	15.247	168	56.246	0	% DL18	218	271	24	164 RJD	0 3m	
0210715 2208 1		2	56.1	66	15.332	168			% DL18	-10	-/-		165 RJD	0 5	
						168				210	270			0.3	
0210715 2228 1		1	56	66	13				% DL17.5	218	270		155 RJD	0 3m	
0210715 2232 1		2	55.3	66	14.052	168			% DL17.5				170 RJD		
0210715 2250 1	1 242	1	55.8	66	12.715	168	56.241	0	% DL17	218	271		172 RJD	0 2m	
0210715 2254 1	1 242	2	55.9	66	12.795	168	56.235	0	% DL17			26	175 RJD		
0210715 2315 1	1 243	1	54.7	66	11.433	168	56.218	0	% DL16.5	220	269	33.9	204 KC	0 2m	Winds are even higher now, calling it for a while after this station
0210715 2319 1	1 243	2	54.6	66	11.595	168	56.14	0	% DL16.5			31.1	195 KC		
0210716 1435 1			44.6	65	48.233	168	56.121	_		221	264		188 JG	0 1m	
0210716 1433 1		2	45.7	65	48.404	168			% BS11	221	254		217 JG	0 2111	
										224	201			0.1	
0210716 1450 1		1	46	65	47.722	168			% BS11.5	221	264		223 JG	0 1m	
0210716 1455 1		2	47	65	47.818	168			% BS11.5				230 JG		
0210716 1456 5		1	47.5	65	47.858	168	53.667		% BS11.5 Laramie	5			235 RJD	0 1m	
0210716 1503 5	5 34	2	47	65	48.032	168	53.521		% BS11.5 Laramie			37	227 RJD		
0210716 1515 1		1	43.3	65	47.169	168			% BS12	218	258		210 RJD	0 1m	
0210716 1520 1		2	43.2	65	47.197	168			% BS12				198 RJD		
0210716 1531 1		1	48.3	65	46.706	168		-	% BS12.5	219	261		215 RJD	0 1m	
0210716 1531 1		2	48.8	65	46.737	168			% BS12.5	210	201		201 RID	0 1111	
								-			26-			0.4	
0210716 1546 1		1	50.6	65	46.252	168			% BS13	218	265		215 RJD	0 1m	
0210716 1551 1		2	50.6	65	46.352	168			% BS13				211 RJD		
0210716 1550 5	5 35	1	51.6	65	46.467	168	47.134		% BS13 Laramie			22	198 RJD	0 1m	
0210716 1611 5	5 35	2	51	65	46.937	168	46.999		% BS13 Laramie			21	188 RJD		
0210716 1625 1	1 249	1	51.2	65	45.771	168	45.509	0	% BS13.5	218	265	18	189 RJD	0 1m	
0210716 1629 1		2	51.2	65	45.799	168			% BS13.5				189 RID		
0210716 1639 1		1	51.2	65	45.213	168		-	% BS14	210	265		181 RJD	0 1.5m	
0210716 1643 1		2	51.4	65	45.257	168			% BS14	210	203		216 RJD	0 1.3111	
								-							
0210716 1651 1			50.4	65	44.768	168			% BS14.5	218	264		206 RJD	0 1m	
0210716 1655 1		2	50.4	65	44.798	168			% BS14.5				217 RJD		
0210716 1656 5		1	50.4	65	44.861	168	41.428		% BS14.5 Laramie				214 RJD	0 1.5m	
0210716 1705 5	5 36	2	50.1	65	44.661	168	40.48		% BS14.5 Laramie			20	183 RJD		
0210716 1717 1	1 252	1	50.1	65	44.283	168	39.751	0	% BS15	218	265	18	108 RJD	0 1m	
0210716 1721 1	1 252	2	50.1	65	44.357	168	39.581	0	% BS15			24	190 RJD		
0210716 1732 1	1 253	1	50.1	65	43.817	168	37.746	0	% BS15.5	218	264	25	187 RJD	0 1.5m	
0210716 1736 1		2	50.2	65	43.851	168			% BS15.5	-10	204		220 RJD	0 1.5	
0210716 1730 1			50.2	65	43.291	168			% BS16	240	264		207 RID	0 1m	
										218	264			0 1m	
0210716 1752 1		2	49.9	65	43.345	168			% BS16				182 RJD		
0210716 1752 5		1	50	65	43.414	168	35.408		% BS16 Laramie	217	267	26	208 RJD	0 2m	
0210716 1800 5		2	50.2	65	43.293	168	35.29		% BS16 Laramie				RJD		
0210716 1813 1	1 255	1	50.6	65	42.727	168	33.464	0	% BS16.5	218	265	22	187 RJD	0 2m	
0210716 1818 1		2	50.1	65	42.774	168			% BS16.5				212 RJD		
0210716 1828 1	1 256	1	53.1	65	42.191	168	31.292	0	% BS17	218	264	21	184 RJD	0 3m	
0210716 1832 1		2	53.3	65	42.281	168			% BS17	-10	20.		206 RJD	0 5	
0210716 1832 1			52.3	65	41.657	168				240	263		187 RJD	0 2.5m	
									% BS17.5	218	203			U 2.5M	
0210716 1847 1		2	51.9	65	41.74	168			% BS17.5				197 RJD		
0210716 1828 5		1	51.7	65	41.748	168	29.253		% BS17.5 Laramie				214 RJD	0 2m	
0210716 1857 5	5 38	2	52.1	65	41.953	168	29.151		% BS17.5 Laramie			25	141 RJD		
0210716 1909 1	1 258	1	52	65	41.11	168	26.86	0	% BS18	218	268	24	197 RJD	0 2m	
0210716 1914 1		2	51.9	65	41.189	168			% BS18				217 RJD		
0210716 1923 1		1	50.9	65	40.673	168		-	% BS18.5	217	264		211 RJD	0 4m	
										21/	204			0 4111	
0210716 1927 1		2	51.1	65	40.747	168			% BS18.5		26-		207 RJD	0.5	
0210716 1952 1		1	50.5	65	40.341	168			% BS19	218	267		200 RJD	0 5m	
0210716 1956 1		2	50.3	65	40.439	168		-	% BS19				197 RJD		
210716 1957 5	5 39	1	50.4	65	40.533	168	23.169		% BS19 Laramie			25	201 RJD	0 5m+	
0210716 2005 5	5 39	2	50.8	65	40.827	168	23.091		% BS19 Laramie				198 RJD		
0210716 2020 1		1	49	65	39.811	168	21.277		% BS19.5	218	265	29	201 RJD	0 5m+	
0210716 2024 1		2	48.9	65	39.894	168			% BS19.5				211 RJD		
			46.9			168				240	263		217 RJD	0 5m	
0210716 2037 1				65	39.245				% BS20	218	203			U 5M	
0210716 2041 1		2	46.7	65	39.309	168		-	% BS20				202 RJD		
0210716 2051 1		1	44.5	65	38.958	168			% BS20.5	218	263		206 RJD	0 5m	Mistakenly named BS20 in cast header file
0210716 2055 1	1 263	2	44.1	65	39.082	168	17.02	0	% BS20.5			24	204 RJD		
0210716 2056 5		1	44.2	65	39.271	168	17.002		% BS20.5 Laramie				200 RJD	0 5m	
0210716 2106 5		2	44.2	65	39.302	168	17.002		% BS20.5 Laramie				195 RJD	0 5	
0210716 2106 3		1	40.4	65	38.536	168				240	260		240 RJD	0 2m	
0210716 2124 1 0210716 2128 1									% BS21	218	266			U 2m	
		2	40.9	65	38.725	168			% BS21				299 RJD		
				65	38.027	168	12.858	1	% BS21.5	218	262	24	191 RJD	0 3m	
0210716 2128 1 0210716 2149 1 0210716 2154 1			37.1 37.2	65	38.168	168	12.832						111 RJD		

20210716	2208	1	266	1	29.9	65	37.431	168	10.657	1	% BS22	218	254	25	170 RJD	0 4m	
20210716	2212	1	266	2	30.5	65	37.644	168	10.81	1	% BS22			30	215 RJD		
20210716	2214	5	41	1	30.2	65	37.77	168	10.922		% BS22 Laramie			30	111 RJD	0 4m	
20210716	2224	5	41	2	31.5	65	37.978	168	11.354		% BS22 Laramie			28	120 RJD		
20210716				1	37.1	65	36.86	168	13.078	0	% SBSnn1.5	218	258		240 RJD	0 2m	Cast named SBSnn2 in header, but is SBSnn1.5
20210716			267	2	37.5	65	37.177	168	13.36	0	% SBSnn1.5				210 RJD		
20210716				1	44	65	35.628	168	17.385		% SBSnn2.5	219	259		203 KC	0 2m	
20210716			268	2	44.1	65	35.778	168	17.379		% SBSnn2.5				150 KC		
20210716				1	47.2	65	34.268	168	21.924		% SBSnn3.5	219	263		216 KC	0 4m	
20210716			269	2	47.6	65	34.383	168	21.932		% SBSnn3.5				186 KC		
20210716			270		50.2	65	33.089	168			% SBSnn4.5	219	265		204 KC	0.5 4m	
20210717			270	2		65	33.204	168			% SBSnn4.5				192 KC		
20210717			271		58.4	65	31.867	168	30.817		% SBSnn5.5	219	274		210 KC	1 3m	
20210717			271		56.8	65	31.986	168	30.772		% SBSnn5.5				194 KC		
20210717			272		54.9	65	30.634	168	35.292		% SBSnn6.5	219	271		212 KC	1 2m	
20210717			272	2	54.6	65	30.732	168	35.229		% SBSnn6.5				197 KC		
20210717				1	55	65	29.375	168	39.846		% SBSnn7.5	220	272		208 KC	1 2m	
20210717				2	54.2	65	29.46	168	39.8		% SBSnn7.5				201 KC		
20210717				1	58	65	28.152	168	44.286		% SBSnn8.5	220	274		203 KC	1 2m	
20210717					58.2	65	28.253	168	44.236	0	% SBSnn8.5				200 KC		
20210717			275		54.9	65	26.887	168	48.945	0	% SBSnn9.5	219	272		184 KC	1 1m	
20210717			275		55.7	65	26.978	168	49.002	0	% SBSnn9.5				203 KC		
20210717					56.7	65	25.661	168	53.421		% SBSnn10.5	219	272		186 KC	1 1m	
20210717	227	1	276	2	56.9	65	25.725	168	53.466	0	% SBSnn10.5			18.3	198 KC		

FILE FORMAT

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LABORATORY

IsoLab, Department of Earth and Space Sciences, University of Washington 206.543.6327 * isolab@uw.edu * https://isolab.ess.washington.edu/

METHOD

Your samples were analyzed on a Picarro - sn(HIDS2064) - named Abel. You can read more about our implementation of this method on our website here: https://isolab.ess.washington.edu/laboratory/water-dD-d18O.php or here https://isolab.ess.washington.edu/SOPs/abel.php

ANALYSIS

Start Time of Analysis: 2021/08/03 08:12:53

Original Filename: HIDS2064_IsoWater_20210803_150950_combined.csv Reduced Filename: HIDS2064_IsoWater_20210803_150950_combined_reduced.txt

Run comments:

REFERENCE MATERIALS

All internationally recognized reference material accepted values can be found at the CIAAW (http://www.ciaaw.org/).

All IsoLab in-house reference material accepted values can be found at https://isolab.ess.washington.edu/resources/standards.php#water.

For this particular analysis, the accepted values are from the MATLAB script Water Standards: 190723.

Reference Waters in this run and their accepted values: Reference Water Accepted d Accepted d180 (vs VSMOW)

KD 0.65 0 BW -156.87 -20.01 SW -75.63 -10.55

RUN INFORMATION

Number of Injections per vial: 10

Number of Injections discarded from beginning of each vial: 5

dD memory estimate: 0.84899 d180 memory estimate: 0.92273

Individual reference water vial raw measurement

TrayPos		Reference I F	RawMean I	RawStdDev	RawMean (RawStdDev	RawMean (RawStdDev d180	Э
	2	SW	20097.8	131.6613	-71.2606	0.065286	-6.6102	0.009365	
	4	RW	19693	214.5355	-14.6118	0.046949	8.9794	0.019604	
	6	KD	19829.4	144.1676	5.4224	0.11311	4.015	0.02487	
	8	BW	19702.4	155.9336	-152.178	0.07681	-16.1366	0.033254	
	14	RW	19885	286.256	-13.7372	0.10722	9.159	0.01239	
	16	BW	19936.2	190.0071	-152.29	0.1061	-16.1022	0.024489	
	18	KD	19824	91.2469	5.4064	0.15733	3.992	0.020396	
	20	SW	19864.8	35.8636	-70.4502	0.49765	-6.5546	0.054427	
	26	BW	19864.4	43.6268	-152.412	0.056116	-16.0962	0.018363	
	28	SW	19708.2	29.853	-70.9318	0.082433	-6.5984	0.01274	
	30	KD	19945.8	90.2258	5.5374	0.05513	3.9972	0.01429	
	32	RW	19795	72.6567	-13.7266	0.15068	9.1486	0.026651	
	34	USGS45	20004.4	181.4561	-5.6562	0.10175	1.746	0.030992	
	35	USGS45	19995.4	31.2698	-5.4624	0.11373	1.7776	0.02122	

Reference Water	Mean_H2C	StdDev_H2	Mean_dD_	StdDev_dD	Mean_d18	StdDev_d1 n	
raw KD	19866.4	68.8154	5.4554	0.071463	4.0014	0.012062	3
raw BW	19834.33	119.7648	-152.294	0.11693	-16.1117	0.0218	3
raw SW	19890.27	196.0445	-70.8809	0.40759	-6.5877	0.029295	3
corrected KD			0.65	0.087577	5.92E-16	0.014941	3
corrected BW			-156.87	0.10233	-20.01	0.019222	3
corrected SW			-75.5766	0.41998	-10.5347	0.02772	3

	Accuracy	Precision
dD	0.053382	0.41998
d18O	0.015324	0.02772

Reference Waters

Date	TrayPos	Reference M	ean_H2C S	StdDev_H2 N	/lean_dD_ S	StdDev_dD I	Mean_d18	StdDev_d18O
8/3/2021 9:47	T1-02	SW	20097.8	131.6613	-75.9793	0.065286	-10.5525	0.009365
8/3/2021 12:53	T1-04	RW	19693	214.5355	-19.4102	0.046949	4.9569	0.019604
8/3/2021 16:00	T1-06	KD	19829.4	144.1676	0.59782	0.11311	0.017232	0.02487
8/3/2021 19:06	T1-08	BW	19702.4	155.9336	-156.769	0.07681	-20.0321	0.033254
8/4/2021 9:38	T1-14	RW	19885	286.256	-18.5209	0.10722	5.1325	0.01239
8/4/2021 12:44	T1-16	BW	19936.2	190.0071	-156.868	0.1061	-20.0004	0.024489
8/4/2021 15:50	T1-18	KD	19824	91.2469	0.60107	0.15733	-0.00935	0.020396
8/4/2021 18:56	T1-20	SW	19864.8	35.8636	-75.1412	0.49765	-10.5027	0.054427
8/5/2021 4:15	T1-26	BW	19864.4	43.6268	-156.973	0.056116	-19.9975	0.018363
8/5/2021 7:21	T1-28	SW	19708.2	29.853	-75.6093	0.082433	-10.5488	0.01274
8/5/2021 10:27	T1-30	KD	19945.8	90.2258	0.75111	0.05513	-0.00788	0.01429
8/5/2021 13:33	T1-32	RW	19795	72.6567	-18.4815	0.15068	5.1166	0.026651
8/5/2021 16:39	T1-34	USGS45	20004.4	181.4561	-10.4197	0.10175	-2.2488	0.030992
8/5/2021 18:12	T1-35	USGS45	19995.4	31.2698	-10.2246	0.11373	-2.2177	0.02122

Sample Information:

Date	Tray-Pos	Sample Nai N	√lean_H2C	StdDev_H2	Mean_dD_	StdDev_dD I	Mean_d18	StdDev_d18O	
8/3/2021 22:12	2 T1-10	LIS3	19566	166.5983	-33.3819	0.098396	-4.2915	0.019424	
8/4/2021 1:19	71-12	LIS2	19574.6	61.476	-23.657	0.16012	-3.0929	0.025762	
8/4/2021 22:03	3 T1-22	LIS2	19615	106.066	-23.6629	0.094302	-3.1141	0.020107	
8/5/2021 1:09	T1-24	1153	19544	57 8835	-32 6919	0 21168	-4 2751	0.015659	

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